

**BAB V**  
**ANALISIS DAN DISAIN STRUKTUR**

**5.1. Data Perencanaan**

Data perencanaan memuat data – data yang diperlukan dalam proses analisis

**5.1.1. Parameter Bahan**

$f_y$	= kuat leleh baja karakteristik	= 36 ksi
$f'_c$	= kuat desak beton karakteristik	= 4 ksi
$E_c$	= modulus elastisitas beton	= $1750 \sqrt{f'_c}$ = 3500 ksi

**5.1.2. Asumsi yang digunakan**

a)	Tebal pelat atap	= 100 mm
b)	Tebal pelat lantai	= 120 mm
c)	Dimensi kolom	= 600 x 800 mm <sup>2</sup>
d)	Dimensi balok induk 1	= 250 x 500 mm <sup>2</sup>
e)	Dimensi balok induk 2	= 400 x 800 mm <sup>2</sup>
f)	Dimensi balok anak	= 200 x 400 mm <sup>2</sup>
g)	Dimensi sloof	= 200 x 400 mm <sup>2</sup>
h)	Tinggi antar tingkat	= 4000 mm
i)	Berat volume beton	= 24 KN/m <sup>3</sup>
j)	Berat volume pasangan batu bata	= 17 KN/m <sup>3</sup>

k) Tata guna ruang sebagai perkantoran dengan beban hidup lantai

$2,5\text{KN/m}^2$  dan beban hidup atap  $1\text{ KN/m}^2$

l) Lapis kedap air =  $0,02\text{ m} \times 0,21\text{ KN/m}^3$  =  $0,42\text{ KN/m}^2$

m) Penggantung + plafon =  $0,18\text{ KN/m}^2$

n) Disting AC =  $0,15\text{ KN/m}^2$

o) Pasir =  $0,03\text{m} \times 18\text{ KN/m}^3$  =  $0,54\text{ KN/m}^2$

p) Spesi =  $0,21\text{m} \times 3\text{ KN/m}^3$  =  $0,63\text{ KN/m}^2$

q) Tembok  $\frac{1}{2}$  bata =  $0,15\text{m} \cdot (4-0,8)\text{m} \cdot 17\text{ KN/m}^3$  =  $8,16\text{ KN/m}^2$

Tabel 5.1 Profil Rencana Kolom

Lantai	Kolom	
	Kolom tepi	Kolom tengah
10	W14x120	W14x120
9	W14x120	W14x120
8	W14x120	W14x120
7	W14x120	W14x120
6	W14x120	W14x120
5	W14x311	W14 x 257
4	W14x311	W14 x 257
3	W14x311	W14 x 257
2	W14x311	W14 x 257
1	W14x311	W14 x 257

Tabel 5.2 Profil Rencana Balok

Lantai	BALOK			
	Balok induk 1 6m tepi	Balok induk 2 12m tepi	Balok induk 3 12 m tengah	Balok anak
10	W14x 82	W21x 62	W24x 55	W16x 36
9	W14x 82	W21x 62	W24x 55	W16x 36
8	W14x 82	W21x 62	W24x 55	W16x 36
7	W14x 82	W21x 62	W24x 55	W16x 36
6	W14x 82	W21x 62	W24x 55	W16x 36
5	W14x 82	W21x 62	W24x 55	W16x 36
4	W14x 82	W21x 62	W24x 55	W16x 36
3	W14x 82	W21x 62	W24x 55	W16x 36
2	W14x 82	W21x 62	W24x 55	W16x 36
1	W14x 82	W21x 62	W24x 55	W16x 36

## 5.2. Perhitungan Gaya-Gaya Yang Bekerja Pada Struktur

### 5.2.1. Perhitungan Beban Akibat Beban Gravitasi

Pada bab ini dilakukan perhitungan terhadap portal arah X dan Y

#### a. Beban Merata pada balok atap

1) Beban mati pada pelat atap ( $W_D$ )

$$\text{Plat Atap (100 mm)} = 0,1 \text{ m} \times 24 \text{ KN/m}^3 = 2,4 \text{ KN/m}^2$$

$$\text{Lapis kedap air} = 0,02 \text{ m} \times 0,21 \text{ KN/m}^3 = 0,42 \text{ KN/m}^2$$

$$\text{Penggantung + plafon} = 0,18 \text{ KN/m}^2$$

$$\text{Dusting AC} = 0,15 \text{ KN/m}^2$$

$$W_D \text{ atap} = 3,15 \text{ KN/m}^2$$

2) Beban hidup plat atap

$$W_L \text{ atap} = 1 \text{ KN/m}^2$$

**b. Pembebanan pada balok lantai**

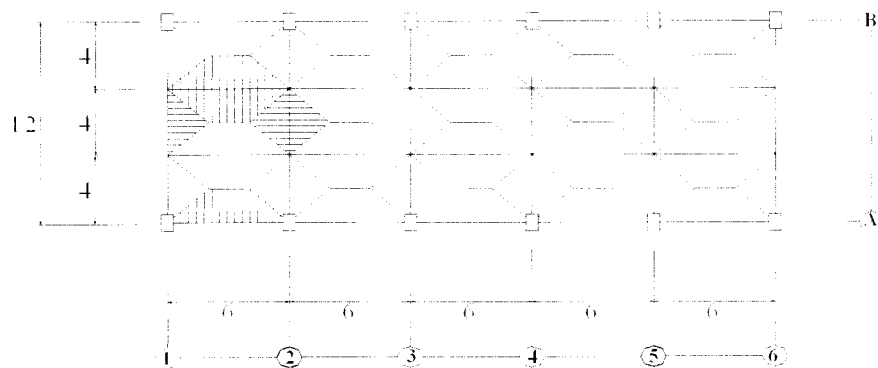
1 ) Beban mati pada pelat lantai ( $W_D$ )

Plat lantai	= 0,12 m x 24 KN/m <sup>3</sup>	= 2,88 KN/m <sup>2</sup>
Keramik	= 1 KN/m <sup>3</sup> x 0,24 m	= 0,24 KN/m <sup>2</sup>
Pasir	= 0,03 m x 18 KN/m <sup>3</sup>	= 0,54 KN/m <sup>2</sup>
Spesi	= 0,21m x 3 KN/m <sup>3</sup>	= 0,63 KN/m <sup>2</sup>
Dusting AC		= 0,15 KN/m <sup>2</sup>
Penggantung + plafon		= <u>0,18 KN/m<sup>2</sup></u>
	$W_D$ lantai	= 4,62 KN/m <sup>2</sup>
Tembok ½ bata = 0,15m. (4-0,8)m. 17 KN/m <sup>3</sup>		= 8,16 KN/m <sup>2</sup>

2 ) Beban hidup lantai perkantoran

$$W_L \text{ lantai} = 2,5 \text{ KN/m}^2$$

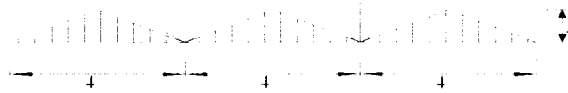
**5.2.1.1. Pembebanan pada Portal Variasi 1**



Gambar 5.1. Pembagian pembebanan pelat

a. Portal 1

1. Beban gravitasi pada balok atap



Gambar 5.2. beban merata dan terpusat balok atap portal 1

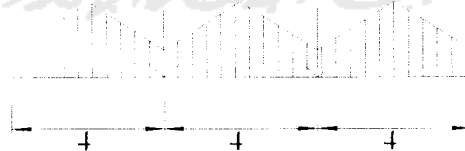
- Beban mati segitiga

$$\begin{aligned}W_{D, \text{atap}} &= W_D \cdot 2 \\ &= 3,15 \text{ KN/m}^2 \cdot 2 \text{ m} = 6,3 \text{ KN/m}\end{aligned}$$

- Beban hidup segitiga

$$\begin{aligned}W_{L, \text{atap}} &= W_L \cdot 2 \\ &= 1 \text{ KN/m}^2 \cdot 2 \text{ m} = 2 \text{ KN/m}\end{aligned}$$

2. Beban gravitasi pada balok lantai



Gambar 5.3. beban merata dan titik balok lantai portal 1

- Beban mati segitiga

$$\begin{aligned}W_{D, \text{lantai}} &= W_D \cdot 2 \\ &= 4,62 \text{ KN/m}^2 \cdot 2 = 9,24 \text{ KN/m}\end{aligned}$$

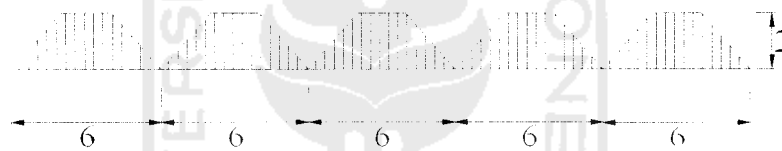
- Beban mati dinding = 8,16 KN/m'
- Beban hidup segitiga

$$\begin{aligned}
 w_{l,\text{lantai}} &= W_L \cdot 2 \\
 &= 2,5 \text{ KN/m}^2 \cdot 2 \text{ m} = 5 \text{ KN/m}'
 \end{aligned}$$

Untuk portal tengah, pembebanannya merupakan 2 kali pembebanan portal tepi tanpa beban mati dinding.

#### b. Portal A

##### 1. Beban gravitasi pada balok atap



Gambar 5.4. beban merata balok atap portal A

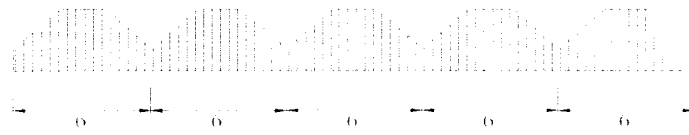
- Beban mati trapesium

$$\begin{aligned}
 w_{D,\text{atap}} &= W_D \cdot 2 \\
 &= 3,15 \text{ KN/m}^2 \cdot 2 \text{ m} = 6,3 \text{ KN/m}'
 \end{aligned}$$

- Beban hidup trapesium

$$\begin{aligned}
 w_{L,\text{atap}} &= W_L \cdot 2 \\
 &= 1 \text{ KN/m}^2 \cdot 2 \text{ m} = 2 \text{ KN/m}'
 \end{aligned}$$

2. Beban gravitasi pada balok lantai



Gambar 5.5. beban merata lantai portal A

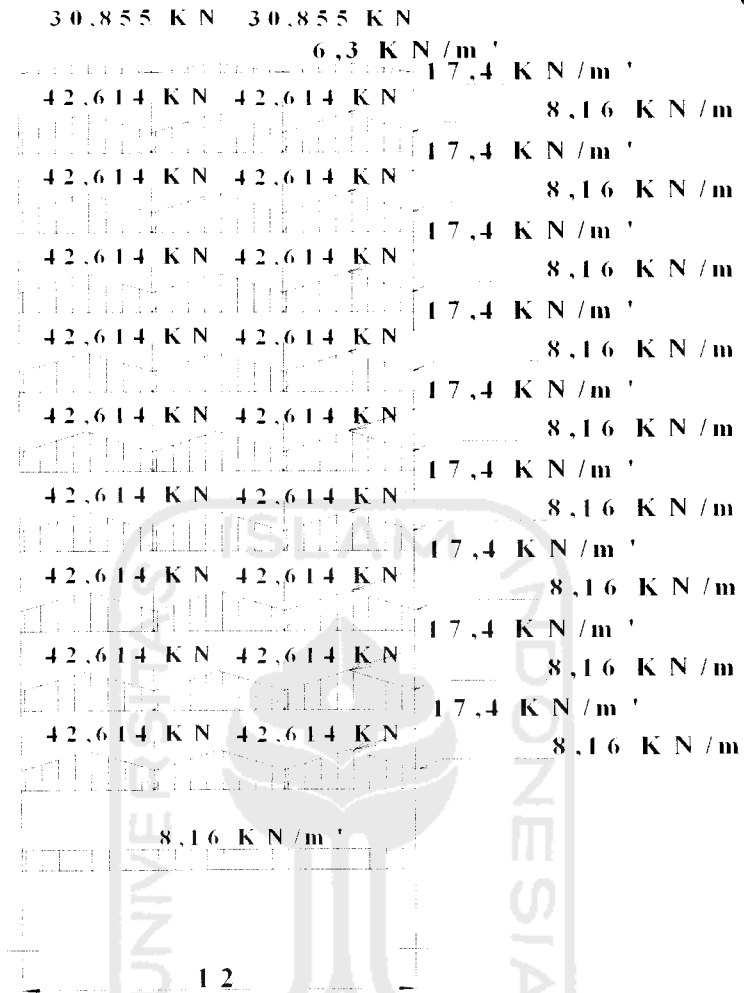
- Beban mati trapesium

$$\begin{aligned} W_{D \text{ lantai}} &= W_D \cdot 2 \\ &= 4,62 \text{ KN/m}^2 \cdot 2 \text{ m} = 9,24 \text{ KN/m} \end{aligned}$$

- Beban mati dinding = 8,16 KN/m

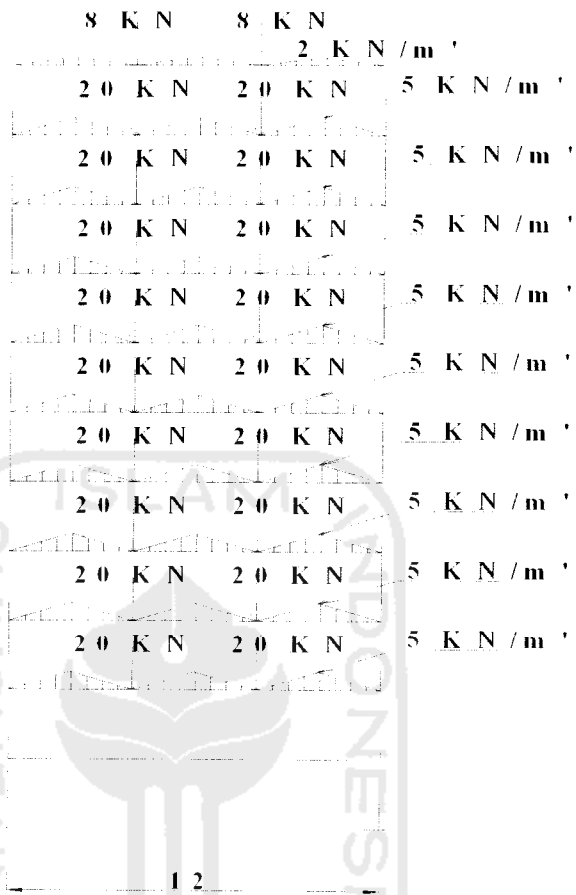
- Beban hidup trapesium

$$\begin{aligned} W_{L \text{ lantai}} &= W_L \cdot 2 \\ &= 2,5 \text{ KN/m}^2 \cdot 2 \text{ m} = 5 \text{ KN/m} \end{aligned}$$

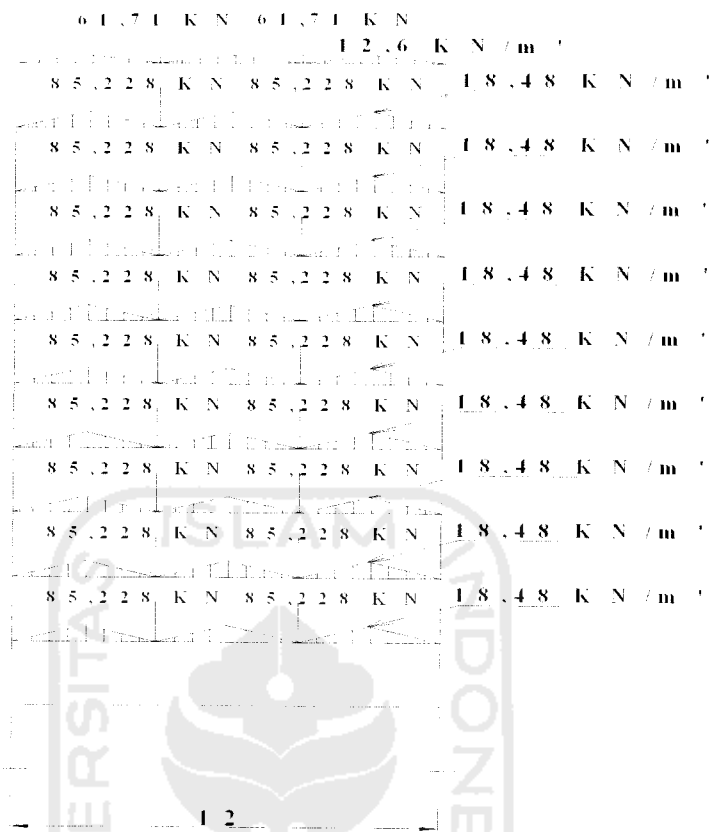


Gambar 5.6. Beban mati portal I V-1

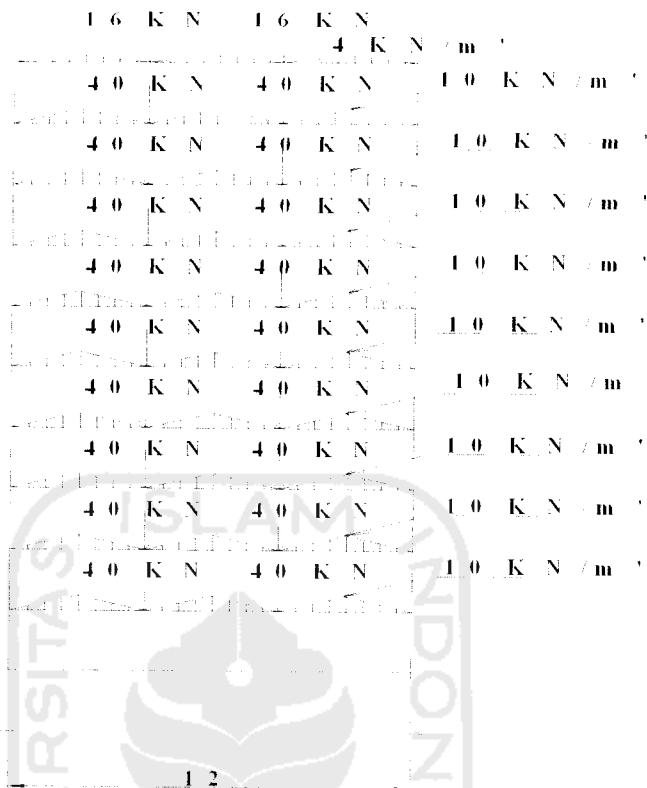




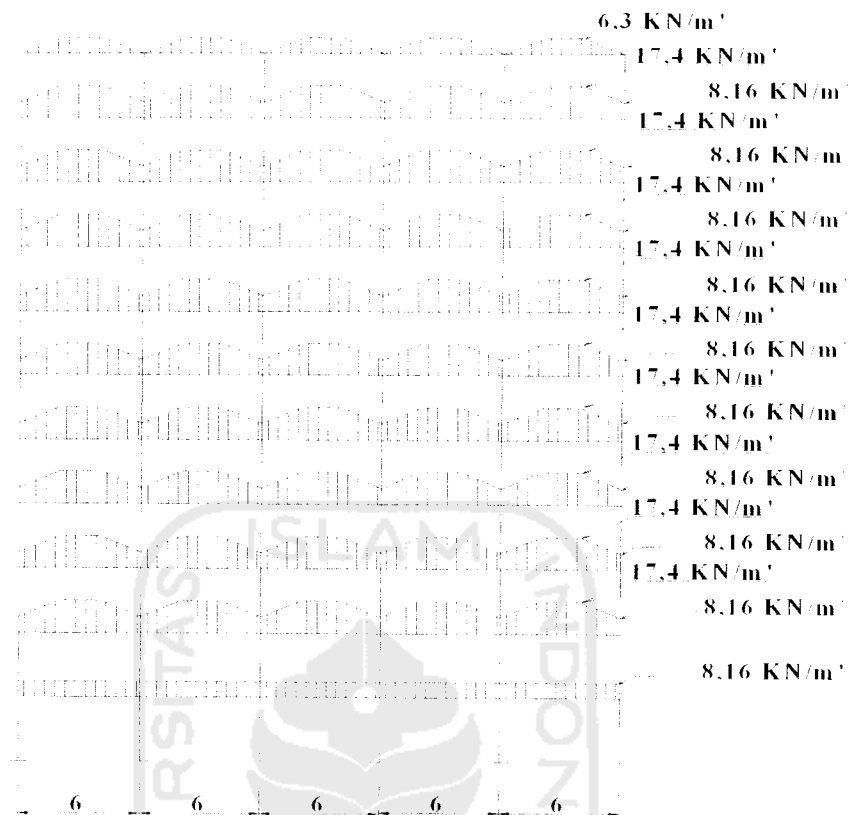
Gambar 5.7. Beban hidup portal 1 V-1



Gambar 5.8. Beban mati portal 2 V-1



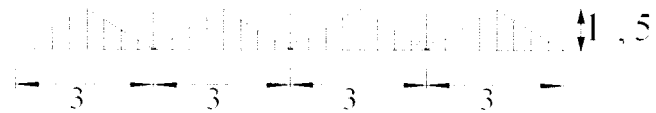
Gambar 5.9. Beban hidup portal 2 V-1



Gambar 5.10. Beban mati portal A V-1

a. Portal 1

1. Beban gravitasi pada balok atap



Gambar 5.13. beban merata dan terpusat balok atap portal 1

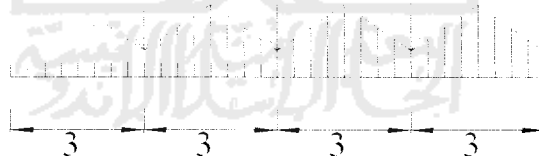
- Beban mati segitiga

$$\begin{aligned} W_{D \text{ atap}} &= W_D \cdot 1,5 \\ &= 3,15 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 4,725 \text{ KN/m} \end{aligned}$$

- Beban hidup segitiga

$$\begin{aligned} W_{L \text{ atap}} &= W_L \cdot 1,5 \\ &= 1 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 1,5 \text{ KN/m} \end{aligned}$$

2. Beban gravitasi pada balok lantai



Gambar 5.14. beban merata dan terpusat balok lantai portal 1

- Beban mati segitiga

$$\begin{aligned} W_{D \text{ lantai}} &= W_D \cdot 1,5 \\ &= 4,6 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 6,93 \text{ KN/m} \end{aligned}$$

- Beban mati dinding = 8,16 KN/m'

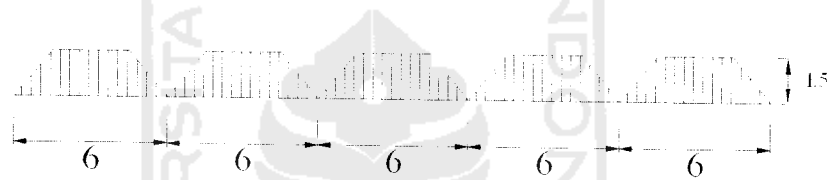
- Beban hidup segitiga

$$\begin{aligned}
 w_{\text{lantai}} &= W_L \cdot 1,5 \\
 &= 2,5 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 3,75 \text{ KN/m}
 \end{aligned}$$

Untuk portal tengah, pembebanannya merupakan 2 kali pembebanan portal tepi tanpa beban mati dinding.

### b. Portal A

1. Beban gravitasi pada balok atap



Gambar 5.15. beban merata balok atap portal A

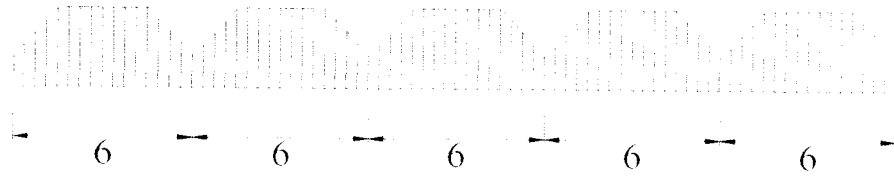
- Beban mati trapesium

$$\begin{aligned}
 w_{\text{atap}} &= W_D \cdot 1,5 \\
 &= 3,15 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 4,725 \text{ KN/m}
 \end{aligned}$$

- Beban hidup trapesium

$$\begin{aligned}
 w_L &= W_L \cdot 1,5 \\
 &= 1 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 1,5 \text{ KN/m}
 \end{aligned}$$

2. Beban gravitasi pada balok lantai



Gambar 5.16. beban merata lantai portal A

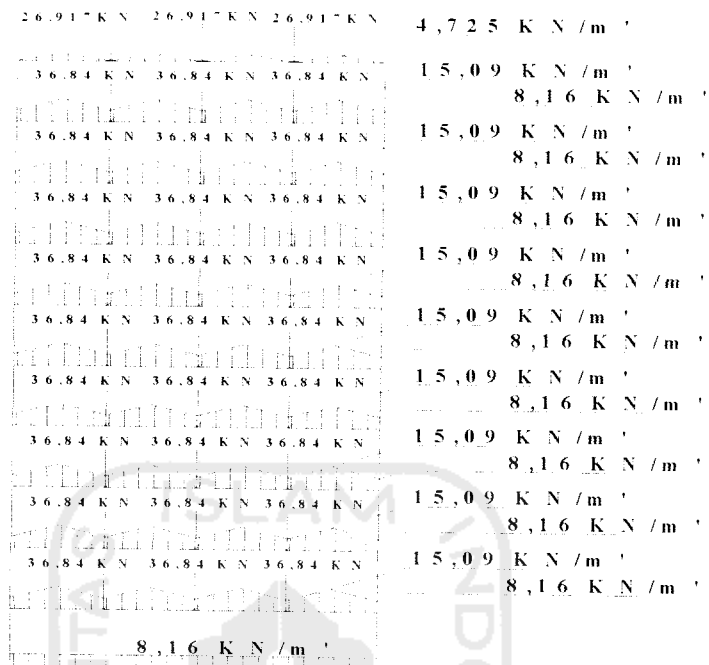
- Beban mati trapesium

$$\begin{aligned}w_{D\text{lantai}} &= W_D \cdot 1,5 \\ &= 4,62 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 6,93 \text{ KN/m}'\end{aligned}$$

- Beban mati dinding = 8,16 KN/m'

- Beban hidup trapesium

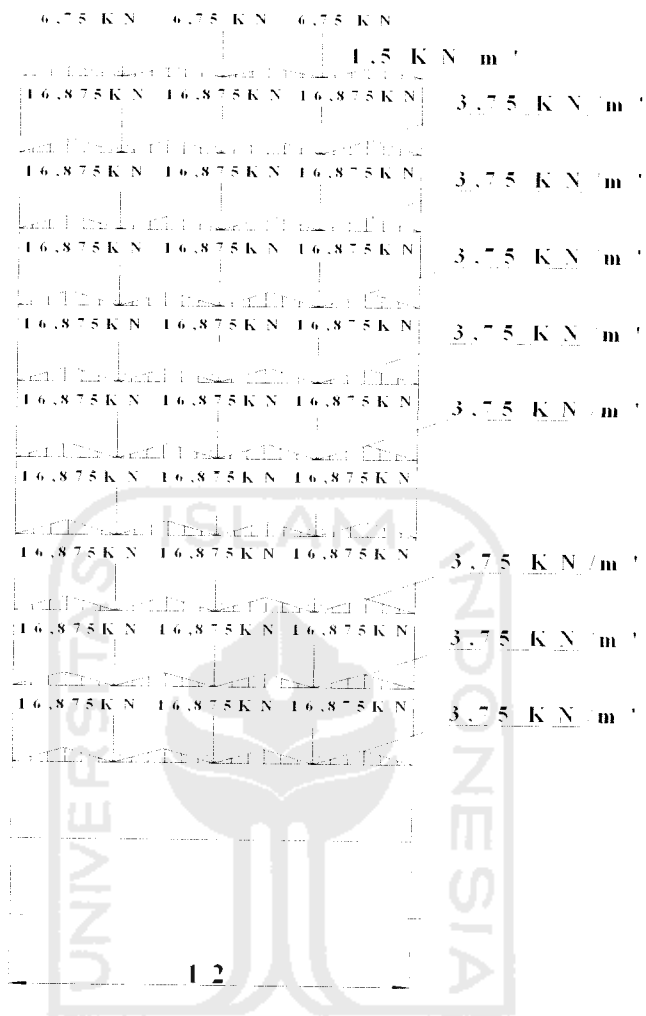
$$\begin{aligned}w_{L\text{lantai}} &= W_L \cdot 1,5 \\ &= 2,5 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 3,75 \text{ KN/m}'\end{aligned}$$



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Gambar 5.17. Beban mati portal 1 V-2

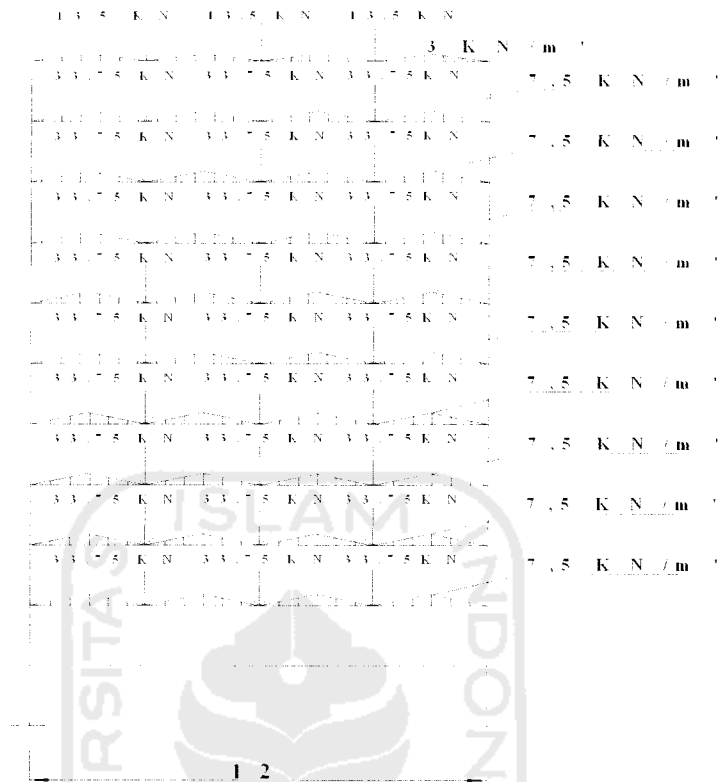




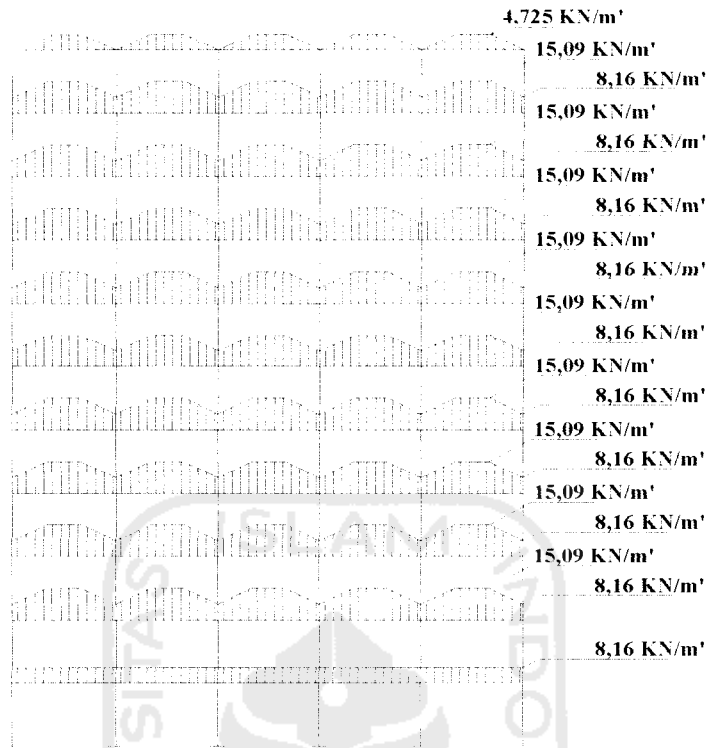
Gambar 5.18. Beban hidup portal 1 V-2



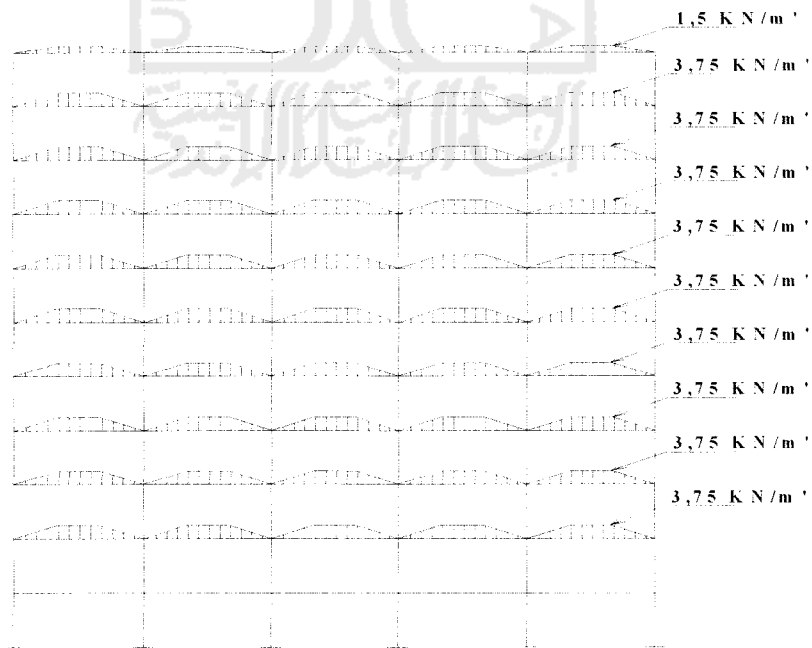
Gambar 5.19. Beban mati portal 2 V-2



Gambar 5.20. Beban hidup portal 2 V-2

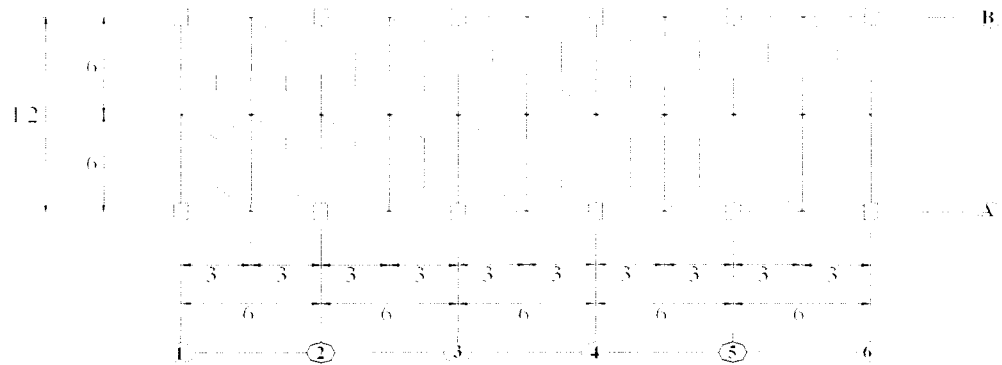


Gambar 5.21. Beban mati portal A V-2



Gambar 5.22. Beban hidup portal A V-2

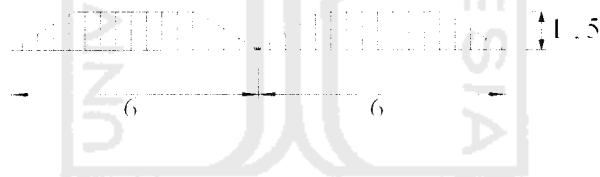
### 5.2.1.3. Pembebanan pada Portal Variasi 3



Gambar 5.23. Pembagian pembebanan pelat

#### a. Portal 1

##### 1. Beban gravitasi pada balok atap



Gambar 5.24. beban merata dan titik balok atap portal 1

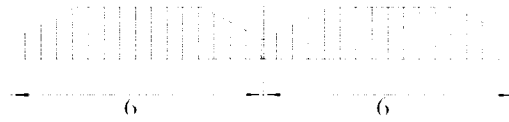
- Beban mati trapesium

$$\begin{aligned} W_{\text{Datap}} &= W_D \cdot 1,5 \\ &= 3,15 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 4,725 \text{ KN/m} \end{aligned}$$

- Beban hidup trapesium

$$\begin{aligned} W_{\text{L.atap}} &= W_L \cdot 1,5 \\ &= 1 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 1,5 \text{ KN/m} \end{aligned}$$

## 2. Beban gravitasi pada balok lantai



Gambar 5.25. beban merata dan terpusat balok lantai portal 1

- Beban mati trapesium

$$\begin{aligned}W_{D\text{lantai}} &= W_D \cdot 1,5 \\ &= 4,62 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 6,93 \text{ KN/m}\end{aligned}$$

- Beban mati dinding = 8,16 KN/m

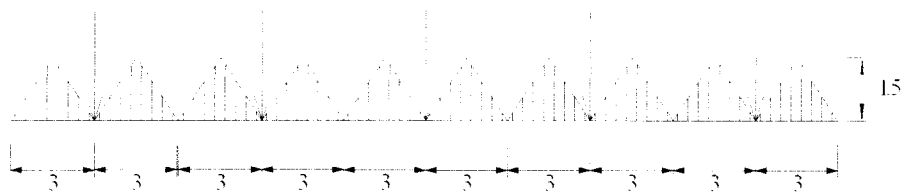
- Beban hidup trapesium

$$\begin{aligned}W_{L\text{lantai}} &= W_L \cdot 1,5 \\ &= 2,5 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 3,75 \text{ KN/m}\end{aligned}$$

Untuk portal tengah, pembebanannya merupakan 2 kali pembebanan portal tepi tanpa beban mati dinding.

### b. Portal A

#### 1. Beban gravitasi pada balok atap



Gambar 5.26 beban merata dan terpusat untuk balok atap portal A

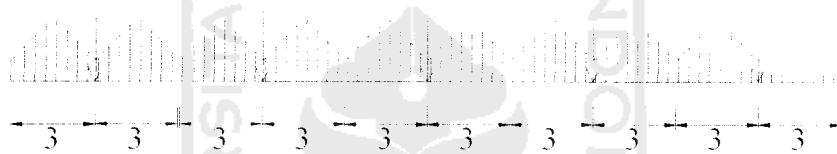
- Beban mati segitiga

$$\begin{aligned}
 w_{\text{atap}} &= W_D \cdot 1,5 \\
 &= 3,15 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 4,725 \text{ KN/m}
 \end{aligned}$$

- Beban hidup segitiga

$$\begin{aligned}
 w_{\text{atap}} &= W_L \cdot 1,5 \\
 &= 1 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 1,5 \text{ KN/m}
 \end{aligned}$$

## 2. Beban gravitasi pada balok lantai



Gambar 5.27. beban merata dan terpusat untuk balok lantai portal A

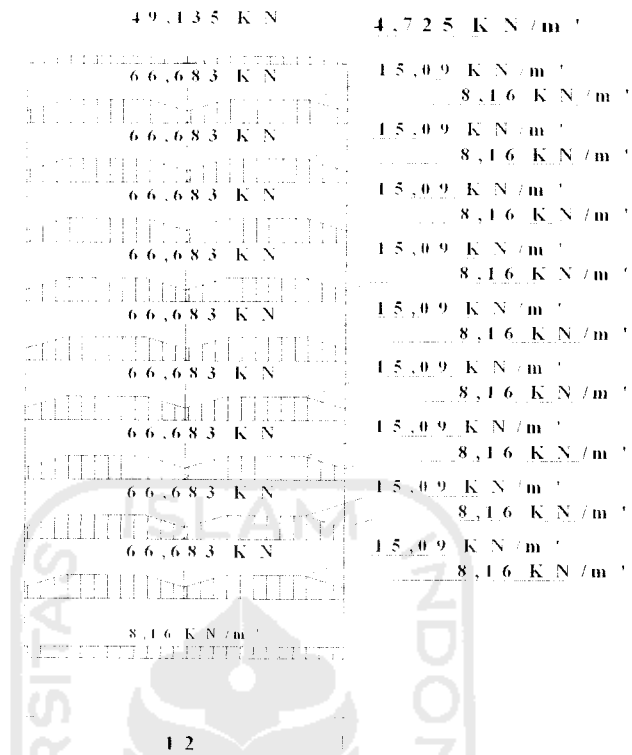
- Beban mati segitiga

$$\begin{aligned}
 w_{\text{lantai}} &= W_D \cdot 1,5 \\
 &= 4,62 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 6,93 \text{ KN/m}
 \end{aligned}$$

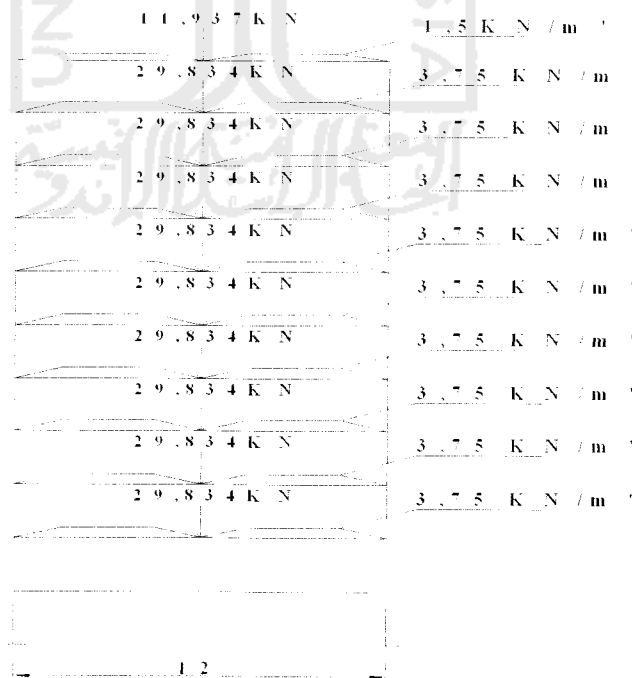
- Beban mati dinding = 8,16 KN/m'

- Beban hidup segitiga

$$\begin{aligned}
 w_{\text{lantai}} &= W_L \cdot 1,5 \\
 &= 2,5 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 3,75 \text{ KN/m}
 \end{aligned}$$

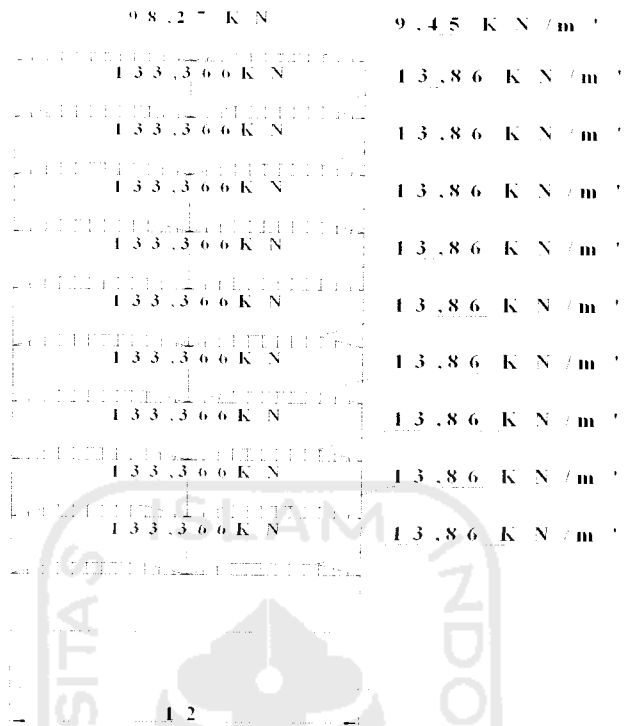


Gambar 5.28. Beban mati portal 1 V-3

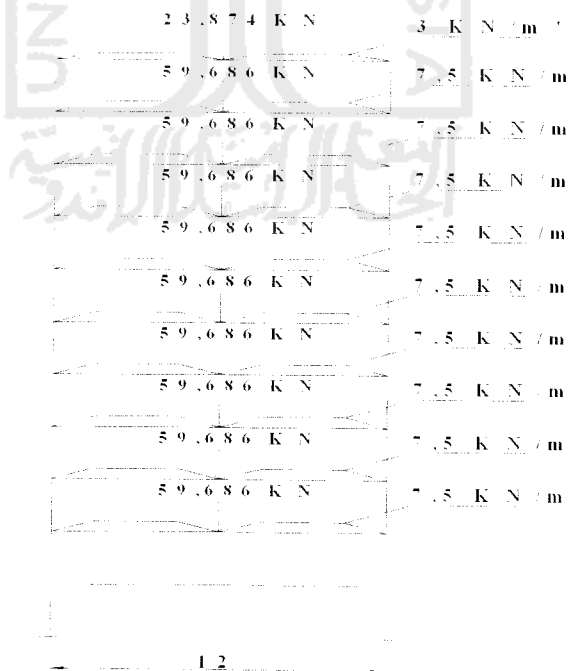


Gambar 5.29. Beban hidup portal 1 V-3



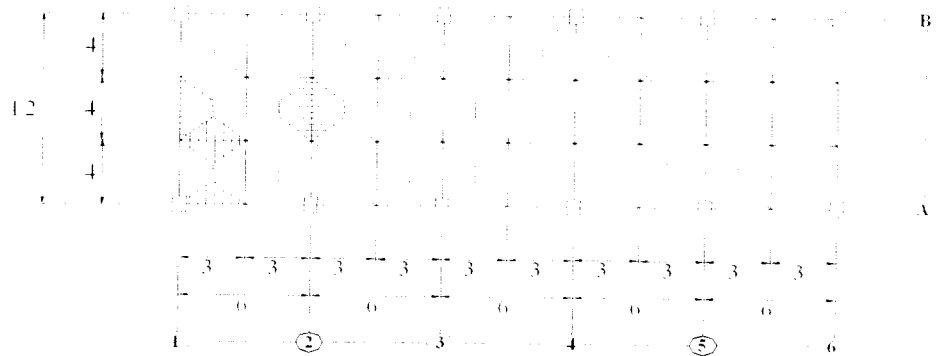


Gambar 5.30. Beban mati portal 2 V-3



Gambar 5.31. Beban hidup portal 2 V-3

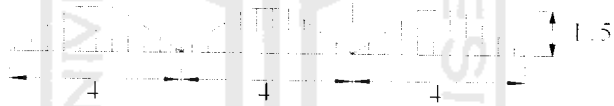
#### 5.2.1.4. Pembebanan pada Portal Variasi 4



Gambar 5.34. Pembagian pembebanan pelat

#### a. Portal 1

1. Beban gravitasi pada balok atap



Gambar 5.35. beban merata dan titik balok atap portal 1

- Beban mati trapesium

$$\begin{aligned} W_{\text{Datap}} &= W_D \cdot 1,5 \\ &= 3,15 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 4,725 \text{ KN/m} \end{aligned}$$

- Beban hidup trapesium

$$\begin{aligned} W_{\text{Latap}} &= W_L \cdot 1,5 \\ &= 1 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 1,5 \text{ KN/m} \end{aligned}$$

2. Beban gravitasi pada balok lantai



Gambar 5.36. beban merata dan terpusat balok lantai portal 1

- Beban mati trapesium

$$\begin{aligned}
 w_D &= W_D \cdot 1,5 \\
 &= 4,62 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 6,93 \text{ KN/m}
 \end{aligned}$$

- Beban mati dinding = 8,16 KN/m'

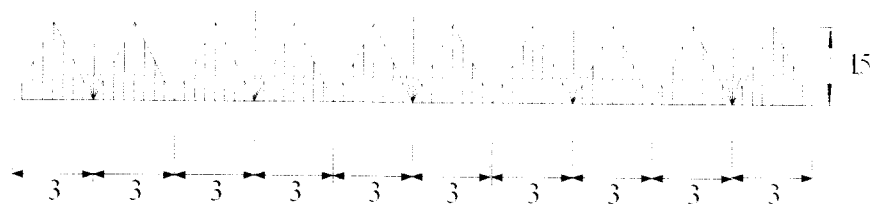
- Beban hidup trapesium

$$\begin{aligned}
 w_L &= W_L \cdot 1,5 \\
 &= 2,5 \text{ KN/m}^2 \cdot 1,5 \text{ m} = 3,75 \text{ KN/m}
 \end{aligned}$$

Untuk portal tengah, pembebanannya merupakan 2 kali pembebanan portal tepi tanpa beban mati dinding

**b. Portal A**

1. Beban gravitasi pada balok atap



Gambar 5.37. beban merata dan terpusat untuk balok atap

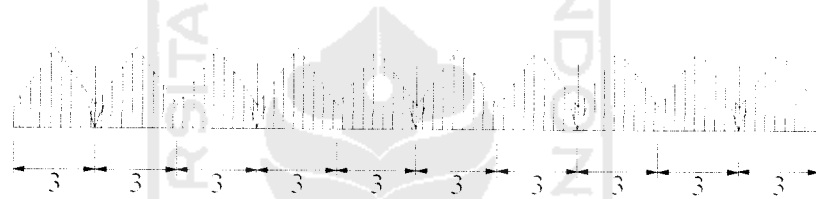
- Beban mati segitiga

$$\begin{aligned} W_{\text{atap}} &= W_D \cdot 1,5 \\ &= 3,15 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 4,725 \text{ KN/m} \end{aligned}$$

- Beban hidup segitiga

$$\begin{aligned} W_{\text{atap}} &= Q_L \cdot 1,5 \\ &= 1 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 1,5 \text{ KN/m} \end{aligned}$$

## 2. Beban gravitasi pada balok lantai



Gambar 5.38. beban merata dan terpusat untuk balok lantai portal A

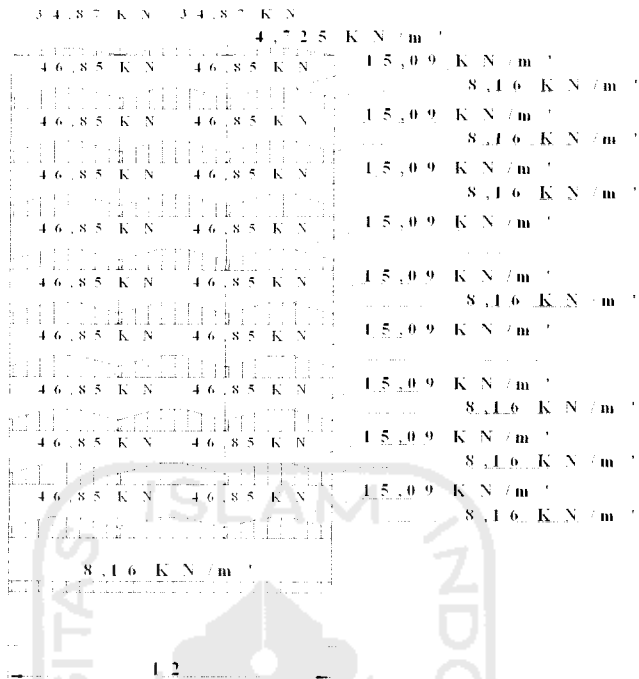
- Beban mati segitiga

$$\begin{aligned} W_{\text{lantai}} &= W_D \cdot 1,5 \\ &= 4,62 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 6,93 \text{ KN/m} \end{aligned}$$

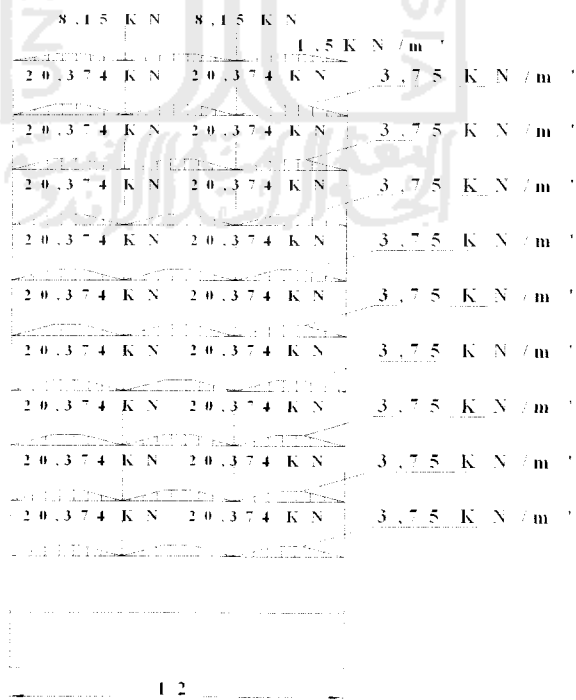
- Beban mati dinding = 8,16 KN/m

- Beban hidup segitiga

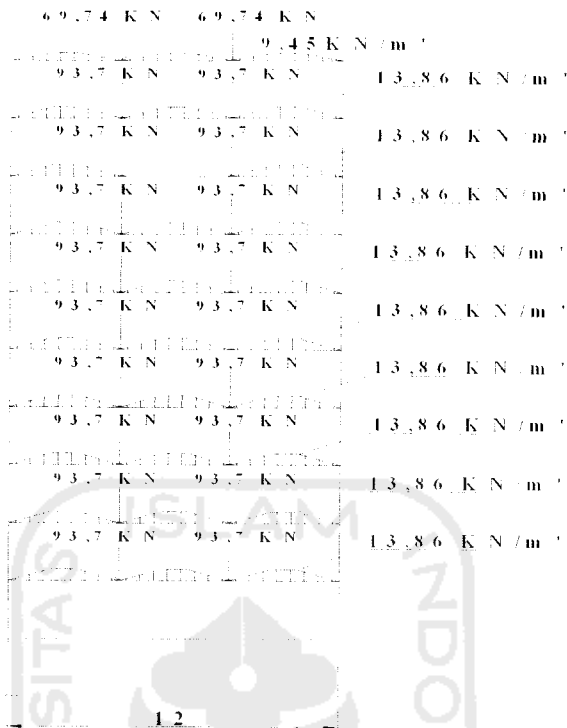
$$\begin{aligned} W_{\text{lantai}} &= W_L \cdot 1,5 \\ &= 2,5 \text{ KN/m}^2 \cdot 1,5 \text{ m} &= 3,75 \text{ KN/m} \end{aligned}$$



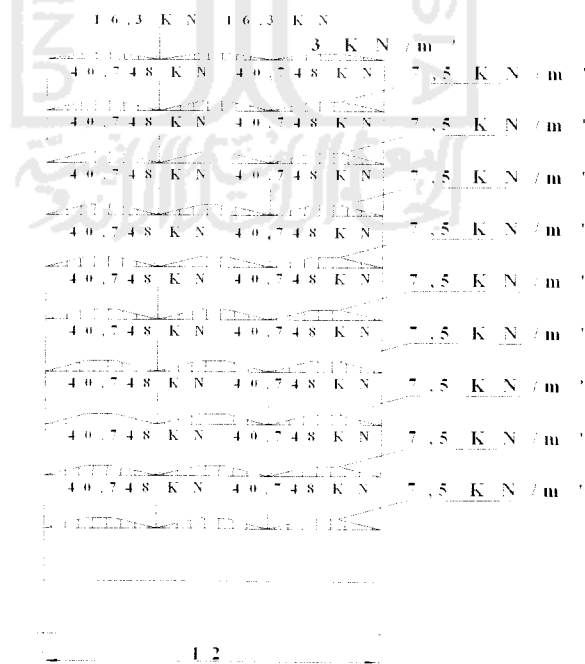
Gambar 5.39. Beban mati portal 1 V-4



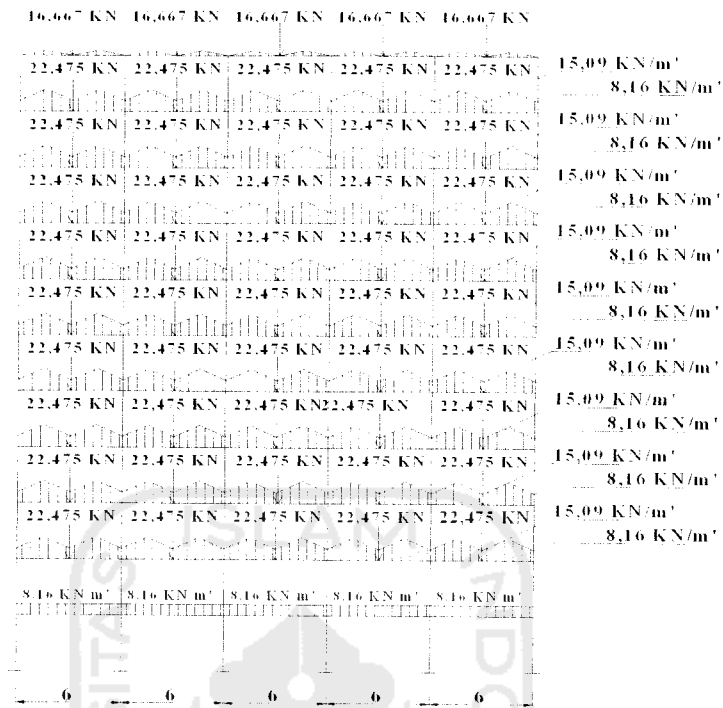
Gambar 5.40. Beban hidup portal 1 V-4



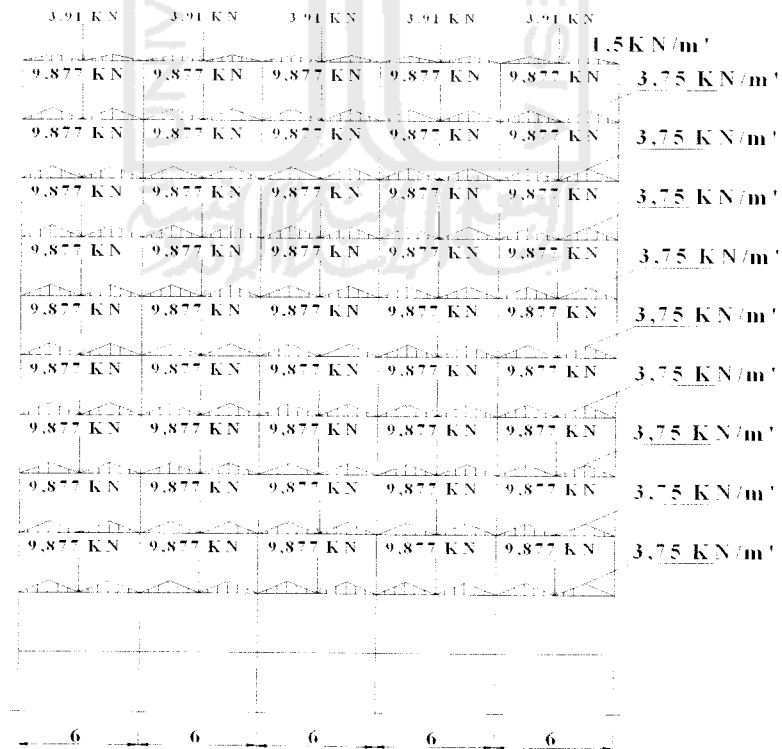
Gambar 5.41. Beban mati portal 2 V-4



Gambar 5.42. Beban hidup portal 2 V-4



Gambar 5.43. Beban mati portal A V-4



Gambar 5.44. Beban hidup portal A V-4

### 5.2.2. Perhitungan Beban Akibat Beban Gempa

Perhitungan gaya geser dasar horizontal akibat beban gempa diawali dengan menghitung berat total bangunan ( $W_t$ ), menentukan waktu getar bangunan ( $T$ ), koefisien gempa dasar ( $C$ ), factor keutamaan ( $I$ ), dan factor jenis struktur ( $K$ ).

#### a. Berat Bangunan Total

Contoh perhitungan portal variasi 1

##### 1. Atap

Beban mati ( $W_D$ )

$$\text{Plat Atap} = A.B.Q_D \text{ atap} = 12,5\text{m} \times 30,4\text{m} \times 3,15 \text{ KN/m}^2 = 11970,4 \text{ KN}$$

$$\text{Balok Induk}_1 = b.h.I.b_j \text{ ,jumlah} = 0,25.(0,5-0,1) (6-0,6).24 \text{ KN/m}^3 .10 = 129,6 \text{ KN}$$

$$\text{Balok Induk}_2 = b.h.I.b_j \text{ ,jml} = 0,4.(0,8-0,1)\text{m}.(12-0,8)\text{m}.24\text{KN/m}^3 .6=451,584\text{KN}$$

$$\text{Balok Anak}_1 = b.h.I.b_j \text{ ,juml} = 0,2.(0,4-0,1)\text{m} .(6-0,4\text{m}.2 \text{ KN/m}^3 .4.10= 80,64 \text{ KN}$$

$$\text{Kolom} = b.h.I/2H.b_j \text{ ,jumlah} = 0,6\text{m}.0,8\text{m}.2\text{m}.24 \text{ KN/m}^3 .12 =276,48 \text{ KN}$$

$$\begin{array}{r} \text{-----} \\ \text{W}_D \end{array} = 2135,30 \text{ KN}$$

Beban hidup

$$\text{W}_L = a.b.Q_L \text{ .koef reduksi} = 12,5.30,4.1.0.8 = 114,00 \text{ KN}$$

$$\begin{array}{r} \text{-----} \\ \text{W}_t \end{array} = 2249,30 \text{ KN}$$



## 2. Lantai 10

Beban mati

$$\text{Plat Lantai} = A.B.Q_{D1} \text{ lantai} = 12,5\text{m} \cdot 30,4\text{m} \cdot 4,62 \text{ KN/m}^2 = 1755,6 \text{ KN}$$

$$\text{Balok Induk}_1 = b.h.l.b_j \cdot \text{jml} = 0,25 \cdot (0,5-0,12)\text{m} \cdot (6-0,6)\text{m} \cdot 24\text{KN/m}^3 \cdot 10 = 123,12\text{KN}$$

$$\text{Balok Induk}_2 = b.h.l.b_j \cdot \text{jml} = 0,4 \cdot (0,8-0,12)\text{m} \cdot (12-0,8)\text{m} \cdot 24\text{KN/m}^3 \cdot 6 = 438,682 \text{ KN}$$

$$\text{Balok Anak}_1 = b.h.l.b_j \cdot \text{jml} = 0,2 \cdot (0,4-0,12)\text{m} \cdot (6-0,4)\text{m} \cdot 24 \text{ KN/m}^3 \cdot 10 = 75,264 \text{ KN}$$

$$\text{Kolom} = 0,6\text{m} \cdot 0,8\text{m} \cdot 24 \text{ KN/m}^3 \cdot 4 \cdot 12 = 552,96 \text{ KN}$$

$$\text{Tembok}_1 = \text{tebal} \cdot L \cdot H \cdot b_j \cdot \text{jml} = 0,15\text{m} \cdot (4-0,8)\text{m} \cdot (12-0,8)\text{m} \cdot 17,2\text{KN/m}^3 = 182,784\text{KN}$$

$$\text{Tembok}_2 = \text{tebal} \cdot L \cdot H \cdot b_j \cdot \text{jml} = 0,15\text{m} \cdot (4-0,5)\text{m} \cdot (6-0,6)\text{m} \cdot 17 \text{ KN/m}^3 \cdot 10 = 481,95\text{KN}$$

$$\text{W}_D = 3610,36 \text{ KN}$$

$$\text{Beban hidup} = a.b.Q_l \cdot \text{koef reduksi} = 12,5\text{m} \cdot 30,4\text{m} \cdot 2,5 \text{ KN/m}^2 \cdot 0,3 = 285,00 \text{ KN}$$

$$\text{W}_{total} = 3895,36 \text{ KN}$$

**3. Lantai 9,8,7,6,5,4,3,2, sama dengan lantai 10 (tipikal)**

Maka berat total bangunan:

$$\begin{aligned} W_t &= W_2 + W_3 + W_4 + W_5 + W_6 + W_7 + W_8 + W_9 + W_{10} + W_{\text{atap}} \\ &= 9.3895,36 + 2249,3 \\ &= 37307,54 \text{ KN} \end{aligned}$$

**b. Waktu Getar Bangunan (T)**

Dengan rumus Empiris

$$T_x = T_y = 0,06 \cdot H^{0,75}$$

$$H = 10,4 = 40 \text{ m}$$

$$T_x = T_y = 0,06 \cdot 40^{0,75} = 0,954 \text{ detik}$$

**c. Koefisien Dasar Gempa (C)**

Dengan  $T = 0,954$  detik

Respon spektrum daerah gempa 3 jenis tanah keras diperoleh nilai C sebesar  $\rightarrow C = 0,035$

**d. Faktor Keutamaan (I) dan Faktor Jenis Struktur (K)**

Berdasarkan PPTGIUG 1987 diperoleh nilai  $I = 1,0$  dan  $K = 1,0$ ; untuk struktur portal baja dengan tingkat daktilitas penuh.

**e. Gaya Geser Dasar (V)**

$$\begin{aligned} V &= C.I.K.Wt \\ &= 0,035.1.1.37307,54 \\ &= 1305.764 \text{ KN} \end{aligned}$$

**f. Distribusi Gaya Horizontal Tingkat**

$$H = 40 \text{ m}, \quad B = 30\text{m}$$

$$H/B = 40/30 = 1,33 < 3$$

Maka seluruh beban didistribusikan sebagai gaya horizontal dengan rumus:

$$F_i = \frac{W_i.F_i}{\sum W_i.F_i} \cdot V$$

Sehingga didapatkan hasil yang disajikan dalam tabel berikut :

Dengan cara yang sama maka didapatkan gaya-gaya akibat gempa untuk variasi portal yang lain yang disajikan dalam tabel berikut:

Tabel 5.3. Distribusi gaya gempa portal V-1

$$V = 1305.764\text{KN}$$

LANTAI	Wx.y KN	Hx.y M	Wx.y*Hx.y KNm	Fx.y KN	Gempa Tepi KN	Gempa Tengah KN
Atap	2,249	40	89972	148.53175	14.853	29.706
10	3,894	36	140196.96	231.44645	23.145	46.289
9	3,894	32	124619.52	205.73018	20.573	41.146
8	3,894	28	109042.08	180.01391	18.001	36.003
7	3,894	24	93464.64	154.29763	15.430	30.860
6	3,894	20	77887.2	128.58136	12.858	25.716
5	3,894	16	62309.76	102.86509	10.287	20.573
4	3,894	12	46732.32	77.148817	7.715	15.430
3	3,894	8	31154.88	51.432544	5.143	10.287
2	3,894	4	15577.44	25.716272	2.572	5.143
Σ			790956.8	1305.764		

Tabel 5.4. Distribusi gaya gempa portal V-2

V= 1319.029KN

LANTAI	Wx.y KN	Hx.y M	Wx.y*Hx.y KNm	Fx.y KN	Gempa Tepi KN	Gempa Tengah KN
Atap	2,290	40	91584.8	151.09378	15.109	30.219
10	3,933	36	141587.712	233.58704	23.359	46.717
9	3,933	32	125855.744	207.63293	20.763	41.527
8	3,933	28	110123.776	181.67881	18.168	36.336
7	3,933	24	94391.808	155.7247	15.572	31.145
6	3,933	20	78659.84	129.77058	12.977	25.954
5	3,933	16	62927.872	103.81646	10.382	20.763
4	3,933	12	47195.904	77.862348	7.786	15.572
3	3,933	8	31463.936	51.908232	5.191	10.382
2	3,933	4	15731.968	25.954116	2.595	5.191
Σ			799523.36	1319.029		

Tabel 5.5. Distribusi gaya gempa portal V-3

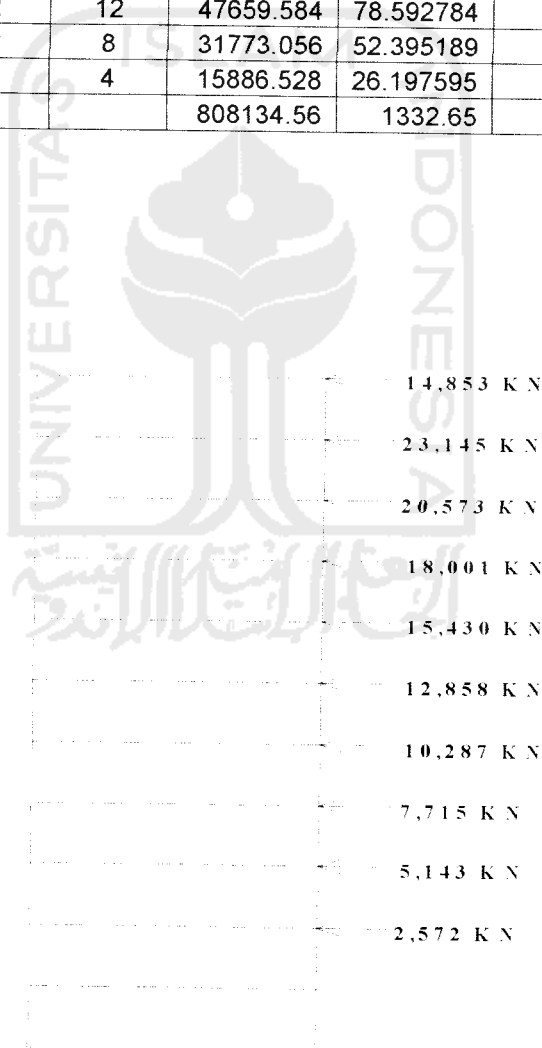
V= 1319.858KN

LANTAI	Wx.y KN	Hx.y M	Wx.y*Hx.y KNm	Fx.y KN	Gempa Tepi KN	Gempa Tengah KN
Atap	2,292	40	91685.6	151.25598	15.126	30.251
10	3,935	36	141672.384	233.7204	23.372	46.744
9	3,935	32	125931.008	207.75147	20.775	41.550
8	3,935	28	110189.632	181.78254	18.178	36.357
7	3,935	24	94448.256	155.8136	15.581	31.163
6	3,935	20	78706.88	129.84467	12.984	25.969
5	3,935	16	62965.504	103.87574	10.388	20.775
4	3,935	12	47224.128	77.906801	7.791	15.581
3	3,935	8	31482.752	51.937868	5.194	10.388
2	3,935	4	15741.376	25.968934	2.597	5.194
Σ			800047.52	1319.858		

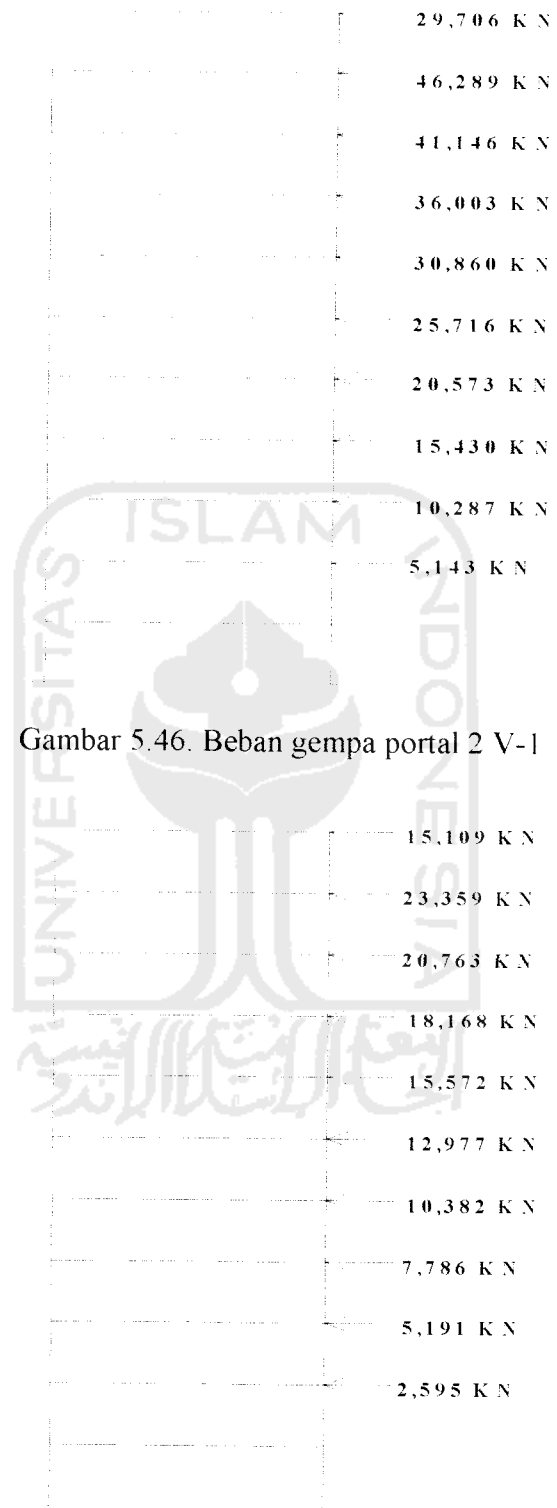
Tabel 5.6. Distribusi gaya gempa portal V-4

V= 1332.65KN

LANTAI	Wx.y KN	Hx.y M	Wx.y*Hx.y KNm	Fx.y KN	Gempa Tepi KN	Gempa Tengah KN
Atap	2,331	40	93240.8	153.75825	15.376	30.752
10	3,972	36	142978.752	235.77835	23.578	47.156
9	3,972	32	127092.224	209.58076	20.958	41.916
8	3,972	28	111205.696	183.38316	18.338	36.677
7	3,972	24	95319.168	157.18557	15.719	31.437
6	3,972	20	79432.64	130.98797	13.099	26.198
5	3,972	16	63546.112	104.79038	10.479	20.958
4	3,972	12	47659.584	78.592784	7.859	15.719
3	3,972	8	31773.056	52.395189	5.240	10.479
2	3,972	4	15886.528	26.197595	2.620	5.240
Σ			808134.56	1332.65		

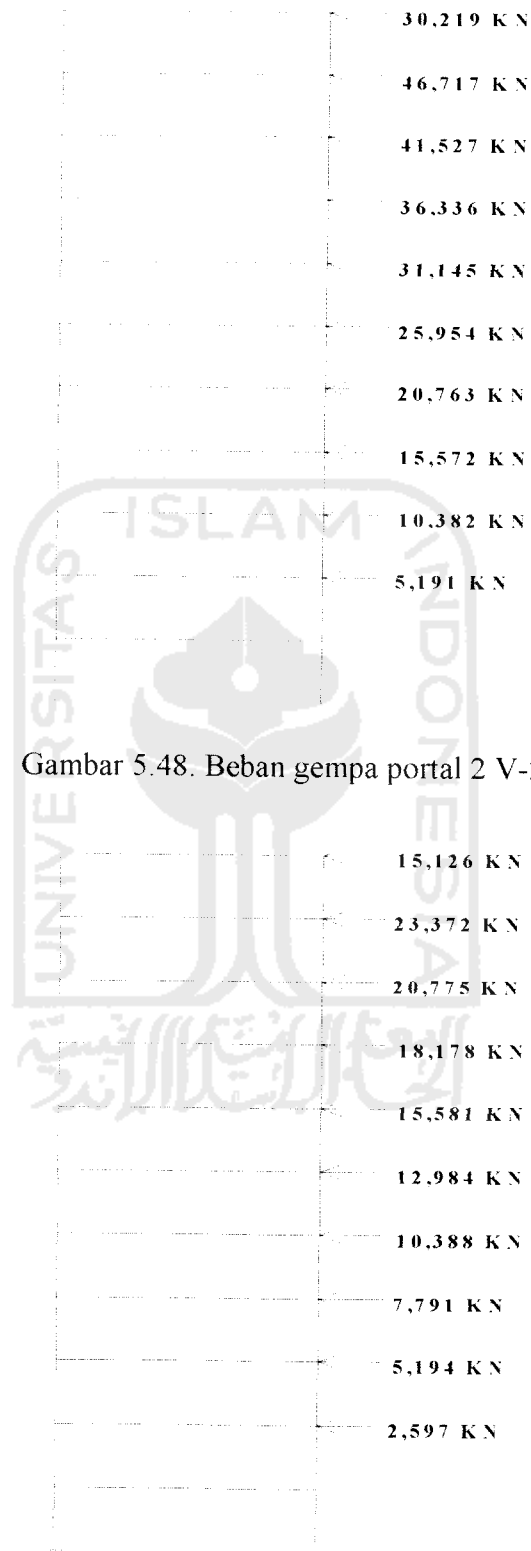


Gambar 5.45. Beban gempa portal I V-1



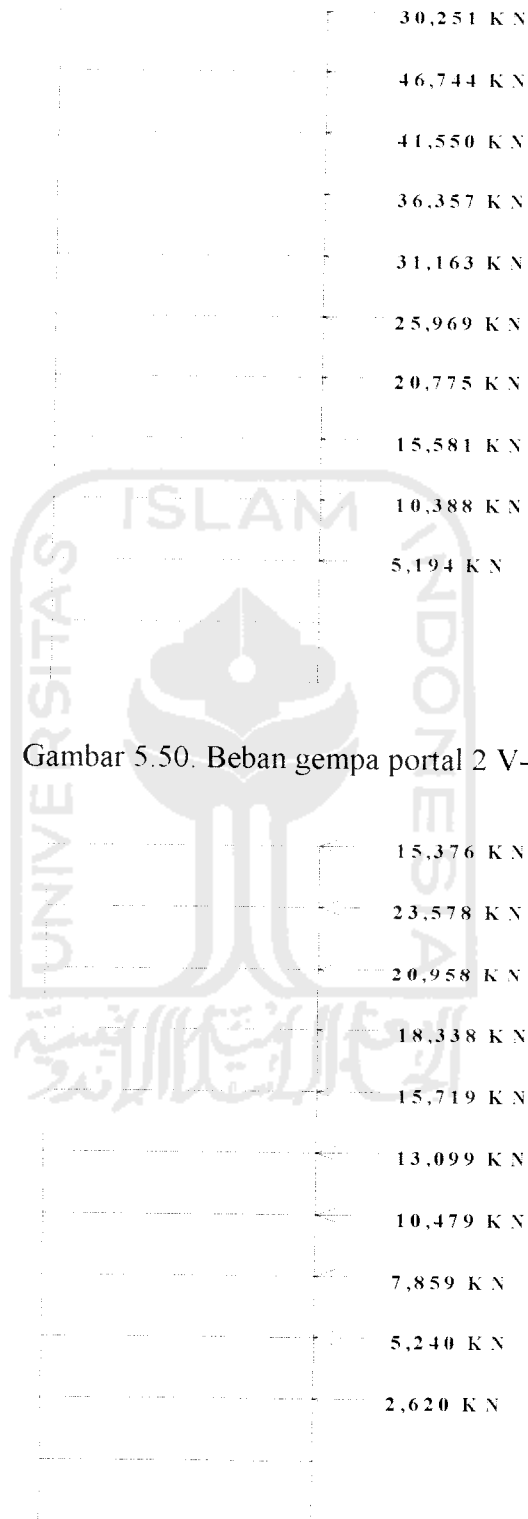
Gambar 5.46. Beban gempa portal 2 V-1

Gambar 5.47. Beban gempa portal 1 V-2

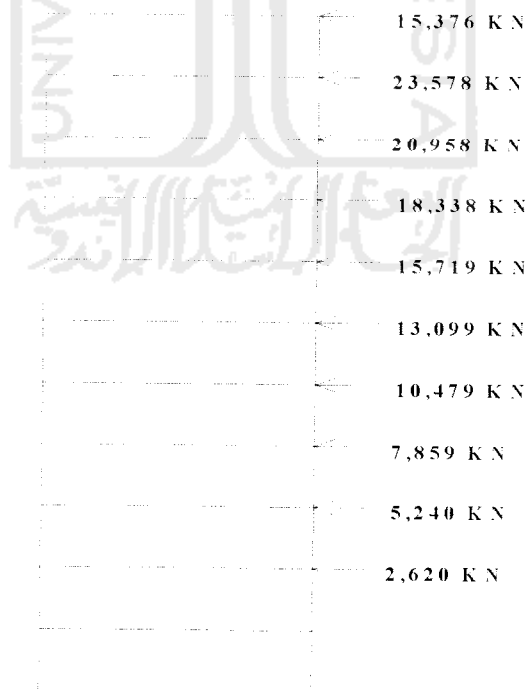


Gambar 5.48. Beban gempa portal 2 V-2

Gambar 5.49. Beban gempa portal 1 V-3

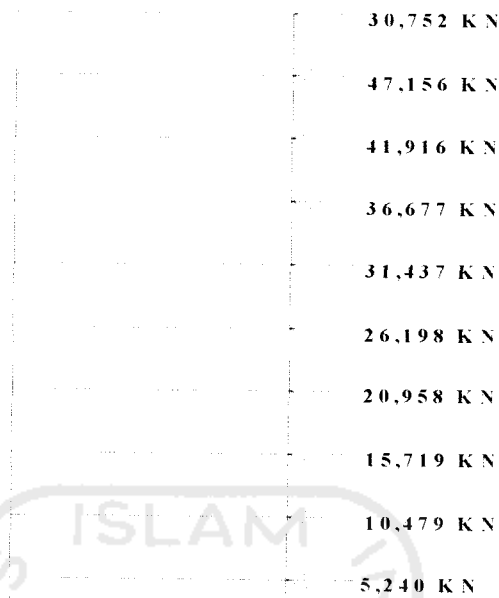


Gambar 5.50. Beban gempa portal 2 V-3



Gambar 5.51. Beban gempa portal 1 V-4





Gambar 5.52. Beban gempa portal 2 V-4

### 5.3. Perencanaan

Dalam perencanaan hanya diambil salah satu perwakilan dari beberapa elemen bangunan yang dihitung. Sedangkan data-data perencanaan diambil dari data-data analisis SAP2000 pada portal variasi 1 dengan balok anak sebagai satu kesatuan terhadap bangunan.

#### 5.3.1. Perhitungan Plat Lantai

##### Menentukan Tebal Minimum Pelat ( h )

Data-data diambil dari portal variasi 1

$$l_x = 4 \text{ m}$$

$$l_y = 6 \text{ m}$$

Pada SK SNI T- 15- 1991- 03 Pasal 3.2.5 butir 3.3 memberikan pendekatan empiris mengenai batasan defleksi dilakukan dengan tebal pelat minimum:

$$\beta = \frac{6000}{4000} = 1.5$$

Tetapi tidak boleh kurang dari :

$$h \geq \frac{ln \left( 0.8 + \frac{fy}{1500} \right)}{36 + 9\beta} = \frac{4000 \left( 0.8 + \frac{240}{1500} \right)}{36 + 9 \cdot 1,5} = 77,576 \text{ mm}$$

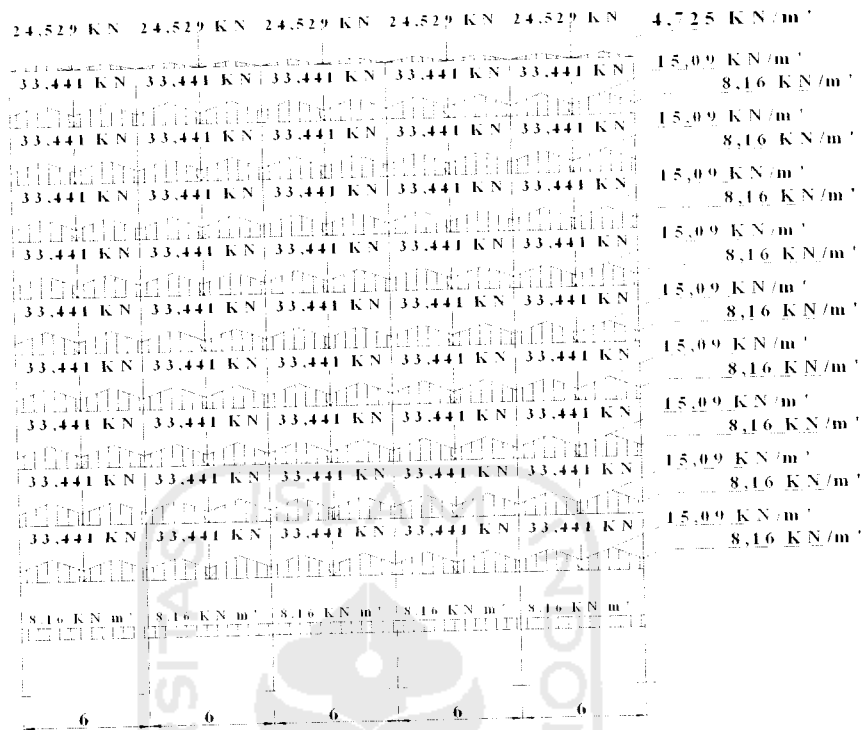
Dan tidak boleh lebih dari

$$h \leq \frac{ln \left( 0.8 + \frac{fy}{1500} \right)}{36} = \frac{4000 \left( 0.8 + \frac{240}{1500} \right)}{36} = 106,667 \text{ mm}$$

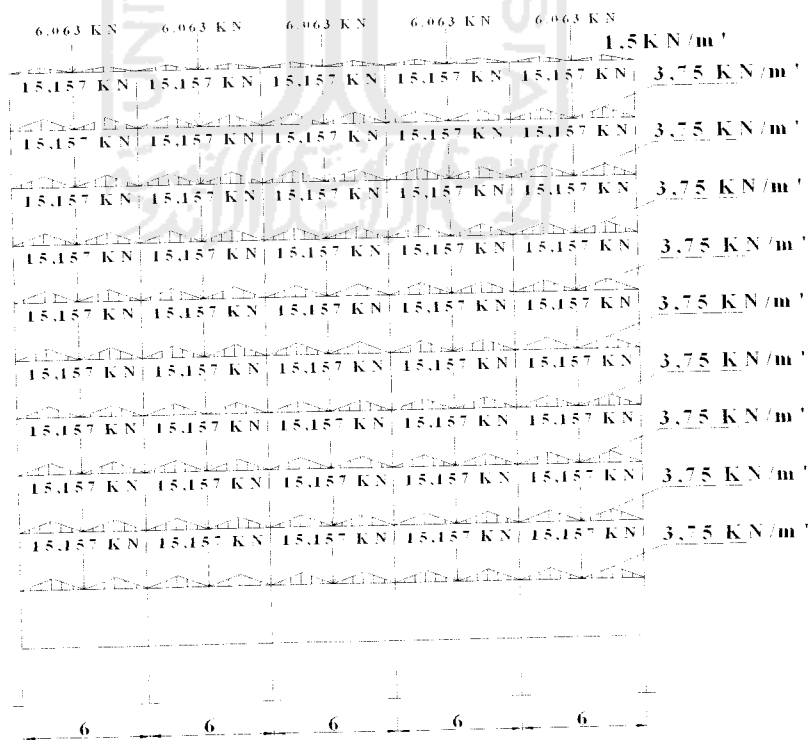
$$77,576 \text{ mm} \leq h \leq 106,667 \text{ mm} , \text{ mak dipakai } h = 120 \text{ mm}$$

Beban lantai :

Beban mati = Beton	= 0,12 m . 24 KN/m <sup>3</sup>	= 2,88 KN/m <sup>2</sup>
= Pasir	= 0,03m . 18 KN/m <sup>3</sup>	= 0,54 KN/m <sup>2</sup>
= Spesi	= 0,03 m . 21 KN/m <sup>3</sup>	= 0,63 KN/m <sup>2</sup>
= Keramik	= 0,03 m . 8 KN/m <sup>3</sup>	= 0,24 KN/m <sup>2</sup>
= dusting AC		= 0,15 KN/m <sup>2</sup>
= plafon		= 0,18 KN/m <sup>2</sup> +
	qd	= 4,62 KN/m <sup>2</sup>



Gambar 5.32. Beban mati portal A V-3



Gambar 5.33. Beban hidup portal A V-3

Ruang kuliah :

$$q_l = 2,5 \text{ KN/m}^2$$

$$q_u = 1,2 q_d + 1,6 q_l$$

$$= 1,2 \cdot 4,62 \text{ KN/m}^2 + 1,6 \cdot 2,5 \text{ KN/m}^2$$

$$= 9,16 \text{ KN/m}^2 \approx 10 \text{ KN/m}^2$$

### 5.3.2. Perencanaan Balok

#### Perhitungan Balok Induk

##### 1. Akibat beban gravitasi dan gempa

Bentang A-B

Bentang yang terjadi lengkung ganda ( double Curvature )

$$Mu_1 = 516,2388 \text{ kN.m} = 380,7778 \text{ k.ft}$$

$$Mu_2 = 345,6003 \text{ kN.m} = 254,9148 \text{ k.ft}$$

$$C_b = 1,75 + 1,05 \left( \pm \frac{M1}{M2} \right) + 0,3 \left( \frac{M1}{M2} \right)^2 \leq 2,30$$

$$C_b = 1,75 + 1,05 \left( \frac{84,3672}{380,7778} \right) + 0,3 \left( \frac{84,3672}{380,7778} \right)^2 = 2,5874 > 2,3$$

Dipakai  $C_b = 2,5874$

Coba profil 14 x 283 ;

$$r_T = 4,46 \text{ in} \quad S_x = 459 \text{ in}^3 \quad b_f = 16,11 \text{ in}$$

$$\frac{d}{A_f} = 0,5 \quad \frac{b_f}{2.t_f} = 3,9 \quad \frac{d}{t_w} = 13$$

$$L_b = 4 \text{ m} = 13,1172 \text{ ft}$$

$$L_c = \frac{76 \cdot b_f}{12 \cdot \sqrt{F_y}} = \frac{76 \cdot 16,11}{12 \cdot \sqrt{36}} = 17,005 \text{ ft}$$

$$L_c = \frac{20000}{12 \cdot \frac{d}{A_f} \cdot F_y} = \frac{20000}{12 \cdot 0,5 \cdot 36} = 92,592 \text{ ft}$$

Nilai  $L_c$  diambil yang terkecil = 17,005 ft

$$L_u = \frac{20000}{12 \cdot \frac{d}{A_f} \cdot F_y} = 92,592 \text{ ft}$$

$$L_u = \frac{r_T}{12} \sqrt{\frac{102000 \cdot C_b}{F_y}} = \frac{4,46}{12} \sqrt{\frac{102000 \cdot 2,5874}{36}} = 77,9488 \text{ ft}$$

Nilai  $L_u$  diambil yang terbesar = 92,592 ft

$$L_b = 13,1172 \text{ ft} < L_u = 92,592 \text{ ft}$$

$$L_b < L_c = 17,005 \text{ ft}$$

$$F_{bx} = 0,66 F_y = 0,6 \cdot 36 = 24 \text{ Ksi}$$

$$\text{Tegangan yang terjadi } f_b = \frac{M_u}{S_x} = \frac{380,7778}{459} = 0,829 \text{ ksi}$$

Karena terdapat beban gempa, maka nilai  $F_b$  boleh dinaikan sebesar 1/3 kali nilai

$F_b$  semula. ( AISC – ASD )

$$1,33 F_b = 1,33 \cdot 24 = 31,92 \text{ ksi} > f_b = 0,829 \rightarrow \text{Aman}$$

$$M \text{ tersedia} = 31,92 \cdot 459 = 14651,28 \text{ K.in} = 1213,45083 \text{ k.ft}$$

Dimana lendutan pada tengah bentang dapat dilihat dari program bantu analisis struktur maupun menggunakan rumus persamaan (3.5-22),

$$\begin{aligned}\Delta_{\text{pertengahan bentang}} &= \frac{5L^2}{48EI} [M_s - 0,1(M_a + M_b)] \\ &= \frac{5 \cdot 13,1172^2}{48 \cdot 29000 \cdot 1330} [1213,45083 - 0,1(380,7778 + 254,9148)] \\ &= 0,0005343\end{aligned}$$

Untuk balok yang mendukung beban lantai,

$$\begin{aligned}\frac{L}{360} &\geq \Delta_{\text{pertengahan bentang}} \\ \frac{13,1172}{360} &= 0,03644 \geq 0,0005343\end{aligned}$$

### 5.3.3. Perencanaan Kolom

Profil W 14 X 311

A	= 91,4 in <sup>2</sup>	I <sub>x</sub>	= 4330 in <sup>4</sup>	I <sub>y</sub>	= 3400 in <sup>4</sup>
d	= 17,2 in	S <sub>x</sub>	= 506 in <sup>3</sup>	S <sub>y</sub>	= 199 in <sup>3</sup>
t <sub>w</sub>	= 1,14 in	Z <sub>x</sub>	= 603 in <sup>3</sup>	Z <sub>y</sub>	= 304 in <sup>3</sup>
b <sub>f</sub>	= 16,23 in	E <sub>s</sub>	= 29000 Ksi	f <sub>u</sub>	= 58 Ksi
t <sub>f</sub>	= 2,26 in	F <sub>y</sub>	= 36 Ksi	f <sub>r</sub>	= 10 Ksi
r <sub>x</sub>	= 6,88 in	G	= 11200 Ksi	C <sub>w</sub>	= 89100 in <sup>6</sup>
r <sub>y</sub>	= 4,2 in	J	= 136 in <sup>4</sup>		

Tegangan yang terjadi

$$f_a = \frac{P}{A} = \frac{799,988}{91,4} = 8,7526 \text{ Ksi}$$

$$f_b = \frac{M}{S} = \frac{536,2 \cdot 12}{506} = 12,7162 \text{ Ksi}$$

Kelangsingan kolom

$$\frac{K.L}{r_x} \text{ atau } \frac{K.L}{r_y}$$

$$\frac{K.L}{r_x} = \frac{1,92.12.13}{6,88} = 43,5345$$

$$\frac{K.L}{r_y} = \frac{13.12}{4,2} = 37,1248$$

Kelangsingan batas

$$C_c = \sqrt{\frac{2\pi^2 E}{F_y}} = \sqrt{\frac{2\pi^2 29000}{36}} = 126 \text{ Ksi}$$

$$C_c = \frac{756}{\sqrt{F_y}} = \frac{756}{\sqrt{36}} = 126,1 \text{ Ksi}$$

$$\frac{K.L/r}{C_c} = \frac{43,5345}{126} = 0,3455$$

Angka keamanan

$$\begin{aligned} F_s &= \frac{5}{3} + \frac{3}{8} \frac{K.L/r}{C_c} - \frac{1}{8} \frac{(K.L/r)^2}{C_c^2} \\ &= \frac{5}{3} + \frac{3}{8} (0,3455) - \frac{1}{8} (0,3455)^2 \\ &= 1,791 \text{ Ksi} \end{aligned}$$

Tegangan desak aksial

$$\begin{aligned} F_a &= \frac{\left(1 - \frac{1}{2} \frac{(K.L/r)^2}{C_c^2}\right) F_y}{F_s} \\ &= 18,9 \text{ Ksi} \end{aligned}$$

Untuk menentukan  $F_a$  bisa dengan menggunakan tabel AISC hal 3 -16 ( 3.17 )

$$\frac{K.L}{r_x} = 43,5345$$

$$F_y = 36 \text{ Ksi}$$

Didapat  $F_a$  dari tabel = 18,92 Ksi

Menentukan  $F_b$  ( tegangan ijin)

Panjang batang antara pengekang lateral

$$L_b = Kl.x = 13,1172 \cdot 12 = 157,4064 \text{ ft}$$

Panjang kritis batang

$$L_c = \frac{76.bf}{12.\sqrt{F_y}} = \frac{76.16,23}{12.\sqrt{36}} = 17,1317 \text{ ft}$$

$$L_u = \frac{20000}{12.F_y \cdot d_{Af}} = \frac{20000}{12.36.0,47} = 98,5027 \text{ ft}$$

$$L_b < L_c$$

$$L_b < L_u$$

Pembesaran momen

$$\frac{f_a}{F_a} = \frac{8,7256}{18,9} = 0,4631 > 0,15$$

Maka  $F_{bx} = 0,66 \cdot F_y = 0,66 \cdot 36 = 23,76 \approx 24 \text{ Ksi}$

$$F_{by} = 0,75 \cdot f_y = 0,75 \cdot 36 = 27 \text{ Ksi}$$

$$F_{e'x} = \frac{12.\pi^2.E}{23\left(\frac{KL}{r}\right)^2} = \frac{12.\pi^2.29000}{23(43,5345)^2} = 78,8546 \text{ Ksi}$$



$$F_{e'y} = \frac{12 \cdot \pi^2 \cdot E}{23 \left( \frac{kL}{r} \right)^2} = \frac{12 \cdot \pi^2 \cdot 29000}{23(37,1248)^2} = 108,4357 \text{ Ksi}$$

$$\frac{C_{mx}}{1 - \frac{f_a}{F_{e'x}}} = \frac{0,9}{1 - \frac{8,7526}{78,846}} = 0,056 < 1$$

$$\frac{C_{my}}{1 - \frac{f_a}{F_{e'y}}} = \frac{0,9}{1 - \frac{8,7526}{108,4357}} = 0,979$$

Cek dengan persamaan interaksi

$$\frac{f_a}{F_a} + \frac{C_{mx} \cdot f_{bx}}{\left(1 - \frac{f_a}{F_{e'x}}\right) F_{bx}} + \frac{C_{my} \cdot f_{by}}{\left(1 - \frac{f_a}{F_{e'y}}\right) F_{by}} \leq 1,0$$

$$= 0,884 < 1 \text{ ok!!!}$$

$$\frac{f_a}{0,6 F_y} + \frac{f_{bx}}{F_{bx}} + \frac{f_{by}}{F_{by}} \leq 1,0$$

$$= 0,826 < 1 \text{ !!!}$$

Profil W14x311 memenuhi

#### 5.3.4. Perhitungan Balok Anak Variasi I

Menggunakan profil W16 x 36 tanpa plat rangkap:

$$A = 10,6 \text{ in}^2$$

$$I_x = 448 \text{ in}^4$$

$$S_x = 56,5 \text{ in}^3$$

$$b_f = 6,985 \text{ in}^2$$

$$n = E_s / E_c = 29000 / 3500 = 8,28 \approx 9$$

$$f'_c = 4 \text{ ksi}$$

$$F_y = 36 \text{ ksi}$$

Menentukan lebar efektif :

$$b_E = \frac{1}{4} \cdot \text{bentangan} = \frac{1}{4} \cdot 236,22 \text{ in} = 59,055 \text{ in}$$

$$b_E = \text{jarak antara balok-balok} = 4 \text{ m} = 157,48 \text{ in}$$

$$b_E = 16(4) + 6,985 = 71 \text{ in} \quad \text{Menentukan}$$

$$y_b = \frac{10,6 \left( \frac{15,86}{2} \right) + \left( \frac{71,4}{9} \right)}{10,6 + \left( \frac{71,4}{9} \right)} = 15,36 \text{ in}$$

$$I_{\text{komposit}} = 448 + 10,6 \cdot (7,43)^2 + \frac{1}{12} \cdot \frac{71}{9} \cdot (4)^3 + \frac{71 \cdot (4)}{9} (2,5)^2 = 1270 \text{ in}^4$$

$$S_{\text{tr}} = \frac{I}{y_b} = \frac{1270}{15,36} = 82,6 \text{ in}^3 \quad (\text{untuk permukaan bawah balok})$$

$$S_{\text{atas}} = \frac{I}{y} = \frac{1270}{4,5} = 282 \text{ in}^3 \quad (\text{untuk permukaan atas beton})$$

Cek tegangan:

Di serat atas plat beton :  $f_c$  yang diijinkan =  $0,45 f'_c = 1,35 \text{ Ksi}$

$$f_c = \frac{(M_{L1} + M_{L2})(12)}{(9)282} = \frac{28,97199 \cdot 12}{9 \cdot 282} = 0,136 < 1,35 \text{ ksi}$$

Diserat bawah balok baja:  $F_b = 0,66 \cdot F_y = 24 \text{ Ksi}$

$$f_b = \frac{(M_{L1} + M_{L2})(12)}{82,6} = \frac{28,97199 \cdot 12}{82,6} = 4,209 \leq 24 \text{ ksi}$$

Untuk  $S_{\text{tr}}$  maksimum yang dapat digunakan:

$$S_{\text{tr}} = \left( 1,35 + 0,35 \frac{M_{L1}}{M_D} \right) \cdot S_s$$

$$S_{tr} = \left( 1,35 + 0,35 \frac{8,06519}{20,9668} \right) \cdot 56,5 = 83,9in > 82,6in$$

Tegangan baja untuk beban yang dipikul secara tak komposit:

$$f_b = \frac{M_{Lr}}{S_s} = \frac{28,34412(12)}{56,5} = 6,019ksi < 0,6F_y$$

Alat penyambung geser:

$$V_h = \frac{0,85 \cdot f'_c \cdot A_c}{2} = \frac{0,85 \cdot (4) \cdot 71 \cdot (4)}{2} = 362kip$$

$$V_h = \frac{A_s \cdot F_y}{2} = \frac{10,6(36)}{2} = 191kip$$

Untuk stud berkepala  $2\frac{1}{2}$  in dengan diameter  $5/8$  in,  $q = 8$  kip/stud:

$$N = \frac{V_h}{q} = \frac{191}{8} = 23,8 \text{ bulatkan } 24$$

Jarak antar stud:

$$p = \frac{\frac{L}{2}}{N} = \frac{236,22}{24} = 9,8425in$$

Gunakan jarak 10 in untuk tiap penyambung stud.