

## BAB IV PERENCANAAN ATAP

Perencanaan atap meliputi, perencanaan gording, perencanaan sagrod, dan perencanaan rangka baja atap, dengan metoda LRFD 2000. Perencanaan atap disajikan dalam Gambar 4.1.

### 4.1 Perencanaan Gording

#### 4.1.1 Pembebanan Gording

Pembebanan gording terdiri dari:

a. Beban Mati ( D )

- Penutup atap genteng, reng dan usuk bidang miring :  $0,5 \text{ kN/m}^2 \times 2,197 \text{ m} = 1,099 \text{ kN/m}$

- Berat gording sendiri C 6 x 10,5 :  $= 0,153 \text{ kN/m}$  +  
 $q_D = 1,252 \text{ kN/m}$

b. Beban hidup ( L )

- Beban pekerja pada atap :  $P_L = 1 \text{ kN}$

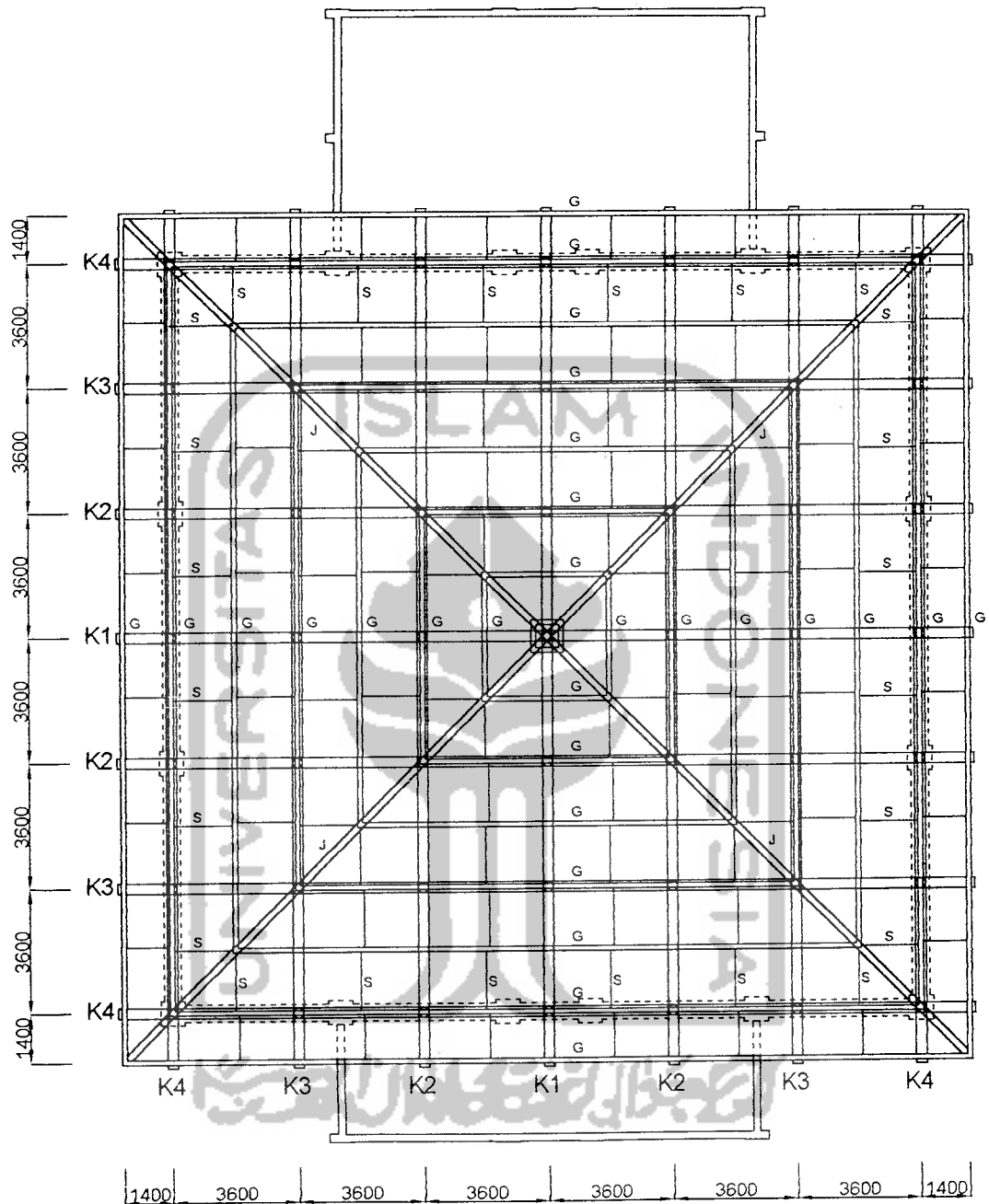
c. Beban Air Hujan ( H )

- Beban air hujan :  $q_H = ( 40 - 0,8 \cdot \alpha ) \text{ kg/m}^2 \times 2,197 \text{ m} = 26,364 \text{ kg/m}$   
 $= 0,264 \text{ kN/m}$

d. Beban Angin ( W )

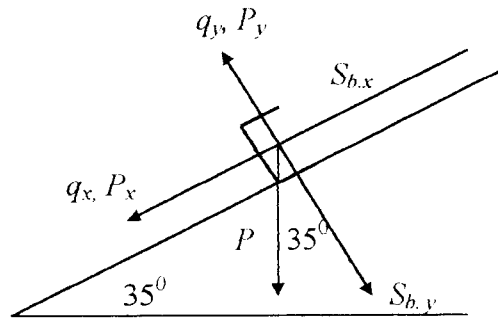
- Tiup angin :  $q_{W, \text{tiup}} = ( 0,02 \cdot \alpha - 0,4 ) \times 60 \text{ kg/m}^2 \times 2,197 \text{ m} = 39,546 \text{ kg/m}$   
 $= 0,396 \text{ kN/m}$

- Hisap angin :  $q_{W, \text{hisap}} = - 0,4 \times 60 \text{ kg/m}^2 \times 2,197 \text{ m} = - 52,728 \text{ Kg/m}$   
 $= - 0,527 \text{ KN/m}$



**Gambar 4.1** Perencanaan atap (Skala 1 : 200)

Keterangan:  
 K : Kuda-kuda  
 G : Gording  
 S : Sagrog  
 J : Jurai



**Gambar. 4.2** Arah pembebanan gording

**Tabel. 4.1** Pembebanan dan Momen Arah Sumbu x dan Sumbu y Gording

No	Jenis Pembebanan	$q_x / P_x$	$q_y / P_y$	$M_x$	$M_y$
		(1)	(2)	(3)	(4)
1	Beban Mati (D)	$q_x = 0,718$	$q_y = 1,026$	1,163	1,662
2	Beban Hidup (L)	$P_x = 0,574$	$P_y = 0,819$	0,517	0,737
3	Beban Hujan (H)	$q_x = 0,115$	$q_y = 0,164$	0,186	0,266
4	Beban Angin (W)				
	- Tiup	0	$q_y = 0,396$	0	0,641
	- Hisap	0	$q_y = -0,527$	0	-0,854

Keterangan Tabel 4.1:

(1) Pembebanan sejajar gording:  $q_x = q \cdot \sin 35^\circ$  (kN/m: untuk beban merata)

$$P_x = P \cdot \sin 35^\circ \text{ (kN: untuk beban terpusat)}$$

(2) Pembebanan tegak lurus gording:  $q_y = q \cos 35^\circ$  (kN/m: untuk beban merata)

$$P_y = P \cdot \cos 35^\circ \text{ (kN: untuk beban terpusat)}$$

(3) Momen sejajar gording:  $M_x = 1/8 \cdot q_x \cdot L^2$  (kNm: untuk beban merata)

$$M_x = 1/4 \cdot P_x \cdot L \text{ (kNm: untuk beban terpusat)}$$

(4) Momen tegak lurus gording:  $M_y = 1/8 \cdot q_y \cdot L^2$  (kNm: untuk beban merata)

$$M_y = 1/4 \cdot P_y \cdot L \text{ (kNm: untuk beban terpusat)}$$

dengan :  $L = 3,6 \text{ m}$



**Tabel. 4.2** Kombinasi Pembebanan LRFD

No.	Kombinasi	$M_{u,x}$ (kNm)	$M_{u,y}$ (kNm)
1	$1,4 M_D$	1,628	2,327
2	$1,2 M_D + 0,5 M_L$	1,654	2,363
2	$1,2 M_D + 0,5 M_{H1}$	1,490	2,127
3	$1,2 M_D + 1,6 M_L + 0,8 M_{W, \text{tump}}$	<b>2,223</b>	<b>3,686</b>
4	$1,2 M_D + 1,6 M_L + 0,8 M_{W, \text{hisap}}$	2,223	2,490
5	$1,2 M_D + 1,3 M_{W, \text{tump}} + 0,5 M_L$	1,654	3,196
6	$1,2 M_D + 1,3 M_{W, \text{hisap}} + 0,5 M_L$	1,654	1,474

#### 4.1.2 Pendimensionian Gording

##### a. Tinjauan searah sumbu x ( sejajar gording )

$M_{u,x} = 2,223$  kNm (kombinasi maksimum)

Diambil mutu baja  $f_y = 240$  MPa, asumsi penampang kompak

Kekuatan desainnya adalah :  $\phi_b Z_x f_y \geq M_{u,x}$

$$Z_x \text{ ( yang diminta )} = \frac{M_{u,x}}{\phi_b f_y} = \frac{2,223 \cdot 10^6}{0,9 \cdot 240} = 10291,67 \text{ mm}^3 = 0,628 \text{ in}^3$$

Pilih profil dari tabel LRFD

coba C 6 x 10,5  $Z_x = 1,15 \text{ in}^3 = 18845,12 \text{ mm}^3 > 10291,67 \text{ mm}^3$  - aman -

Cek batas penampang kompak untuk C Shape

- Untuk sayap

$$\lambda = \frac{b_f}{t_f} = \frac{51,6636}{8,7122} = 5,93 < \lambda_p = \frac{170}{\sqrt{f_y}} = \frac{170}{\sqrt{240}} = 10,97 \text{ - aman -}$$

- Untuk badan

$$\lambda = \frac{h_c}{t_w} = \frac{111,125}{7,9756} = 13,93 < \lambda_p = \frac{1680}{\sqrt{f_y}} = \frac{1680}{\sqrt{240}} = 108,44 \text{ -aman-}$$

##### b. Tinjauan searah sumbu y (tegak lurus gording)

$M_{u,y} = 3,686$  kNm ( kombinasi pembebanan maksimum)

Kekuatan desainnya adalah:  $\phi_b Z_x f_y \geq M_{u,y}$

$$Z_x \text{ ( yang diminta )} = \frac{M_{u,y}}{\phi_b f_y} = \frac{3,686 \cdot 10^6}{0,9 \cdot 240} = 17064,81 \text{ mm}^3$$

$Z_x$  profil =  $100780,44 \text{ mm}^3 > 17064,81 \text{ mm}^3$  - Ok -

**c. Cek lendutan sejajar gording**

Cek lendutan sejajar gording:

- $q_x = 1,2.qD_x + 1,6.qL_x = 1,2.0,718 + 1,6.0 = 0,862 \text{ kN/m}$  (kombinasi maks.)
- $P_x = 1,2.PD_x + 1,6.PL_x = 1,2.0 + 1,6.0,574 \text{ kN} = 0,918 \text{ kN}$  (kombinasi maks)
- Panjang gording  $L = 3600 \text{ mm}$
- $E = 200.000 \text{ MPa}$
- $I_y = 0,866 \text{ in}^4 = 360456,4 \text{ mm}^4$

$$\begin{aligned} \Delta_x &= \frac{5.q_x.L^4}{384.E.I_y} + \frac{P_x.L^3}{48.E.I_y} \\ &= \frac{5.0,862.3600^4}{384.200000.360456,4} + \frac{0,918.10^3.3600^3}{48.200000.360456,4} \\ &= 26,15 + 12,37 \\ &= 38,52 \text{ mm} > L/360 = 3600/360 = 10 \text{ mm} \quad \text{- tidak aman -} \end{aligned}$$

- Perlu dipasang sagrod pada tengah bentang gording sehingga  
 $L = 3600/2 = 1800 \text{ mm}$
- Cek kembali Lendutan sejajar gording

$$\begin{aligned} \Delta_x &= \frac{5.q_x.L^4}{384.E.I_y} + \frac{P_x.L^3}{48.E.I_y} \\ &= \frac{5.0,862.1800^4}{384.200000.360456,41} + \frac{0,918.10^3.1800^3}{48.200000.360456,41} \\ &= 1,63 + 1,55 \\ &= 3,18 \text{ mm} < L/360 = 1800/360 = 5 \text{ mm} \quad \text{- aman -} \end{aligned}$$

Cek lendutan tegak lurus gording

- $q_y = 1,2q.D_y + 1,6q.L_y + 0,8.qW_{y,tutup} = 1,2.1,026 + 1,6.0 + 0,8.0,396$   
 $= 1,548 \text{ kN/m}$  (kombinasi maks.)
- $P_y = 1,2.PD_y + 1,6.PL_y + 0,8.PW_{y,tutup} = 1,2.0 + 1,6.0,819 + 0,8.0$   
 $= 1,310 \text{ kN}$  (kombinasi maks.)
- Panjang gording  $L = 3600 \text{ mm}$
- $E = 200.000 \text{ MPa}$
- $I_x = 15,2 \text{ in}^4 = 6326717,67 \text{ mm}^4$

$$\begin{aligned} \Delta_y &= \frac{5.q_y.L^4}{384.E.I_x} + \frac{P_y.L^3}{48.E.I_x} \\ &= \frac{5.1,548.3600^4}{384.200000.6326717,67} + \frac{1,310.10^3.3600^3}{48.200000.6326717,67} \end{aligned}$$

$$= 2,673 + 1,053$$

$$= 3,726 \text{ mm} < l/360 = 3600/360 = 10 \text{ mm} \quad \text{- aman -}$$

Profil C 6 x 10,5 dapat dipakai dengan memasang sagrod ditengah bentang gording

## 4.2 Perencanaan Sagrod

### 4.2.1 Pembebanan Sagrod

#### a. Beban Mati ( D )

$$\text{-Beban penutup atap} : 0,5 \text{ kN/m}^2 \times 13,184 \text{ m} \times 3,6 \text{ m} = 23,73 \text{ kN}$$

$$\text{- Beban gording} : 0,153 \text{ kN/m}^2 \times 3,6 \text{ m} \times 6 \text{ m} = 3,31 \text{ kN}$$

$$\text{- Beban sagrod taksiran} : 0,05 \text{ kN/m}^2 \times 13,118 \text{ m} = 0,66 \text{ kN} +$$

$$P_D = 27,70 \text{ kN}$$

#### b. Beban Hidup ( L )

$$\text{- Beban pekerja} : P_L = 1 \text{ kN} \times 6 \text{ pekerja tiap gording} = 6 \text{ kN}$$

#### d. Beban Hujan ( H )

$$\text{- Beban hujan: } P_H = 0,264 \text{ kN/m}^2 \times 13,184 \text{ m} \times 3,6 \text{ m} = 9,4925 \text{ kN}$$

Kombinasi pembebanan terbesar

$$N_u = 1,2 P_D + 1,6 P_L + 0,5 P_H$$

$$= 1,2 \cdot 27,7004 + 1,6 \cdot 6 + 0,5 \cdot 9,4925$$

$$= 47,5867 \text{ kN}$$

$$N_{u,x} = 47,5867 \cdot \sin 35^\circ = 27,2946 \text{ kN}$$

### 4.2.2 Pendimensionian Sagrod

$$N_u \leq \phi N_n$$

$$N_u \leq 0,90 \cdot A_g \cdot f_y$$

$$A_g = \frac{N_{u,x}}{0,9 \cdot f_y} = \frac{27,2946 \cdot 10^3}{0,9 \cdot 240} = 226,36 \text{ mm}^2$$

$$A_g = \frac{1}{4} \pi D^2$$

$$126,36 = \frac{1}{4} \cdot \pi D^2$$

$$D = 12,68 \text{ mm} , \text{ diambil } D = 16,93 \text{ mm} = 2/3 \text{ inch}$$

$$A_g \text{ profil} = \frac{1}{4} \cdot \pi \cdot 16,93^2 = 225,115 \text{ mm}^2 > 126,36 \text{ mm}^2 \quad \text{- aman -}$$

$$\begin{aligned} \text{berat sendiri} &= 78,5 \text{ kN/m}^3 \times 225,115 \cdot 10^{-6} \text{ m}^2 \\ &= 0,022 \text{ kN/m} < \text{berat taksiran} = 0,05 \text{ kN/m} \text{ --aman--} \end{aligned}$$

### 4.3 Perencanaan Kuda-Kuda Rangka Baja

Perencanaan kuda-kuda rangka baja meliputi, pembebanan kuda-kuda, analisis struktur, gaya batang rencana, pendimensian, dan perencanaan sambungan titik buhul. Jenis kuda-kuda yang direncanakan disajikan dalam Gambar 4.3 s/d Gambar 4.6.

#### 4.3.1 Perencanaan Pembebanan Kuda-Kuda

##### 1. Perencanaan Berat Sendiri Kuda-Kuda

Profil rangka baja di rencanakan terlebih dahulu untuk mendapatkan berat sendiri, disajikan pada Tabel 4.3 berikut ini.

**Tabel 4.3** Berat Sendiri Profil Rangka Baja Kuda-Kuda

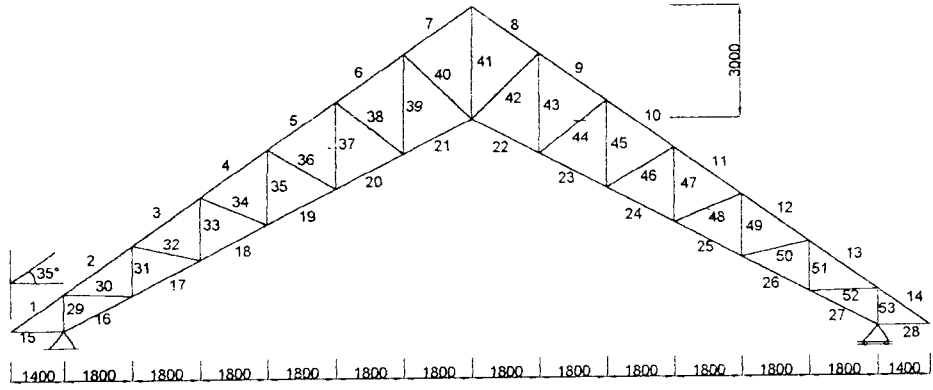
Nama Batang	Profil	Berat ( $q$ ) (kN/m)
Batang atas (a)	2.80.80.8	0,1932
Batang bawah (b)	2.70.70.7	0,1476
Batang diagonal (d)	2.60.60.6	0,1084
Batang pertemuan (vp)	O $d = 3''$ , $t = 4 \text{ mm}$	0,0713
Batang vertikal (v)	2.50.50.5	0,0754

##### a. Perencanaan Beban sendiri Kuda-Kuda K1

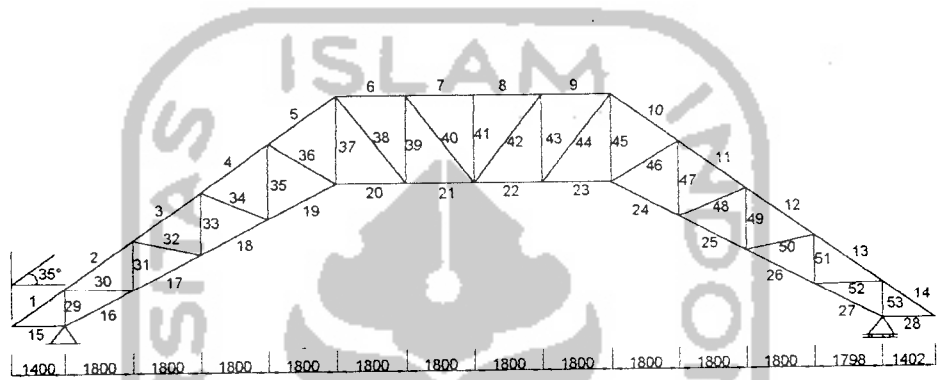
Beban sendiri kuda-kuda K1 disajikan pada Tabel 4.4 berikut ini.

**Tabel 4.4** Beban Sendiri Total Kuda-Kuda K1

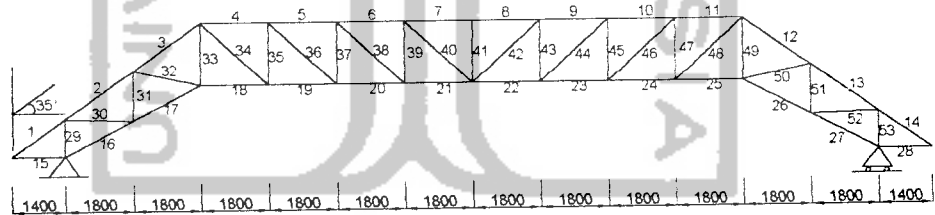
Nama Batang	( $L$ ) Panjang (m)	$P = q \times L$ (kN)
Atas (a)	29,782	5,75
Bawah (b)	27,076	4,00
Diagonal (d)	24,924	2,70
Vertikal (v)	11,94	0,90
Vertikal pertemuan (vp)	12,918	0,92
	$P \text{ total} =$	14,27 kN



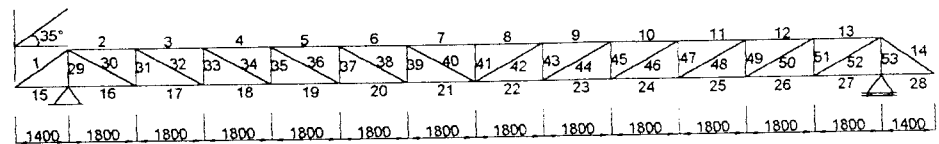
Gambar 4.3 Perencanaan Kuda-Kuda Rangka Baja K1



Gambar 4.4 Perencanaan Kuda-Kuda Rangka Baja K2



Gambar 4.5 Perencanaan Kuda-Kuda Rangka Baja K3



Gambar 4.6 Perencanaan Kuda-Kuda Rangka Baja K4



$$P_{\text{profil+plat buhul}} = 14,27 \times 1,25 = 17,84 \text{ kN}$$

- Beban titik masing-masing joint oleh berat sendiri

$$Pk1 = 17,84/15 = 1,19 \text{ kN}$$

- $P_{\text{jurai}} = (L \times q) \cdot 1,25 = 1,25(6,2152 \times 0,1502) = 0,94 \text{ kN}$

- $P'k1 = Pk1 + P_{\text{jurai}} = 1,19 + 1,18 = 2,37 \text{ kN}$

#### b. Perencanaan Beban Sendiri Kuda-Kuda K2

Beban sendiri kuda-kuda K2 disajikan pada Tabel 4.5, berikut ini

**Tabel 4.5** Beban Sendiri Total Kuda-Kuda K2

Nama Batang	(L) Panjang (m)	$P = q \times L$ (kN)
Atas (a)	28,194	5,45
Bawah (b)	26,184	3,85
Diagonal (d)	27,118	2,94
Vertikal (v)	11,266	0,85
Vertikal pertemuan (vp)	12,244	0,87
	$P_{\text{total}} =$	13,96 kN

$$P_{\text{profil+plat buhul}} = 13,96 \times 1,25 = 17,45 \text{ kN}$$

- Beban titik masing-masing joint oleh berat sendiri

$$Pk1 = 17,45/15 = 1,16 \text{ kN}$$

- $P_{\text{jurai}} = (L \times q) \cdot 1,25 = 1,25(6,2152 \times 0,1502) = 1,18 \text{ kN}$

- $P'k1 = Pk1 + P_{\text{jurai}} = 1,16 + 1,18 = 2,34 \text{ kN}$

c. Perencanaan Beban Sendiri Kuda-Kuda K3

Beban sendiri kuda-kuda K3 disajikan pada Tabel 4.6 berikut ini.

**Tabel 4.6** Beban Sendiri Total Kuda-Kuda K3

Nama Batang	(L) Panjang (m)	$P = q \times L$ (kN)
Atas (a)	26,606	5,14
Bawah (b)	25,292	3,73
Diagonal (d)	26,838	2,91
Vertikal (v)	9,246	0,70
Vertikal pertemuan (vp)	10,225	0,73
	$P \text{ total} =$	13,21 kN

$$P_{\text{profil+plat buhul}} = 13,21 \times 1,25 = 16,51 \text{ kN}$$

- Beban titik masing-masing joint oleh berat sendiri

$$Pk1 = 16,51/15 = 1,10 \text{ kN}$$

-  $P_{\text{jurai}} = (L \times q) \cdot 1,25 = 1,25(6,2152 \times 0,1502) = 1,18 \text{ kN}$

-  $P'k1 = Pk1 + P_{\text{jurai}} = 1,10 + 1,18 = 2,28 \text{ kN}$

d. Perencanaan Beban Sendiri Kuda-Kuda K4

Beban sendiri kuda-kuda K4 disajikan pada Tabel 4.7 berikut ini

**Tabel 4.7** Beban Sendiri Total Kuda-Kuda K4

Nama Batang	(L) Panjang (m)	$P = q \times L$ (kN)
Atas (a)	25,018	4,83
Bawah (b)	24,4	3,60
Diagonal (d)	24,588	2,67
Vertikal (v)	5,88	0,44
Vertikal pertemuan (vp)	6,86	0,49
	$P \text{ total} =$	12,03 kN

$$P_{\text{profil+plat buhul}} = 12,03 \times 1,25 = 15,04 \text{ kN}$$

- Beban titik masing-masing joint oleh berat sendiri

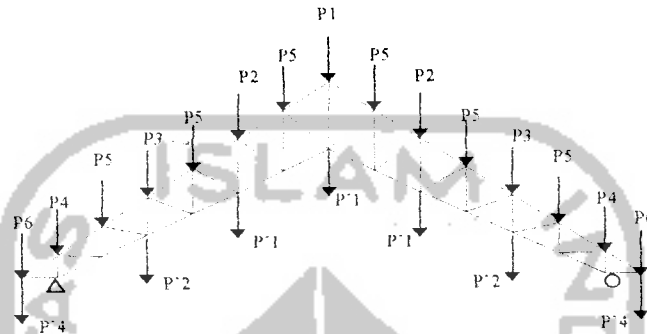
$$Pk1 = 15,04/15 = 1,0 \text{ kN}$$

-  $P_{\text{jurai}} = (L \times q) \cdot 1,25 = 1,25(5,5246 \times 0,1502) = 1,04 \text{ kN}$

$$- P'k1 = Pk1 + P_{\text{jurai}} = 1,0 + 1,04 = 1,04 \text{ kN}$$

## 2. Perencanaan Beban Mati Kuda-Kuda

### a. Perencanaan Beban Mati Kuda-Kuda K1



Gambar 4.7 Perencanaan beban mati kuda-kuda K1

#### 1. Beban titik $P1$

- Berat sendiri:  $2 \cdot P'K1 = 2 \cdot 2,37 = 4,74 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot (2,197 \cdot 3,6) / 2 = 1,98 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = 0,121 \text{ kN} +$   
 $P1 = 7,531 \text{ kN}$

#### 2. Beban titik $P2$

- Berat sendiri:  $PK1 + PK2 = 1,19 + 1,16 = 2,35 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = 0,121 \text{ kN} +$   
 $P2 = 7,111 \text{ kN}$

#### 3. Beban titik $P3$

- Berat sendiri:  $PK1 + PK3 = 1,19 + 1,10 = 2,29 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = 0,121 \text{ kN} +$

$$P3 = 7,051 \text{ kN}$$

4. Beban titik  $P4$

- Berat sendiri:  $PK1 + PK4 = 1,19 + 1,00 = 2,19 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +
- $$P4 = 6,884 \text{ kN}$$

5. Beban titik  $P5$

- Berat sendiri:  $PK1 = 1,19 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121 \text{ kN}}$  +
- $$P5 = 5,951 \text{ kN}$$

6. Beban titik  $P6$

- Berat sendiri:  $PK1 = 1,19 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 1,099 \cdot 3,6 = 1,99 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 0,855 \cdot 2 \cdot 1,25 = \underline{0,047 \text{ kN}}$  +
- $$P6 = 3,917 \text{ kN}$$

7. Beban titik  $P'1$

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 3,6 = 1,426 \text{ kN}$
  - Penggantung baja ( $d = 3/4''$ ) =  $0,022 \times 5,541 = \underline{0,122 \text{ kN}}$  +
- $$P'1 = 1,548 \text{ kN}$$

8. Beban titik  $P'2$

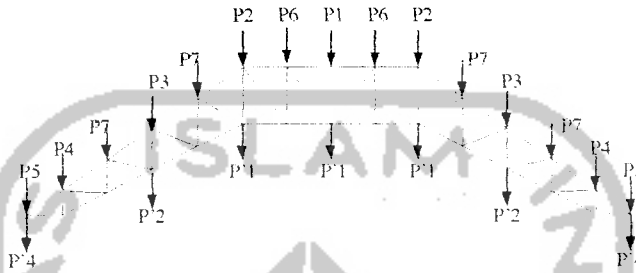
- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 5,4 = 2,138 \text{ kN}$
  - Penggantung baja ( $d = 3/4''$ ) =  $0,022 \times 1,848 = \underline{0,041 \text{ kN}}$  +
- $$P'2 = 2,179 \text{ kN}$$

9. Beban titik  $P'4$

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 1,8 = 0,713 \text{ kN}$

- Penggantungan baja ( $d=3/4''$ ) =  $0,022 \times 0 = \underline{0,000 \text{ kN}}$  +  
 $P'4 = 0,713 \text{ kN}$

#### b. Perencanaan Beban Mati Kuda-Kuda K2



Gambar. 4.8 Perencanaan pembebanan mati kuda-kuda K2

1. Beban titik  $P1$ 
  - Berat sendiri:  $PK1 + PK2 = 1,19 + 1,16 = 2,35 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121 \text{ kN}}$  +  
 $P1 = 7,111 \text{ kN}$
2. Beban titik  $P2$ 
  - Berat sendiri:  $2 \cdot P'K2 = 2 \cdot 2,34 = 4,68 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121 \text{ kN}}$  +  
 $P2 = 9,441 \text{ kN}$
3. Beban titik  $P3$ 
  - Berat sendiri:  $PK2 + PK3 = 1,16 + 1,10 = 2,26 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121 \text{ kN}}$  +  
 $P3 = 7,021 \text{ kN}$

4. Beban titik  $P_4$ 

- Berat sendiri:  $PK_2 + PK_4 = 1,16 + 1,00 = 2,16$  kN
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95$  kN
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69$  kN
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054}$  kN +
- $$P_4 = 6,424 \text{ kN}$$

5. Beban titik  $P_5$ 

- Berat sendiri:  $PK_2 = 1,16$  kN
  - Berat penutup atap:  $0,5 \cdot 1,099 \cdot 3,6 = 1,99$  kN
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69$  kN
  - Berat sagrod:  $0,022 \cdot 0,855 \cdot 2 \cdot 1,25 = \underline{0,047}$  kN +
- $$P_5 = 4,289 \text{ kN}$$

6. Beban titik  $P_6$ 

- Berat sendiri:  $PK_2 = 1,16$  kN
- $$P_6 = 1,16 \text{ kN}$$

7. Beban titik  $P_7$ 

- Berat sendiri:  $PK_2 = 1,16$  kN
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95$  kN
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69$  kN
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121}$  kN +
- $$P_7 = 5,921 \text{ kN}$$

8. Beban titik  $P'1$ 

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 3,6 = 1,426$  kN
  - Penggantung baja ( $d=3/4''$ ) =  $0,022 \times 5,541 = \underline{0,122}$  kN +
- $$P'1 = 1,548 \text{ kN}$$

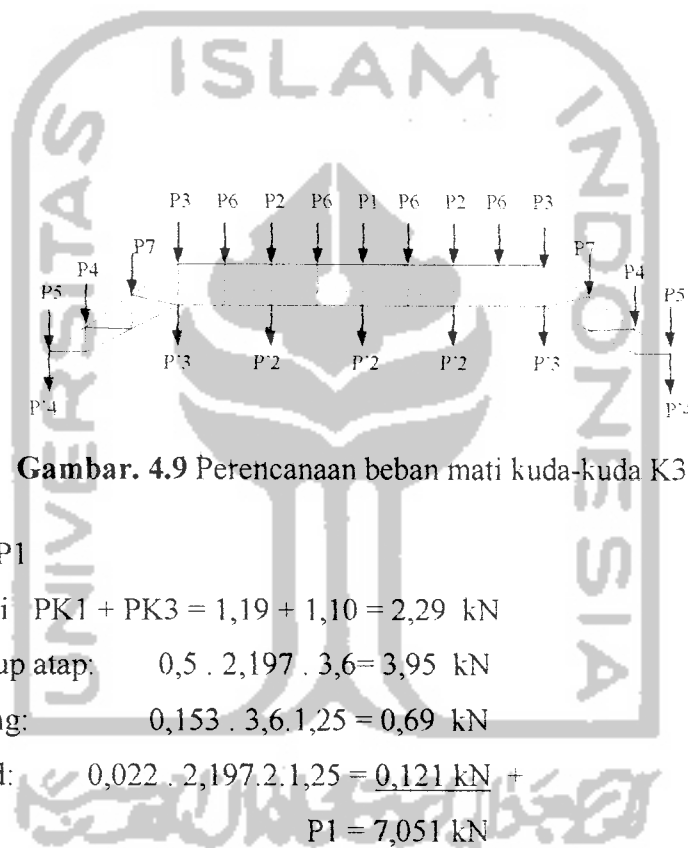
9. Beban titik  $P'2$ 

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 5,4 = 2,138$  kN
  - Penggantung baja ( $d=3/4''$ ) =  $0,022 \times 1,848 = \underline{0,041}$  kN +
- $$P'2 = 2,179 \text{ kN}$$

## 10. Beban titik P'4

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 1,8 = 0,713 \text{ kN}$
- Penggantung baja ( $d=3/4''$ ) =  $0,022 \times 0 = 0,000 \text{ kN} +$   
 $P'4 = 0,713 \text{ kN}$

## c. Perencanaan Beban Mati Kuda-Kuda K3



Gambar. 4.9 Perencanaan beban mati kuda-kuda K3

## 1. Beban titik P1

- Berat sendiri:  $PK1 + PK3 = 1,19 + 1,10 = 2,29 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2,1,25 = 0,121 \text{ kN} +$   
 $P1 = 7,051 \text{ kN}$

## 2. Beban titik P2

- Berat sendiri:  $PK2 + PK3 = 1,16 + 1,1 = 2,26 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2,1,25 = 0,121 \text{ kN} +$   
 $P2 = 7,021 \text{ kN}$

## 3. Beban titik P3

- Berat sendiri:  $2 \cdot P'K3 = 2 \cdot 2,28 = 4,56 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$

- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121 \text{ kN}}$  +  
 $P3 = 9,321 \text{ kN}$
4. Beban titik P4
- Berat sendiri:  $PK3 + PK4 = 1,1 + 1,00 = 2,1 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +  
 $P4 = 6,364 \text{ kN}$
5. Beban titik P5
- Berat sendiri:  $PK3 = 1,1 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 1,099 \cdot 3,6 = 1,99 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 0,855 \cdot 2 \cdot 1,25 = \underline{0,047 \text{ kN}}$  +  
 $P5 = 4,229 \text{ kN}$
6. Beban titik P6
- Berat sendiri:  $PK3 = 1,1 \text{ kN}$   
 $P6 = 1,1 \text{ kN}$
7. Beban titik P7
- Berat sendiri:  $PK3 = 1,1 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121 \text{ kN}}$  +  
 $P5 = 5,861 \text{ kN}$
8. Beban titik P'2
- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 5,4 = 2,138 \text{ kN}$
  - Penggantung baja ( $d = 3/4''$ )  $= 0,022 \times 1,848 = \underline{0,041 \text{ kN}}$  +  
 $P'2 = 2,179 \text{ kN}$



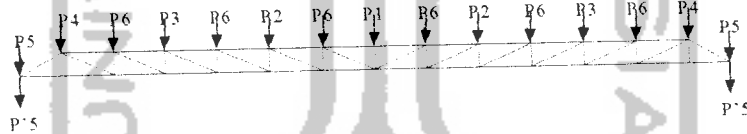
## 9. Beban titik P'3

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 5,4 \times 5,4 = 3,2076 \text{ kN}$
- Penggantung baja (d = 3/4") =  $0,022 \times 1,848 = \underline{0,041 \text{ kN}}$  +  
 $P'3 = 3,2486 \text{ kN}$

## 10. Beban titik P'4

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 1,8 = 0,713 \text{ kN}$
- Penggantung baja (d = 3/4") =  $0,022 \times 0 = \underline{0,000 \text{ kN}}$  +  
 $P'4 = 0,713 \text{ kN}$

## d. Perencanaan Beban Mati Kuda-Kuda K4



Gambar. 4.10 Perencanaan pembebanan mati kuda-kuda K4

## 1. Beban titik P1

- Berat sendiri  $PK1 + PK4 = 1,19 + 1,0 = 2,29 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +  
 $P1 = 6,454 \text{ kN}$

## 2. Beban titik P2

- Berat sendiri:  $PK2 + PK4 = 1,16 + 1,0 = 2,16 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +

$$P2 = 6,424 \text{ kN}$$

3. Beban titik P3

- Berat sendiri:  $PK3 + PK4 = 1,1 + 1,0 = 2,1 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +
- $$P3 = 6,364 \text{ kN}$$

4. Beban titik P4

- Berat sendiri:  $2 \cdot PK4 = 2 \cdot 2,04 = 4,08 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +
- $$P4 = 8,344 \text{ kN}$$

5. Beban titik P5

- Berat sendiri:  $PK4 = 1,0 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,047 \text{ kN}}$  +
- $$P5 = 5,687 \text{ kN}$$

6. Beban titik P6

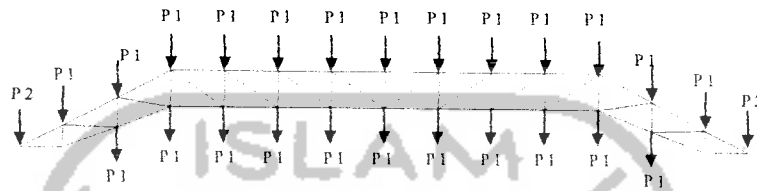
- Berat sendiri:  $PK4 = 1,0 \text{ kN}$

$$P6 = 1,0 \text{ kN}$$

7. Beban titik P'5

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 4,86 = 0,5346 \text{ kN}$
  - Penggantung baja ( $d = 3/4''$ ) =  $0,022 \times 0 = \underline{0,000 \text{ kN}}$  +
- $$P'5 = 0,5346 \text{ kN}$$

**c. Perencanaan Beban Hidup Kuda-Kuda K3**

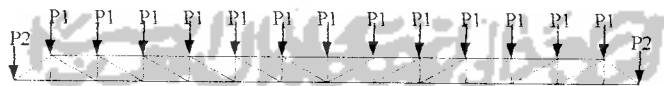


**Gambar. 4.13** Perencanaan beban hidup kuda-kuda K3

Beban hidup:  $P1 = 1 \text{ kN}$

$P2 = 2 \text{ kN}$

**d. Perencanaan beban hidup kuda-kuda K4**



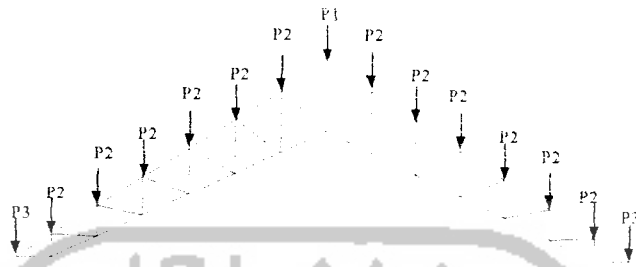
**Gambar. 4.14** Perencanaan beban hidup kuda-kuda K4

Beban hidup:  $P1 = 1 \text{ kN}$

$P2 = 2 \text{ kN}$

#### 4. Perencanaan Beban Air Hujan Kuda-Kuda

##### a. Perencanaan beban air hujan kuda-kuda K1

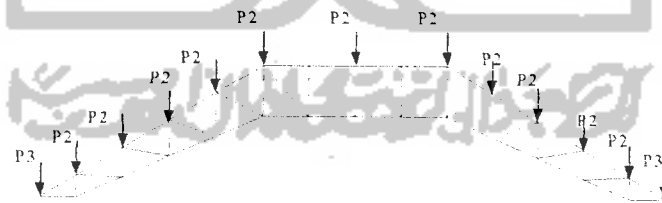


Gambar. 4.15 Perencanaan beban air hujan kuda-kuda K1

Beban air hujan :

- $P1 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6 : 2) = 0,48 \text{ kN}$
- $P2 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8 \cdot 35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

##### b. Perencanaan beban air hujan kuda-kuda K2

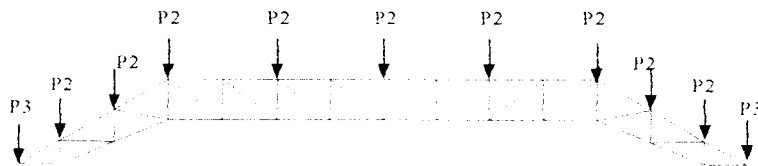


Gambar. 4.16 Perencanaan beban air hujan kuda-kuda K2

Beban air hujan :

- $P2 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8 \cdot 35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

### c. Perencanaan beban air hujan kuda-kuda K3

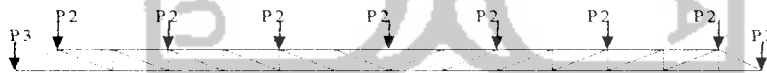


**Gambar. 4.17** Perencanaan beban air hujan kuda-kuda K3

Beban air hujan :

- $P2 = 0,01 \times (40 - 0,8.35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8.35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

### d. Perencanaan beban air hujan kuda-kuda K4



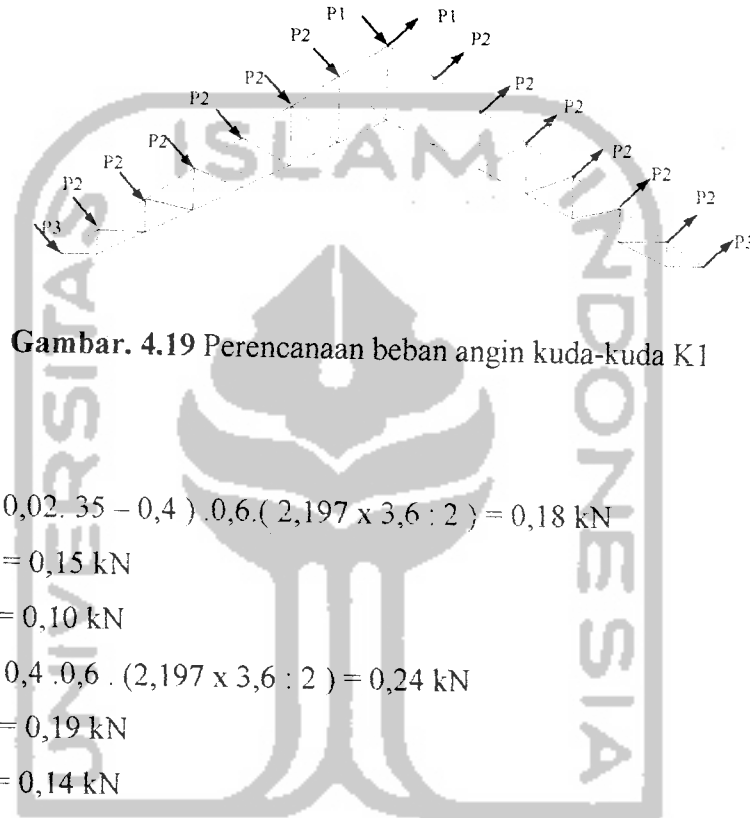
**Gambar. 4.18** Perencanaan beban air hujan kuda-kuda K4

Beban air hujan :

- $P1 = 0,01 \times (40 - 0,8.35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8.35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

## 5. Perencanaan Beban Angin Kuda-Kuda

### a. Perencanaan beban angin kuda-kuda K1



Gambar. 4.19 Perencanaan beban angin kuda-kuda K1

Beban Angin:

- P1

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6 : 2) = 0,18 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,15 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,10 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6 : 2) = 0,24 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,19 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,14 \text{ kN}$$

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = 1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

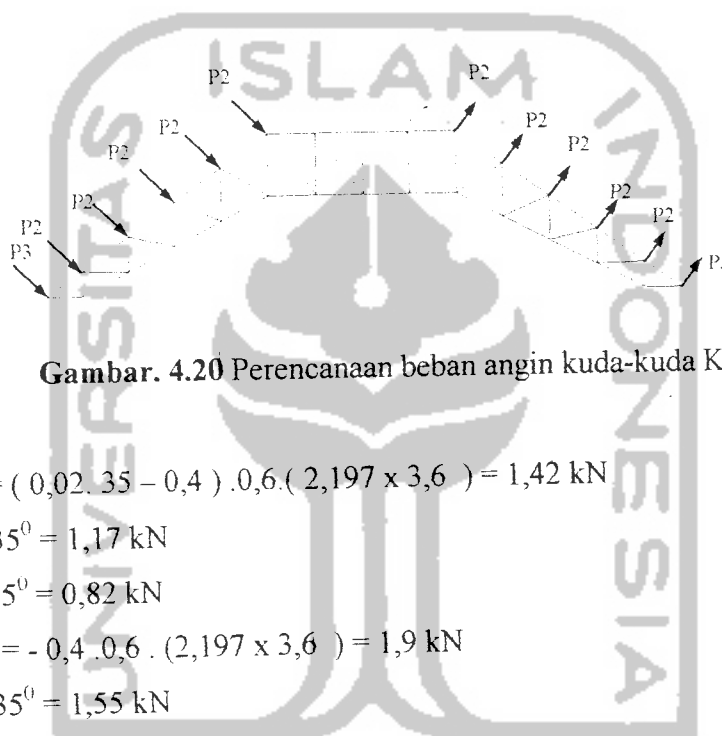
$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = 1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$

### b. Perencanaan beban angin kuda-kuda K2



Gambar. 4.20 Perencanaan beban angin kuda-kuda K2

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = 1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

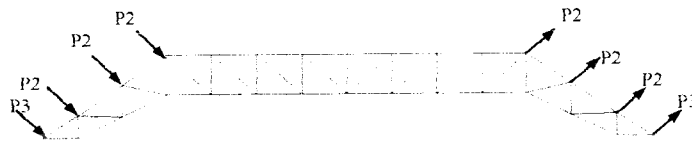
$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = 1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$

### c. Perencanaan beban angin kuda-kuda K3



Gambar. 4.21 Perencanaan beban angin kuda-kuda K3

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = -1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

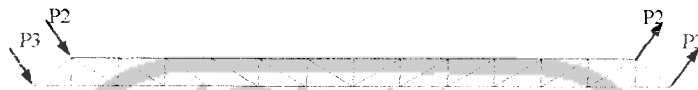
$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = -1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$



#### d. Perencanaan beban angin kuda-kuda K4



Gambar. 4.22 Perencanaan beban angin kuda-kuda K4

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = 1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = 1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$

#### 4.3.2 Analisis Struktur Kuda-Kuda

Analisis struktur kuda-kuda rangka baja menggunakan program aplikasi komputer SAP 90, dengan input data-data sebagai berikut ini:

1. Nomor joint dan element, sesuai bentuk dan ukuran rangka
2. Dukungan rangka baja dianggap sendi dan roll.
3. Luas profil baja yang dipakai.

4. Inersia profil baja.
5. Modulus elastisitas baja,  $E = 200000 \text{ MPa}$
6. Pembebanan berupa beban terpusat.

Input data-data program dan hasil output program disajikan dalam lampiran.

### 4.3.3 Gaya Batang Rencana Kuda-Kuda

Gaya batang rencana kuda-kuda rangka baja merupakan hasil dari kombinasi gaya-gaya batang hasil analisis stuktur, menurut LRFD,2000 sebagai berikut.

$$N_{u1} = 1,4 N_D$$

$$N_{u2} = 1,2 N_D + 0,5 N_L$$

$$N_{u3} = 1,2 N_D + 0,5 N_H$$

$$N_{u4} = 1,2 N_D + 1,6 N_L + 0,8 N_{Wkiri}$$

$$N_{u5} = 1,2 N_D + 1,6 N_L + 0,8 N_{Wkanan}$$

$$N_{u6} = 1,2 N_D + 1,3 N_{W,kiri} + 0,5 N_L$$

$$N_{u7} = 1,2 N_D + 1,3 N_{W,kanan} + 0,5 N_L$$

$$N_{u8} = 0,9 N_D - 1,3 N_{W,kiri}$$

$$N_{u9} = 0,9 N_D - 1,3 N_{W,kanan}$$

Sebagai contoh perhitungan dinjau pada gaya batang rencana kuda-kuda K1 nomor batang 1.

Diketahui:

$$N_D = 8,7000 \text{ kN} ; N_L = 3,4100 \text{ kN} ; N_R = 0,9800 \text{ kN} ;$$

$$N_{Wki} = 1,2300 \text{ kN} ; N_{Wka} = -1,6200 \text{ kN}$$

$$\begin{aligned} N_u &= 1,2 \cdot N_D + 1,6 \cdot N_L + 0,8 \cdot N_{Wki} \\ &= 1,2 \cdot 8,7000 + 1,6 \cdot 3,4100 + 0,8 \cdot 1,2300 \end{aligned}$$

$$= 16,8800 \text{ kN ( kombinasi terbesar )}$$

Dengan cara yang sama dapat dihitung gaya batang rencana kuda-kuda yang lainnya berdasarkan kombinasi faktor beban, dipilih yang terbesar yang disajikan pada Tabel 4.8

Tabel 4.8 Gaya Batang Kuda-Kuda (Satuan kN)

Kuda-kuda	No.	N.D	N.L	N.H	N.W.ki	N.W.ka	N.u.1	N.u.2	N.u.3	N.u.4	N.u.5	N.u.6	N.u.7	N.u.8	N.u.9	N.u tarik	N.u tekan	Jenis	
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]	
K1	1	8,7000	3,4100	0,9800	1,2300	-1,6200	12,1800	12,1450	10,9300	16,8800	14,6000	13,7440	10,0390	6,2310	9,9360	16,8800	-	-	a
	2	-60,1900	-15,6600	-7,5300	8,8800	11,9100	-84,2660	-80,0560	-75,9930	-104,3880	-87,7560	-91,6020	-64,5750	42,6270	-69,6540	-	-104,3880	a	
	3	-93,7200	-24,4800	-11,3800	-13,1900	17,6700	-131,2060	-124,7040	-118,1540	-162,1840	-137,4960	-141,8510	-101,7330	-67,2010	-107,3190	-	-162,1840	a	
	4	-105,6000	-28,0700	-12,8700	-14,4000	19,3200	-147,8400	-140,7550	-133,1550	-183,1520	-156,1760	-159,4750	-115,6390	-76,3200	-120,1560	-	-183,1520	a	
	5	-108,4200	-28,7300	-13,0300	-13,9100	18,7000	-151,7880	-144,4690	-136,6190	-187,2000	-161,1120	-162,5520	-120,1590	-79,4950	-121,8880	-	-187,2000	a	
	6	-103,3900	-27,5800	-12,3700	-12,3500	16,6600	-144,7460	-137,8580	-130,2530	-178,0760	-154,8680	-153,9130	-116,2000	-76,9960	-114,7090	-	-178,0760	a	
	7	-94,9400	-25,1700	-11,1400	-10,0700	13,6600	-132,9160	-126,5130	-119,4980	-162,2560	-143,2720	-139,6040	-108,7550	-72,3550	-103,2040	-	-162,2560	a	
	8	-103,3900	-27,5800	-12,3700	-9,9000	10,2200	-144,7460	-137,8580	-130,2530	-172,9160	-143,0400	-139,9810	-108,3780	-71,9780	-103,5810	-	-162,4880	a	
	9	-108,4200	-28,7300	-13,0300	-1,9100	6,7200	-151,7880	-144,4690	-136,6190	-177,6000	-170,8960	-146,9520	-135,7330	-95,0950	-106,3140	-	-177,6000	a	
	10	-105,6000	-28,0700	-12,8700	1,3300	3,6300	-147,8400	-140,7550	-133,1550	-170,5680	-168,7280	-139,0260	-136,0360	-96,7690	-99,7590	-	-170,5680	a	
	11	-93,7200	-24,4800	-11,3800	3,3500	1,8000	-131,2080	-124,7040	-118,1540	-148,9520	-148,9520	-150,6880	-120,3490	-88,7030	-85,8820	-	-150,6880	a	
	12	-60,1900	-15,6600	-7,5300	3,3700	0,2200	-84,2660	-80,0560	-75,9930	-97,4600	-97,4600	-75,6770	-80,3440	-58,5520	-53,8850	-	-97,4600	a	
	13	8,7000	3,4100	0,9800	0,0100	0,0000	12,1800	12,1450	10,9300	15,9040	15,9040	12,1580	12,1450	7,8170	7,8300	15,8960	-	-	a
	14	-7,1200	-2,7900	-0,8000	-1,5100	2,0000	-9,9680	-9,9390	-8,9440	-14,2160	-11,4080	-11,9020	-7,3390	-4,4450	-9,0080	-	-14,2160	b	
	15	-7,9100	-3,1200	-0,8900	11,2800	-11,0400	-11,0740	-11,0520	-9,9370	-5,4600	-23,3160	3,6120	-25,4040	-21,7830	7,2330	-	-25,4040	b	
	16	55,4500	14,4300	6,9300	19,8100	-22,4400	77,6300	73,7550	70,0050	105,4760	118,4240	99,5080	44,5830	47,9910	112,1200	105,4760	-	-	b
	17	86,3000	22,5400	10,4800	23,0400	-26,8000	136,1220	129,6010	122,6010	176,4680	136,5960	159,5530	94,7610	57,5550	122,3470	176,4680	-	-	b
	18	97,2300	25,8500	11,8500	21,6600	-25,0100	139,7900	133,0500	125,8200	179,4840	142,1480	161,2080	100,5370	61,7070	122,3780	179,4840	-	-	b
	19	95,0600	25,3600	11,3700	19,2900	-21,8900	133,0840	126,7520	119,7570	170,0800	147,1480	161,2080	100,5370	60,4770	114,0110	170,0800	-	-	b
	20	99,8500	26,4600	12,0000	21,6600	-25,0100	139,7900	133,0500	125,8200	179,4840	142,1480	161,2080	100,5370	61,7070	122,3780	179,4840	-	-	b
	21	95,0600	25,3600	11,3700	10,9200	-13,5200	133,0840	126,7520	119,7570	170,0800	147,1480	161,2080	100,5370	60,4770	114,0110	170,0800	-	-	b
	22	99,8500	26,4600	12,0000	6,0500	-9,4200	139,7900	133,0500	125,8200	166,9960	143,8320	140,9480	109,1760	71,3580	103,1300	163,3840	-	-	b
	23	97,2300	25,8500	11,8500	1,8400	-5,6400	136,1220	129,6010	122,6010	159,5080	154,8200	140,9150	120,8040	82,0000	102,1110	166,9960	-	-	b
	24	86,3000	22,5400	10,4800	-1,2400	-2,4700	120,8200	114,8300	108,8000	138,6320	137,6480	113,2180	111,6190	79,2820	80,8810	138,6320	-	-	b
	25	55,4500	14,4300	6,9300	-2,3500	-0,3600	77,6300	73,7550	70,0050	87,7480	89,3400	70,7000	73,2870	52,9600	50,3730	89,3400	-	-	b
	26	-7,9100	-3,1200	-0,8900	0,0000	0,0000	-11,0740	-11,0520	-9,9370	-14,4920	-14,4840	-11,0650	-11,0520	-7,1060	-7,1190	-	-14,4920	b	
	27	-7,1200	-2,7900	-0,8000	-0,0100	0,0000	-9,9680	-9,9390	-8,9440	-13,0160	-13,0080	-9,9520	-9,9390	-6,3950	-6,4080	-	-13,0160	b	
	28	-48,0200	-12,5100	-5,9700	9,4900	9,4900	-67,2280	-63,8790	-60,6090	-83,3200	-70,0480	-73,1090	-51,5420	-33,9880	-55,5550	-	-83,3200	vp	
	29	-17,7800	-4,2500	-2,2900	-1,9300	2,6000	-24,8920	-23,4610	-22,4810	-29,6800	-26,0560	-25,9700	-20,0810	-13,4930	-19,3820	-	-29,6800	vp	
	30	-1,0400	0,3900	-0,1500	1,3500	-1,7600	-1,4560	-1,0530	-1,3230	0,4560	-2,0320	0,7020	-3,3410	-2,6910	1,3520	-	-3,3410	vp	
	31	100,7300	27,7000	12,2200	11,6800	-15,6900	141,0220	134,7260	126,9660	174,5400	152,6440	149,9100	114,3290	75,4730	111,0540	152,6440	-	-	vp
	32	-1,0400	0,3900	-0,1500	-4,1300	3,7100	-1,4560	-1,0530	-1,3230	-3,9280	2,3440	-6,4220	3,7700	4,4330	-5,7590	-	-6,4220	vp	
	33	-17,7800	-4,2500	-2,2900	-0,7200	1,3700	-24,8920	-23,4610	-22,4810	-28,7120	-27,0400	-24,3970	-21,6800	-15,0660	-17,7830	-	-28,7120	vp	
	34	-48,0200	-12,5100	-5,9700	2,9500	-0,8300	-67,2280	-63,8790	-60,6090	-75,2800	-78,3040	-60,0440	-64,9580	-47,0530	-42,1390	-	-78,3040	vp	
	35	56,2200	15,5700	6,9400	7,5600	-10,1100	78,7080	75,2490	70,9340	98,4240	84,2880	85,0770	62,1060	40,7700	63,7410	98,4240	-	-	d
	36	28,1300	7,4000	3,2400	2,7800	-3,7200	39,3820	37,4560	35,3760	47,8200	42,8200	41,0700	32,6200	21,7030	30,1530	47,8200	-	-	d
	37	10,4700	3,1700	1,3100	0,1900	-0,2900	14,6580	14,1490	13,2190	17,7880	17,4040	14,3960	13,7720	9,1760	9,8000	17,7880	-	-	d
	38	2,7000	0,6400	0,1500	-1,4200	1,8500	3,7800	3,5600	3,3150	3,1280	5,7440	1,7140	5,9650	4,2760	0,0250	5,9650	-	-	d
	39	-5,3400	-1,2300	-0,7000	-2,6600	3,5100	-7,4760	-7,0230	-6,7580	-10,5040	-5,5680	-10,4810	-2,4600	-1,3480	-9,3690	-	-10,5040	d	
	40	-9,0900	-2,6000	-1,3400	3,6800	4,8500	-12,7260	-12,2060	-11,5780	-18,0120	-11,1880	-16,9920	-5,9030	-3,3970	-14,4860	-	-18,0120	d	
	41	-0,9900	-2,6000	-1,3400	6,6600	-5,4700	-12,7260	-12,2060	-11,5780	-9,7400	-19,4480	-3,5500	-19,3190	-6,9390	-1,0700	-	-19,4480	d	
	42	-5,3400	-1,2300	-0,7000	5,4900	-4,6400	-7,4760	-7,0230	-6,7580	-3,9840	-12,0680	0,1140	-13,0550	-11,9330	1,2260	-	-13,0550	d	
	43	2,7000	0,6400	0,1500	4,3400	-3,8900	3,7800	3,5600	3,3150	7,7360	1,1520	9,2020	-1,4970	-3,2120	7,4870	9,2020	-	-	d

Tabel 4.8 Lanjutan

Kuda-kuda	No.	ND	NL	NH	NWHi	NWka	Nu.1	Nu.2	Nu.3	Nu.4	Nu.5	Nu.6	Nu.7	Nu.8	Nu.9	Nu tarik	Nu tekan	Jenis		
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]		
K1	48	10,4700	3,1700	1,3100	2,9600	-3,0400	14,6580	14,1490	13,2190	20,0040	15,2040	17,9970	10,1970	5,5750	13,3750	20,0040	-	d		
	50	28,1300	7,4000	3,2400	1,0000	-1,9200	39,3820	37,4560	35,3760	46,3960	44,0600	38,7560	34,9600	24,0170	27,8130	46,3960	-	d		
	52	56,2200	15,5700	6,9400	-2,0700	-0,3200	78,7080	75,2490	70,9340	70,9340	92,1200	72,5580	74,8300	53,2890	51,0140	92,7200	-	d		
	31	-31,0100	-7,5900	-3,8300	4,2100	5,6100	-43,4140	-41,0070	-39,1270	-52,7240	-44,8680	-46,4800	-33,7140	-22,4360	-35,2020	-	-52,7240	v		
	35	-8,9300	-1,7000	-1,1200	-0,1700	0,2500	-12,5020	-11,5660	-11,2760	-13,5720	-13,2360	-11,7870	-11,2410	-7,8160	-8,3620	-	-13,5720	v		
	39	5,5700	2,2800	0,7300	2,7300	-3,5900	7,7980	7,8240	7,0490	7,0490	12,5160	7,4600	11,3730	3,1570	1,4640	9,6800	12,5160	-	v	
	43	5,5700	2,2800	0,7300	-5,5700	4,6900	7,7980	7,8240	7,0490	7,0490	14,0840	14,0840	0,5830	13,9210	12,2540	-1,0840	14,0840	-	v	
	47	-8,9300	-1,7000	-1,1200	-2,5100	2,5800	-12,5020	-11,5660	-11,2760	-11,2760	-15,4440	-11,3720	-14,8290	-8,2120	-4,7740	-11,3910	-	-15,4440	v	
	51	-31,0100	-7,5900	-3,8300	1,1500	0,1700	-43,4140	-41,0070	-39,1270	-52,7240	-48,4360	-49,2200	-39,5120	-40,7860	-29,4040	-28,1300	-	-49,2200	v	
	K2	1	8,6600	3,4100	0,9900	1,2300	-1,6200	12,1240	12,0970	10,8870	16,8320	14,5520	13,6960	9,9910	6,1950	9,9000	16,8320	-	a	
		2	-55,6500	-15,6600	-5,9500	-9,2200	11,3100	-77,9100	-74,6100	-69,7550	-99,2120	-82,7880	-86,5960	-59,9070	-38,0990	-64,7880	-	-99,2120	a	
		3	-86,4600	-24,4800	-8,8600	-13,7100	16,7000	-121,0440	-115,9920	-108,1820	-153,8880	-129,5600	-133,8150	-94,2820	-59,9910	-99,5240	-	-153,8880	a	
		4	-96,5900	-28,0700	-9,7300	-15,0600	18,1200	-135,2260	-129,9430	-120,7730	-172,8680	-146,3240	-149,5210	-106,3870	-67,3530	-110,4870	-	-172,8680	a	
		5	-98,1100	-28,7100	-9,4400	-14,6400	17,3000	-137,3540	-132,0870	-122,4520	-175,3800	-149,8280	-151,1190	-109,5970	-69,2670	-110,7890	-	-175,3800	a	
		6	-84,7100	-25,8600	-7,9300	-9,9800	12,4400	-118,5940	-114,5820	-105,6170	-151,0120	-133,0760	-127,5560	-98,4100	-63,2650	-92,4110	-	-151,0120	a	
		7	-88,0000	-26,6300	-8,1100	-7,1200	9,5700	-123,2000	-118,9150	-109,6550	-153,9040	-140,5520	-128,1710	-106,4740	-69,9440	-91,6410	-	-153,9040	a	
		8	-88,0000	-26,6300	-8,1100	-7,1100	9,5600	-123,2000	-118,9150	-109,6550	-153,8960	-140,5600	-128,1580	-106,4870	-69,9570	-91,6280	-	-153,8960	a	
		9	-84,7100	-25,8600	-7,9300	-4,2500	6,7000	-118,5940	-114,5820	-105,6170	-146,4280	-137,6680	-120,1070	-105,8720	-70,7140	-84,9490	-	-146,4280	a	
		10	-98,1100	-28,7100	-9,4400	-3,0300	5,7000	-137,3540	-132,0870	-122,4520	-166,0920	-159,1080	-136,0260	-124,6770	-84,3600	-95,7090	-	-166,0920	a	
		11	-96,5900	-28,0700	-9,7300	0,2700	2,7900	-135,2260	-129,9430	-120,7730	-160,6040	-158,5880	-129,5920	-126,3160	-87,2820	-90,5580	-	-160,6040	a	
		12	-86,4600	-24,4800	-8,8600	2,3900	0,6000	-121,0440	-115,9920	-108,1820	-141,0080	-142,4400	-112,8850	-115,2120	-75,0260	-80,9210	-	-142,4400	a	
		13	-55,6500	-15,6600	-5,9500	2,4100	-0,3200	-77,9100	-74,6100	-69,7550	-89,9080	-92,0920	-71,4770	-75,0260	-53,2180	-53,2180	-	-92,0920	a	
		14	8,6600	3,4100	0,9900	1,6300	1,2400	12,1240	12,0970	10,8870	14,5440	16,8400	16,8400	9,9780	13,7090	9,9130	16,8400	-	a	
		15	-7,0800	-2,7900	-0,8100	-1,5100	2,0000	-9,9120	-9,8910	-8,9010	-14,1680	-14,1680	-11,3600	-11,8540	-7,2910	-4,4090	-8,9720	-	-14,1680	b
		16	-7,8800	-3,1200	-0,9000	10,0900	-9,5400	11,0320	-11,0160	-9,9060	-6,3760	-22,0800	-22,0800	2,1010	-23,4180	-20,2090	5,3100	-	-23,4180	b
		17	51,2600	14,4300	5,4800	18,9300	-20,3900	71,7640	68,7270	64,2520	99,7440	68,2880	93,3360	93,3360	42,2200	21,5250	72,6410	99,7440	-	b
		18	79,6300	22,5400	8,1600	22,1300	-24,1200	111,4820	106,8260	99,6360	149,3240	112,3240	135,5950	135,5950	75,4700	42,8980	103,0230	149,3240	-	b
		19	88,8800	25,8300	8,9500	22,4400	-24,1900	124,4320	119,5710	111,1310	165,9360	128,6320	148,7430	148,7430	88,1240	50,8200	111,4390	165,9360	-	b
		20	80,4300	23,5400	7,7400	18,8100	-19,7700	112,6020	108,2860	100,3860	149,2280	118,3640	132,7390	132,7390	82,5850	47,9340	98,0880	149,2280	-	b
		21	84,7100	25,8600	7,9300	15,9800	-16,9400	118,5940	114,5820	105,6170	155,8120	129,4760	135,3560	135,3560	92,5600	55,4650	98,2610	155,8120	-	b
		22	84,7100	25,8600	7,9300	10,2500	-11,2200	118,5940	114,5820	105,6170	151,2280	134,0520	127,9070	127,9070	99,9960	62,9140	90,8250	151,2280	-	b
		23	80,4300	23,5400	7,7400	7,4000	-8,3700	112,6020	108,2860	100,3860	140,1000	127,4840	117,9060	117,9060	97,4050	62,9140	83,2680	140,1000	-	b
		24	88,8800	25,8300	8,9500	4,0400	-5,7900	124,4320	119,5710	111,1310	151,2160	143,3520	124,8230	124,8230	112,0440	74,7400	87,5190	151,2160	-	b
		25	79,6300	22,5400	8,1600	0,8700	-2,8600	111,4820	106,8260	99,6360	132,3160	129,3320	107,9570	107,9570	103,1080	70,5360	75,3850	132,3160	-	b
		26	51,2600	14,4300	5,4800	-0,3700	1,0900	71,7640	68,7270	64,2520	84,3040	83,7280	68,2460	67,3100	46,6150	46,6150	47,5510	84,3040	-	b
		27	-7,8800	-3,1200	-0,9000	2,2500	-1,7100	-11,0320	-9,9120	-8,9010	-12,6480	-15,8160	-8,0910	-8,0910	-13,2390	-10,0170	-4,8690	-	-15,8160	b
		28	-7,0800	-2,7900	-0,8100	2,0100	-1,5200	-9,9120	-9,8910	-8,9010	-11,3520	-14,1760	-7,2780	-7,2780	-11,8670	-8,9850	-4,3960	-	-14,1760	b
		29	-45,2200	-12,5100	-5,0200	-7,3000	9,1300	-63,3080	-60,5190	-56,7740	-80,1200	-66,9760	-70,0090	-70,0090	-48,6500	-31,2080	-52,5670	-	-80,1200	vp
		33	-16,1800	-4,2500	-1,7300	-2,0600	2,3900	-22,6520	-21,5410	-20,2810	-27,8640	-24,3040	-24,3040	-24,2190	-18,4340	-11,8840	-17,6690	-	-27,8640	vp
		37	41,1200	12,4000	4,2000	10,8700	-12,0100	57,5680	55,5440	51,4440	77,8800	59,5760	69,6750	69,6750	39,9310	22,8770	52,6210	77,8800	-	vp
		41	-7,0700	-1,0100	-0,4800	-0,0100	0,0100	-9,9880	-8,9890	-8,7240	-10,1080	-10,0920	-9,0020	-9,0020	-8,9760	-6,3500	-6,3760	-	-10,1080	vp
		45	41,1200	12,4000	4,2000	-0,4100	0,7300	57,5680	55,5440	51,4440	68,8560	68,6000	55,0110	54,5950	37,5410	37,5410	37,9570	68,8560	-	vp
		49	-16,1800	-4,2500	-1,7300	-0,8100	1,1400	-22,6520	-21,5410	-20,2810	-26,8640	-25,3040	-22,5940	-22,5940	-20,0590	-13,5090	-16,0440	-	-26,8640	vp
		53	-45,2200	-12,5100	-5,0200	3,7900	-1,9600	-63,3080	-60,5190	-56,7740	-71,2480	-75,8480	-55,5920	-55,5920	-63,0670	-45,6250	-38,1500	-	-75,8480	vp

Tabel 4.8 Lanjutan

Kuda-kuda	No.	N/D	NL	NH	N/Wf	N/Wk	Nu.1	Nu.2	Nu.3	Nu.4	Nu.5	Nu.6	Nu.7	Nu.8	Nu.9	Nu.tank	Nu.tekan	Jenis		
																			[1]	[2]
K2	30	52,4800	15,5700	5,6600	7,8300	-9,6200	73,4720	70,7610	65,8060	94,1520	80,1920	80,9400	58,2550	37,0530	59,7380	94,1520	-	-	d	
	32	25,8600	7,4000	2,4400	2,9400	-3,4100	36,2040	34,7320	32,2520	45,2240	40,1440	38,5540	30,2990	19,4520	27,7070	45,2240	-	-	d	
	34	8,8900	3,1600	0,7600	0,3000	-0,0700	12,4460	12,2480	11,0480	15,9680	12,6380	12,6380	12,1570	7,6110	8,0920	15,9680	-	-	d	
	36	1,5800	0,6500	-0,2600	-1,3300	2,0100	2,2120	2,2210	1,7660	1,8720	4,5440	0,4920	4,8340	3,1510	-1,1910	4,5440	-	-	d	
	38	7,0200	3,8000	0,3100	-4,6100	4,6100	9,8280	10,3240	8,5790	10,8160	18,1920	4,3310	16,3170	12,3110	0,3250	18,1920	-	-	d	
	40	5,3600	1,2500	0,3000	-4,6700	4,6700	7,5040	7,0570	6,5820	4,6960	12,1680	0,9860	13,1280	10,8950	-1,2470	12,1680	-	-	d	
	42	5,3600	1,2500	0,3000	-4,6700	4,6700	7,5040	7,0570	6,5820	4,6960	12,1680	0,9860	13,1280	10,8950	-1,2470	12,1680	-	-	d	
	44	7,0200	3,8000	0,3100	-4,6500	4,6500	9,8280	10,3240	8,5790	18,2240	16,3690	4,2790	16,3690	0,2730	12,3630	18,2240	-	-	d	
	46	1,5800	0,6500	-0,2600	-1,3300	2,0100	2,2120	2,2210	1,7660	6,4720	-0,0480	7,9670	-2,6280	-4,3240	6,2710	7,9670	-	-	d	
	48	8,8900	3,1600	0,7600	3,0400	-2,8100	12,4460	12,2480	11,0480	18,1560	13,4760	16,2000	8,5950	4,0490	11,6540	18,1560	-	-	d	
	50	25,8600	7,4000	2,4400	1,1300	-1,6000	36,2040	34,7320	32,2520	43,7760	41,5920	36,2010	32,6520	21,8050	25,3540	43,7760	-	-	d	
	52	52,4800	15,5700	5,6600	-2,3300	0,5400	73,4720	70,7610	65,8060	86,0240	88,3200	67,7320	71,4630	50,2610	46,5300	88,3200	-	-	d	
	31	-28,9500	-7,5900	-3,1200	-4,3500	5,3400	-40,5300	-38,5350	-36,3000	-50,3640	-42,6120	-44,1900	-31,5930	-20,4000	-32,9970	-	-50,3640	v		
	35	-7,2500	-1,6800	-0,6400	-0,2400	0,0500	-10,1500	-9,5400	-9,0200	-11,5800	-11,3480	-9,8520	-2,5990	-12,1800	-9,5900	-6,5900	-	-11,5800	v	
	39	-5,3400	-1,9500	-0,2300	-3,6800	3,6800	-7,4760	-7,3830	-6,5230	-6,5840	-12,4800	-6,0000	-12,1410	-2,6250	-0,0480	-9,5640	-	-12,4800	v	
	43	-5,3400	-1,9500	-0,2300	-3,6600	3,6600	-7,4760	-7,3830	-6,5230	-12,4560	-6,0000	-12,1410	-2,6250	-0,0480	-9,5640	-	-12,4800	v		
	47	-7,5200	-1,6800	-0,6400	-2,5800	2,5800	-10,5280	-9,8640	-9,3440	-13,7760	-9,8000	-13,2180	-6,7570	-3,4140	-9,8750	-	-13,7760	v		
	51	-28,9500	-7,5700	-3,1200	-1,2900	1,2900	-40,5300	-38,5250	-36,3000	-45,8200	-47,0920	-36,8480	-38,9150	-27,7320	-25,6650	-	-47,0920	v		
	K3	1	8,1900	3,4100	0,9900	1,2300	-1,6300	11,4660	11,5330	10,3230	16,2680	13,1320	13,1320	9,4140	5,7720	9,4900	16,2680	-	-	a
		2	-50,9500	-15,6600	-4,7600	-6,3200	7,1500	-71,3300	-68,9700	-63,5200	-91,2520	-80,4760	-77,1860	-59,6750	-37,6390	-55,1500	-	-91,2520	a	
		3	-78,7200	-24,4700	-6,9600	-9,0300	10,0000	-110,2080	-106,6990	-97,9440	-140,8400	-125,6160	-118,4380	-93,6990	-59,1090	-83,8480	-	-140,8400	a	
		4	-81,9900	-27,6600	-7,2600	-6,9800	8,0400	-114,7860	-112,2180	-102,0180	-148,2280	-136,2120	-121,2920	-101,7660	-64,7170	-84,2430	-	-148,2280	a	
		5	-98,1900	-33,1000	-8,8000	-5,7200	6,7800	-137,4660	-134,3780	-122,2280	-175,3640	-165,3640	-141,8140	-125,5640	-80,9350	-97,1850	-	-175,3640	a	
		6	-104,5100	-36,3600	-9,3300	-4,4600	5,5300	-146,3140	-143,5920	-130,0770	-187,1560	-179,1640	-149,3900	-136,4030	-88,2610	-101,2480	-	-187,1560	a	
		7	-109,5300	-37,4600	-9,8400	-3,2100	4,2700	-153,3420	-150,1660	-136,3560	-193,9400	-187,9560	-154,3260	-144,6150	-94,4170	-104,1280	-	-193,9400	a	
		8	-104,5100	-36,3600	-9,8400	-3,2000	4,2700	-153,3420	-150,1660	-136,3560	-193,9320	-187,9560	-154,3260	-144,6150	-94,4170	-104,1280	-	-193,9320	a	
9		-98,1900	-33,1000	-8,3300	-1,9400	3,0000	-146,3140	-143,5920	-130,0770	-185,1400	-181,1880	-146,1140	-139,6920	-91,5370	-97,9590	-	-185,1400	a		
10		-98,1900	-33,1000	-8,8000	-0,6800	1,7500	-137,4660	-134,3780	-122,2280	-171,3320	-169,3880	-135,2620	-132,1030	-87,4870	-90,6460	-	-171,3320	a		
11		-81,9900	-27,6600	-7,2600	0,5700	0,4900	-114,7860	-112,2180	-102,0180	-142,1880	-142,2520	-111,4770	-111,5810	-74,5320	-74,4280	-	-142,1880	a		
12		-78,7200	-24,4700	-6,9600	0,0600	0,0600	-110,2080	-106,6990	-97,9440	-132,8960	-133,5680	-105,5290	-106,6210	-72,0180	-70,9260	-	-132,8960	a		
13		-50,9500	-15,6600	-4,7600	1,4800	-0,6500	-71,3300	-68,9700	-63,5200	-85,0120	-86,7160	-67,0460	-69,8150	-47,7790	-45,0100	-	-86,7160	a		
14		8,1900	3,4100	0,9900	-1,6400	1,2400	11,4660	11,5330	10,3230	13,9720	16,2760	9,4010	13,1450	9,5030	5,7590	16,2760	-	-	a	
15		-6,6900	-2,7900	-0,8100	-1,5100	2,0000	-9,3660	-9,4230	-8,4330	-13,7000	-10,8920	-11,3860	-6,8230	-4,0580	-8,6210	-	-11,3860	b		
16		-7,4400	-3,1100	-0,9000	-5,8100	5,8100	-10,4160	-10,4830	-9,3780	-9,2560	-18,1040	-2,9300	-17,3080	-14,2490	0,1290	-	-18,1040	b		
17		46,8900	14,4100	4,3800	11,9500	-12,2600	65,6460	63,4730	58,4580	88,8840	69,5160	79,0080	47,5350	26,6660	58,1390	88,8840	-	-	b	
18		64,5900	20,0900	5,7100	12,0400	-12,2600	90,4260	87,5530	80,3630	119,2840	99,8440	103,2050	71,6150	42,4790	74,0690	119,2840	-	-	b	
19		82,0300	27,6700	7,2600	10,7900	-10,9100	114,8420	112,2410	102,0660	151,3400	133,9800	126,2980	98,0880	59,8000	88,0100	151,3400	-	-	b	
20		98,2400	33,1200	8,8100	9,5300	-9,6500	137,5360	134,4480	122,2930	178,5040	163,1600	146,8370	121,9030	76,0270	100,9610	178,5040	-	-	b	
21		104,5200	36,3700	9,3300	8,2800	-8,3900	146,3280	143,6090	130,0890	190,2400	176,9040	154,3730	132,7020	83,3040	104,9750	190,2400	-	-	b	
22		104,5200	36,3700	9,3300	5,7600	-5,8800	146,3280	143,6090	130,0890	188,2240	178,9120	151,0970	135,9650	86,5800	101,7120	188,2240	-	-	b	
23		98,2400	33,1200	8,8100	4,5100	-4,6200	137,5360	134,4480	122,2930	174,4880	167,1840	140,3110	128,4420	82,5530	94,4220	174,4880	-	-	b	
24		64,5900	20,0900	5,7100	3,2500	-3,3600	114,8420	112,2710	102,0660	145,3080	140,0200	116,4960	107,9030	69,6020	78,1950	145,3080	-	-	b	
25		82,0300	27,6700	7,2600	1,9900	-2,1100	90,4260	87,5530	80,3630	111,2440	107,9640	90,1400	84,8100	55,5440	60,8740	111,2440	-	-	b	
26		46,8900	14,4100	4,3800	0,4800	-0,7900	65,6460	63,4730	58,4580	79,7080	78,6920	64,0970	62,4460	41,5770	43,2280	79,7080	-	-	b	

Tabel 4.8 Lanjutan

Kuda-kuda	No.	N.D	[3]	N.L	N.H	N.W.ki	N.W.ke	N.u.1	N.u.2	N.u.3	N.u.4	N.u.5	N.u.6	N.u.7	N.u.8	N.u.9	N.u.tarik	N.u.tekan	Jenis		
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]			
K3	27	-7,4400	-3,1100	-0,9000	2,2600	-1,7100	-10,4160	-10,4630	-9,3780	-12,0960	-15,2720	-7,5450	-12,7060	-9,6340	-4,4730	-	-15,2720	b			
	28	-6,6900	-2,7900	-0,8100	2,0100	-1,5200	-9,3660	-9,4230	-8,4330	-10,8840	-13,7080	-6,8100	-11,3990	-8,6340	-4,0450	-	-13,7080	b			
	29	-42,0600	-12,5200	4,3100	-5,5600	6,6300	-58,8840	-56,7320	-52,6270	-74,9520	-65,2000	-63,9600	-48,1130	-30,6260	-46,4730	-	-74,9520	vp			
	33	19,6700	6,9800	1,6100	5,1400	-5,3100	27,5380	26,6040	24,4090	37,3160	28,9560	33,2860	19,7010	11,0210	24,6060	37,3160	-	-	vp		
	37	-12,7000	-3,9800	-1,4200	1,1500	-1,1500	-17,7800	-17,2300	-15,9500	-20,6880	-22,5280	-22,5280	-15,7350	-15,7350	-12,9250	-	-	-20,6880	vp		
	41	-7,0400	-1,0000	-0,9400	0,0000	0,0000	-9,8560	-8,9480	-8,9180	-10,0480	-10,0480	-10,0480	-8,9480	-8,9480	-6,3360	-	-	-10,0480	vp		
	45	-12,7000	-3,9800	-1,4200	1,1500	-1,1500	-17,7800	-17,2300	-15,9500	-22,5280	-22,5280	-22,5280	-18,7250	-15,7350	-12,9250	-	-	-20,6880	vp		
	49	19,6700	6,9800	1,6100	5,1400	-0,0500	27,5380	26,6040	24,4090	33,1080	33,1080	33,1640	26,4480	26,5390	17,8590	17,7680	33,1640	-	-	vp	
	53	-42,0600	-12,5200	4,3100	3,2300	-2,1600	-58,8840	-56,7320	-52,6270	-67,9200	-67,9200	-72,2320	-52,5330	-59,5400	-42,0630	-35,0460	-	-	-72,2320	vp	
	30	48,2400	15,5500	4,6900	5,4500	6,2100	67,5360	65,6630	60,2330	87,1280	77,8000	72,7480	57,5900	36,3810	51,4890	87,1280	-	-	-	d	
	32	23,3900	7,4300	1,8500	1,4600	-1,3000	32,7460	31,7830	28,9930	41,1240	38,9160	33,6810	30,0930	19,1530	22,7410	41,1240	-	-	-	d	
	34	23,6200	10,2800	2,1000	-1,6800	1,6800	33,0680	33,4840	29,3940	43,4480	46,1360	31,3000	35,6680	23,4420	19,0740	46,1360	-	-	-	d	
	36	21,9300	7,3600	2,0900	-1,7000	1,7000	30,7020	29,9960	27,3610	36,7320	39,4520	27,7860	32,2060	21,9470	17,5270	39,4520	-	-	-	d	
	38	8,4900	4,4100	0,7000	0,6900	-1,7000	1,7000	11,8860	12,3930	10,5380	15,8840	18,6040	10,1830	14,6030	9,8510	5,4310	18,6040	-	-	-	d
	40	6,8000	1,4800	0,6900	1,7000	1,7000	9,5200	8,9000	8,5050	9,1680	11,8880	11,8880	6,6900	11,1100	8,3300	3,9100	11,8880	-	-	-	d
	42	6,8000	1,4800	0,6900	1,7000	1,7000	9,5200	8,9000	8,5050	11,8960	11,8960	11,1230	6,6770	3,8970	8,3430	11,8880	-	-	-	d	
	44	8,4900	4,4100	0,7000	0,6900	-1,7000	1,7000	11,8860	12,3930	10,5380	18,6040	15,8840	14,6030	10,1830	5,4310	9,8510	18,6040	-	-	-	d
46	21,9300	7,3600	2,0900	1,7000	1,7000	30,7020	29,9960	27,3610	39,4520	39,4520	32,2060	32,2060	27,7860	17,5270	21,9470	39,4520	-	-	-	d	
48	23,6200	10,2800	2,1000	1,7000	1,7000	33,0680	33,4840	29,3940	46,1520	43,4320	35,6940	31,2740	19,0480	22,9100	46,1520	-	-	-	v		
50	23,3900	7,4300	1,8500	1,5900	1,5900	32,7460	31,7830	28,9930	41,2280	38,8120	33,8500	29,9240	18,9840	22,9100	41,2280	-	-	-	v		
52	48,2400	15,5500	4,6900	5,4500	6,2100	67,5360	65,6630	60,2330	81,5040	83,4160	63,6090	66,7160	45,4700	42,3630	83,4160	-	-	-	v		
31	-26,5700	-7,5700	-2,5900	3,4400	-3,0200	3,4400	-37,1980	-35,6690	-33,1790	-46,4120	-41,2440	-39,5950	-31,1970	-19,9870	-28,3850	-	-	-46,4120	v		
35	-15,8800	-5,9300	-1,4100	1,1500	-1,1500	-22,2320	-22,0210	-19,7610	-27,6240	-29,4640	-20,5260	-23,5160	-15,7870	-12,7970	-	-	-29,4640	v			
39	-5,7300	-1,9900	-0,4700	1,1500	-1,1500	-8,0220	-7,8710	-7,1110	-9,1400	-10,9800	-9,1400	-9,3660	-6,3760	-6,6520	-	-	-10,9800	v			
43	-5,7300	-1,9900	-0,4700	1,1500	-1,1500	-8,0220	-7,8710	-7,1110	-10,9800	-9,1400	-9,1400	-9,3660	-6,3760	-6,6520	-	-	-10,9800	v			
47	-15,8800	-5,9300	-1,4100	1,1500	-1,1500	-22,2320	-22,0210	-19,7610	-29,4640	-29,4640	-23,5160	-20,5260	-12,7970	-15,7870	-	-	-29,4640	v			
51	-26,5700	-7,5700	-2,5900	0,8700	0,8700	-37,1980	-35,6690	-33,1790	-43,3000	-44,3560	-34,5380	-36,2540	-25,0440	-23,3280	-	-	-44,3560	v			
K4	1	7,2500	3,4500	0,8500	1,0400	-1,3800	10,1500	10,4250	9,1250	15,0520	13,1160	11,7770	8,6310	5,1730	8,3190	15,0520	-	-	a		
	2	2,9500	1,0000	0,4200	0,4900	-0,4400	4,1300	4,0400	3,7500	5,5320	4,7880	4,6770	3,4680	2,0180	3,2270	5,5320	-	-	-	a	
	3	1,6800	0,9300	0,1400	0,8500	-0,7100	2,3520	2,4810	2,0860	4,1840	2,9360	3,5860	1,5580	0,4070	2,4350	4,1840	-	-	-	a	
	4	0,3300	-0,1400	0,0900	0,8400	-0,6700	0,4620	0,3260	0,4410	0,8440	-0,3640	1,4180	-0,5450	-0,7950	1,1680	0,8440	-	-	-	a	
	5	0,7800	0,5600	0,0400	0,8200	-0,6300	1,0920	1,2160	0,9560	2,4980	1,3280	2,2880	0,3970	-0,3640	1,5210	2,4900	-	-	-	a	
	6	0,2500	-0,2300	0,0800	0,7000	-0,5300	0,3500	0,1850	0,3400	0,4920	-0,4920	1,0950	-0,5040	-0,6850	0,9140	0,9140	-	-	-	a	
	7	1,5200	0,7500	0,1200	0,5700	-0,4300	2,1280	2,1990	1,8840	3,4800	2,6800	2,9400	1,6400	0,6270	1,9270	3,4800	-	-	-	a	
	8	1,5200	0,7500	0,1200	0,5700	-0,4300	2,1280	2,1990	1,8840	3,4800	2,6800	2,9400	1,6400	0,6270	1,9270	3,4800	-	-	-	a	
	9	0,2500	-0,2300	0,0800	0,6800	-0,5100	0,3500	0,1850	0,3400	0,4760	-0,4760	1,0690	-0,4760	-0,6590	0,8880	1,0690	-	-	-	a	
	10	0,7800	0,5600	0,0400	0,7800	-0,5900	1,0920	1,2160	0,9560	2,4560	1,3600	2,2300	0,4490	-0,3120	1,4690	1,4690	-	-	-	a	
	11	0,3300	-0,1400	0,0900	0,6800	-0,5100	0,4620	0,3260	0,4410	0,7160	-0,2360	1,2100	-0,3370	-0,5870	0,9600	0,9600	-	-	-	a	
	12	1,6800	0,9300	0,1400	0,5700	-0,4300	2,3520	2,4810	2,0860	3,9600	3,1600	3,2220	1,9220	0,7710	2,0710	3,9600	-	-	-	a	
	13	2,9500	1,0000	0,4200	0,2000	-0,1500	4,1300	4,0400	3,7500	5,0200	5,0200	4,3000	3,8450	2,3950	2,8500	5,0200	-	-	-	a	
	14	7,2500	3,4500	0,8500	1,3800	-1,3800	10,1500	10,4250	9,1250	13,1160	15,0440	8,6310	11,7640	8,3190	5,1860	15,0440	-	-	-	a	
	15	-0,9400	-2,8300	-0,6900	1,6900	-1,3160	-1,4730	-6,6720	-4,3040	-4,1940	-4,3040	-4,1940	-4,3040	-4,3040	-4,3040	-4,3040	-	-	-6,6720	b	
	16	-5,9300	-2,8200	-0,6900	1,4000	-0,9800	-8,3020	-7,4610	-6,5260	-10,5080	-12,4120	-6,7060	-9,8000	-7,1570	-4,0630	-	-	-12,4120	b		
	17	-2,9200	-0,9900	-0,4200	1,4000	-0,9800	-4,0880	-3,9990	-3,7140	-3,9990	-5,8720	-2,1790	-5,2730	-4,4480	-1,3540	-	-	-5,8720	b		

Tabel 4.8 Lanjutan

Kuda-kuda	No.	ND	[3]	NL	NH	NWki	NWka	Nu.1	Nu.2	Nu.3	Nu.4	Nu.5	Nu.6	Nu.7	Nu.8	Nu.9	Nu tarik	Nu tekan	Jenis
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]	
K4	18	-1,6600	-0,9200	-0,1400	1,0300	-0,7000	-2,3240	-2,4520	-2,0620	-2,6400	-4,0240	-1,1130	-3,3620	-2,8330	-0,5840	-	-4,0240	b	
	19	-0,3200	0,1500	-0,0800	0,6700	-0,4400	-0,4480	-0,3090	-0,4240	0,3920	-0,4960	0,5620	-0,8810	-1,1590	0,2840	-	-1,1590	b	
	20	-0,7700	-0,5600	-0,0400	0,6900	-0,4800	-1,0780	-1,2040	-0,9440	-1,2680	-2,2040	-0,3070	-1,8280	-1,5900	-0,0590	-	-2,2040	b	
	21	-0,2500	0,2300	-0,0800	0,8300	-0,6200	-0,3500	-0,1850	-0,3400	0,7320	-0,4280	0,8940	-0,9910	-1,3040	0,5810	-	-0,9910	b	
	22	-0,2500	0,2300	-0,0800	0,8500	-0,6400	-0,3500	-0,1850	-0,3400	0,7480	-0,4440	0,9200	-1,0170	-1,3300	0,6070	0,9200	-	b	
	23	-0,7700	-0,5600	-0,0400	0,7500	-0,5600	-1,0780	-1,2040	-0,9440	-1,2200	-2,2680	-0,2290	-1,6680	-1,6680	0,0350	-	-2,2680	b	
	24	-0,3200	0,1500	-0,0800	0,8500	-0,6400	-0,4480	-0,3090	-0,4240	0,5360	-0,6560	0,7960	-1,1410	-1,3930	0,5440	-	-1,3930	b	
	25	-1,6600	-0,9200	-0,1400	0,9500	-0,7200	-2,3240	-2,4520	-2,0620	-2,7040	-4,0400	-1,2170	-3,3880	-2,7290	-0,5580	-	-4,0400	b	
	26	-2,9200	-0,9900	-0,4200	1,3300	-1,0000	-4,0980	-3,9990	-3,7140	-4,0240	-5,8880	-2,2700	-5,2990	-4,3570	-1,3280	-	-5,8880	b	
	27	-5,9300	-2,8200	-0,6900	1,6900	-1,2700	-8,3020	-8,5250	-7,4610	-10,2760	-12,6440	-6,3290	-10,1770	-7,5340	-3,6860	-	-12,6440	b	
	28	-5,9400	-2,8300	-0,6900	1,6900	-1,2700	-8,3160	-8,5430	-7,4730	-10,3040	-12,6720	-6,3460	-10,1940	-7,5430	-3,6950	-	-12,6720	b	
	29	-14,1400	-3,9900	-1,4700	-1,4400	3,0200	-19,7960	-18,9630	-17,7030	-24,5040	-20,9360	-20,8350	-15,0370	-10,8540	-16,6520	-	-24,5040	vp	
	33	-7,0800	-1,6000	-0,8600	-0,0100	0,0200	-9,9120	-9,2960	-8,9260	-11,0640	-11,0400	-9,3090	-9,2700	-6,3590	-6,3980	-	-11,0640	vp	
	37	-6,7000	-1,4500	-0,8100	-0,0700	0,0500	-9,3800	-8,7650	-8,4450	-10,4160	-10,3200	-8,3560	-8,7000	-5,9390	-6,0850	-	-10,4160	vp	
	41	-6,4500	-1,0200	-0,8400	0,0000	0,0000	-9,0300	-8,2500	-8,1600	-9,3720	-9,3720	-8,2500	-8,2500	-5,8950	-5,8950	-	-9,3720	vp	
	45	-6,7000	-1,4500	-0,8400	-0,0600	0,0400	-9,3800	-8,7650	-8,4600	-10,4080	-10,3280	-8,3430	-8,7130	-5,9520	-6,0820	-	-10,4080	vp	
	49	-7,0800	-1,6000	-0,8100	0,0500	-0,0400	-9,9120	-9,2960	-8,9010	-11,0160	-11,0880	-9,2310	-9,3480	-6,4370	-6,3200	-	-11,0880	vp	
	53	-14,1400	-3,9900	-1,4700	2,3700	-1,7800	-19,7960	-18,9630	-17,7030	-21,4560	-24,7760	-15,8820	-21,2770	-15,8070	-10,4120	-	-24,7760	vp	
	30	3,4000	2,0700	0,3100	-0,4100	0,3100	4,7600	5,1150	4,2350	7,0640	7,6400	4,6820	5,5180	3,5930	2,6570	7,6400	-	d	
	32	1,4200	0,0700	0,3200	-0,4000	0,3000	1,9880	1,7390	1,8640	1,4960	2,0560	1,2190	2,1290	1,7980	0,8880	2,1290	-	d	
	34	1,5100	1,2100	0,0600	0,0200	-0,0500	2,1140	2,4170	1,8420	3,7640	3,7080	2,4430	2,3520	1,3330	1,4240	3,7640	-	d	
	36	-0,5300	-0,8000	0,0500	0,0200	-0,0500	-0,7420	-1,0360	-0,6110	-1,9000	-1,9560	-1,0100	-1,1010	-0,5030	-0,4120	-	-1,9560	d	
	38	0,5900	0,8900	-0,0500	0,1400	-0,1100	0,8260	1,1530	0,6830	2,2440	2,0440	1,3350	1,0100	0,3490	0,6740	2,2440	-	d	
	40	-1,4500	-1,1200	-0,0500	0,1500	-0,1200	-2,0300	-2,3000	-1,7650	-3,4120	-3,6280	-2,1050	-2,4560	-1,5000	-1,1490	-	-3,6280	d	
	42	-1,4500	-1,1200	-0,0500	0,1200	-0,0900	-2,0300	-2,3000	-1,7650	-3,4360	-3,6040	-2,1440	-2,4170	-1,4610	-1,1880	-	-3,6040	d	
	44	0,5900	0,8900	0,0500	0,1200	-0,0900	0,8260	1,1530	0,6830	2,2280	2,0600	1,3090	1,0360	0,3750	0,6480	2,2280	-	d	
	46	-0,5300	-0,8000	0,0600	-0,1100	0,0900	-0,7420	-1,0360	-0,6060	-2,0040	-1,8440	-1,1790	-0,9190	-0,3340	-0,5940	-	-2,0040	d	
	48	1,5100	1,2100	0,0600	-0,1200	0,0900	2,1140	2,4170	1,8420	3,6520	3,8200	2,2610	2,5340	1,5150	1,2420	3,8200	-	d	
	50	1,4200	0,0700	0,3200	-0,4200	0,3100	1,9880	1,7390	1,8640	1,4800	2,0640	1,1930	2,1420	1,8240	0,8750	2,0640	-	d	
	52	3,4200	2,0700	0,3100	-0,4000	0,3000	4,7880	5,1390	4,2590	7,0960	7,6560	4,6190	5,5290	3,5580	2,6880	7,6560	-	d	
	31	-1,6700	-9,8600	-0,1500	0,1900	-0,1400	-2,3380	-6,9340	-2,0790	-17,6280	-17,8920	-6,6670	-7,1160	-1,7500	-1,3210	-	-17,8920	v	
	35	-0,7500	-5,9400	-0,0300	0,0200	-1,0500	-3,8700	-3,8700	-0,9150	-10,4120	-10,3880	-3,8830	-3,8440	-0,6620	-0,7010	-	-10,4120	v	
	39	-1,6700	-1,9800	0,0200	-0,0700	0,0500	-2,3380	-2,9940	-1,9940	-5,2280	-5,1320	-3,0850	-2,9290	-1,4120	-1,5680	-	-5,2280	v	
	43	3,4000	-1,9800	0,0200	-0,0600	0,0400	4,7600	3,0900	4,0900	0,8640	0,9440	3,0120	3,1420	3,1360	3,0080	4,0900	-	v	
	47	1,4200	-5,9400	-0,0300	0,0600	-0,0400	1,9880	-1,2660	1,6890	-7,7520	-7,8320	-1,1880	-1,3180	1,2000	1,3300	-	-7,8320	v	
	51	-1,6700	-9,8600	-0,1500	0,2000	-0,1500	-2,3380	-6,9340	-2,0790	-17,6200	-17,9000	-6,6740	-7,1290	-1,7630	-1,3080	-	-17,9000	v	

Keterangan Tabel 4.8

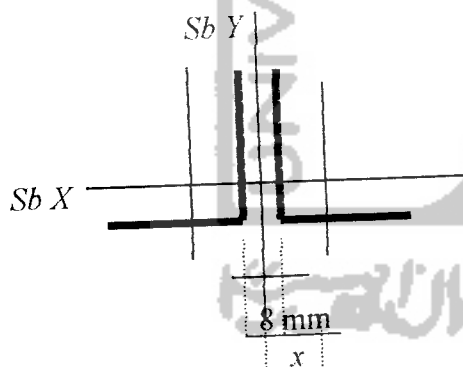
- [1] Kuda-kuda yang ditinjau
- [2] Nomer batang
- [3] ND = Gaya batang akibat beban mati
- [4] NL = Gaya batang akibat beban hidup atap
- [5] NH = Gaya batang akibat beban hujan
- [6] NWki = Gaya batang akibat beban angin kiri
- [7] NWka = Gaya batang akibat beban angin kanan
- [8] Nu.1 = 1,4ND
- [9] Nu.2 = 1,2ND + 1,6NL
- [10] Nu.3 = 1,2ND + 1,6NH
- [11] Nu.4 = 1,2ND + 1,6NL + 0,8NWki
- [12] Nu.4 = 1,2ND + 1,6NL + 0,8NWka
- [13] Nu.6 = 1,2ND + 1,3NWki + 0,5NL
- [14] Nu.6 = 1,2ND + 1,3NWka + 0,5NL
- [15] Nu.8 = 0,9ND - 1,3NWki
- [16] Nu.8 = 0,9ND - 1,3NWka
- [17] Nu Tarik = Gaya batang tarik kombinasi maksimum
- [18] Nu Tekan = Gaya batang tekan kombinasi maksimum
- [19] Jenis batang: a = batang atas, b = batang bawah  
d = batang diagonal, v = batang vertikal  
vp = batang pertemuan antar kuda-kuda

#### 4.3.4 Pendimensionian Kuda-Kuda Rangka Baja

Sebagai contoh perhitungan ditinjau pada pendimensionian rangka baja kuda-kuda K1, untuk pendimensionian batang tekan adalah batang atas (a) nomor 5, dan untuk pendimensionian batang tarik adalah batang bawah (b) nomor 20.

##### 1. Pendimensionian Batang Tekan (Batang atas (a) Nomor: 5)

- $L = 2197$  mm
- $N_u = 187,2000$  kN
- di coba profil 2L 70.70.7  
data-data profil:  
 $A_{profil} = 940$  mm<sup>2</sup>  
 $r_x = r_y = 21,24$  mm  
 $I_x = I_y = 424000$  mm<sup>4</sup>
- Cek angka perbandingan kelangsingan batang tekan:  $L_k/r < 200$   
 $L_k = k.L = 1. 2197 = 2197$  mm  
mencari  $r$  pilih yang terkecil untuk profil 2L 70.70.7



Gambar 4.23 Penampang profil 2L 70.70.7

$$x = e + tp/2 = 19,7 + 8/2 = 23,7 \text{ mm}$$

$$\begin{aligned} I_y \text{ dua profil} &= 2 (I_y + A.x^2) \\ &= 2.(42,4.10^4 + 940.23,7^2) \\ &= 1903977,2 \text{ mm}^4 \end{aligned}$$

$$r_y = \sqrt{I_y/A_g} = \sqrt{(1903977,2/(2.940))} = 31,45 \text{ mm}$$

$$I_x \text{ dua profil} = 2.I_x = 2.424000 = 848000 \text{ mm}^4$$

$$r_x = \sqrt{I_x/A_g} = \sqrt{(848000/(2.940))} = 21,24 \text{ mm}$$

di pilih  $r$  terkecil  $r = r_x = 21,24$  mm



$$L_k/r_x = 2197/21,24 = 103,437 < 200 \quad \text{- aman-}$$

- parameter kelangsingan batang tekan

$$\lambda_c = \frac{1}{\pi} \frac{L_k}{r} \sqrt{\frac{f_y}{E}}$$

$$\begin{aligned} \lambda_c &= \frac{1}{\pi} \frac{2197}{21,24} \sqrt{\frac{240}{200000}} \\ &= 1,141 \end{aligned}$$

untuk  $0,25 < (\lambda_c = 1,141) < 1,2$

maka  $\omega = 1,43 / (1,6 - 0,67 \cdot \lambda_c)$

$$= 1,43 / (1,6 - 0,67 \cdot 1,141) = 1,711$$

- Kuat tekan nominal

$$\begin{aligned} \phi N_n &= \phi A_g (f_y / \omega) \\ &= 0,87 \cdot 2.940 \cdot (240 / 1,711) \\ &= 224165,6 \text{ N} = 224,1656 \text{ kN} \end{aligned}$$

$(\phi N_n = 224,1656 \text{ kN}) > (N_u = 187,2000 \text{ kN}) \quad \text{- aman-}$

## 2. Pendimensian Batang Tarik (Batang bawah (b) Nomor: 20)

- $L = 2023 \text{ mm}$
- $N_u = 179,4840 \text{ kN}$
- dicoba profil 2L50.50.5

data-data profil:

$$A_{profil} = 480 \text{ mm}^2$$

$$r = r_x = 15,1 \text{ mm (jari-jari girasi terkecil)}$$

- Cek angka perbandingan kelangsingan batang tarik

$$L/r = 2023/15,1 = 133,974 < 240 \quad \text{- aman-}$$

- Kuat tarik nominal batang tarik

$$\begin{aligned} \phi N_n &= \phi A_g f_y \\ &= 0,90 \cdot (2.480) \cdot 240 \\ &= 207360 \text{ N} = 207,3600 \text{ kN} \end{aligned}$$

$(\phi N_n = 207,3600 \text{ kN}) > (N_u = 179,4840 \text{ kN}) \quad \text{-aman-}$

Dengan cara yang sama dapat dihitung pendimensian seluruh rangka baja kuda-kuda disajikan pada Tabel 4.9.

Tabel 4.9 Pendimensian Rangka Baja Kuda-Kuda

Kuda-Kuda	No.	Pan-jang (mm)	N <sub>v</sub> tarik (kN)	N <sub>v</sub> tekan (kN)	Profil	A (mm <sup>2</sup> )	r <sub>x</sub> (mm)	Analisis Batang Tekan						Analisis Batang Tarik		Ket.	Jenis Batang	
								L/r <sub>x</sub> <200	λ <sub>c</sub>	φ <sub>1</sub>	φ <sub>2</sub>	φN <sub>n1</sub> (kN)	φN <sub>n2</sub> (kN)	L/r <sub>x</sub> <240	φN <sub>n</sub> (kN)			
																		[9]
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	
K1	1	1709	16,8800	-	2L 70 70 7	940	21,24	-	-	-	-	-	-	80,461	406,0800	Aman	a	
	2	2197	-	-104,3880	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	3	2197	-	-162,1840	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	4	2197	-	-183,1520	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	5	2197	-	-187,2000	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	6	2197	-	-178,0760	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	7	2197	-	-162,2560	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	8	2197	-	-162,4880	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	9	2197	-	-172,9160	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	10	2197	-	-177,6000	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	11	2197	-	-170,5680	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	12	2197	-	-150,6880	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	13	2197	-	-97,4600	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	14	1709	15,8960	-	-	2L 70 70 7	940	21,24	-	-	-	-	-	-	80,461	406,0800	Aman	a
	15	1400	-	-14,2160	2L 50 50 5	480	15,1	92,715	1,022	1,563	-	125,3154	-	-	-	-	Aman	b
	16	2023	-	-25,4040	2L 50 50 5	480	15,1	133,974	1,477	-	2,728	-	71,7913	-	-	-	Aman	b
	17	2023	105,4760	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	18	2023	157,8880	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	19	2023	176,4680	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	20	2023	179,4840	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	21	2023	170,0800	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	22	2023	163,3840	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	23	2023	166,9960	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	24	2023	159,5080	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	25	2023	138,6320	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	26	2023	89,3400	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,3600	Aman	b
	27	2023	-	-14,4920	2L 50 50 5	480	15,1	133,974	1,477	-	2,728	-	71,7913	-	-	-	Aman	b
	28	1400	-	-13,0160	2L 50 50 5	480	15,1	92,715	1,022	1,563	-	125,3154	-	-	-	-	Aman	b
	29	980	-	-83,3200	O 76,3,3,2	734,9	25,9	37,838	0,417	1,083	-	138,4357	-	-	-	-	Aman	vp
	33	1653	-	-29,6800	O 76,3,3,2	734,9	25,9	63,822	0,704	1,267	-	118,3099	-	-	-	-	Aman	vp
	37	2326	-	-3,3410	O 76,3,3,2	734,9	25,9	89,807	0,990	-	1,226	-	122,3058	-	-	-	Aman	vp
	41	3000	152,6440	-	-	O 76,3,3,2	734,9	25,9	-	-	-	-	-	-	115,830	158,7384	Aman	vp
	45	2326	-	-6,4220	O 76,3,3,2	734,9	25,9	89,807	0,990	-	1,226	-	122,3058	-	-	-	Aman	vp
	49	1653	-	-28,7120	O 76,3,3,2	734,9	25,9	63,822	0,704	1,267	-	118,3099	-	-	-	-	Aman	vp
	53	980	-	-78,3040	O 76,3,3,2	734,9	25,9	37,838	0,417	1,083	-	138,4357	-	-	-	-	Aman	vp
	30	1801	98,4240	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	133,407	185,7600	Aman	d
	32	1842	47,8200	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	136,444	185,7600	Aman	d
	34	1942	17,7880	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	143,852	185,7600	Aman	d
	36	2092	5,9650	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	154,963	185,7600	Aman	d
	38	2282	-	-10,5040	2L 45 45 5	430	13,5	169,037	1,864	-	4,343	-	40,3993	-	-	-	Aman	d
	40	2503	-	-18,0120	2L 45 45 5	430	13,5	185,407	2,044	-	5,225	-	33,5802	-	-	-	Aman	d
	42	2503	-	-19,4440	2L 45 45 5	430	13,5	185,407	2,044	-	5,225	-	33,5802	-	-	-	Aman	d
	44	2282	-	-13,0550	2L 45 45 5	430	13,5	169,037	1,864	-	4,343	-	40,3993	-	-	-	Aman	d
	46	2092	9,2020	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	154,963	185,7600	Aman	d
	48	1942	20,0040	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	143,852	185,7600	Aman	d
	50	1842	46,3960	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	136,444	185,7600	Aman	d
	52	1801	92,7200	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	133,407	185,7600	Aman	d
	31	1317	-	-52,7240	2L 45 45 5	430	13,5	97,556	1,076	-	1,446	-	121,2923	-	-	-	Aman	v
	35	1990	-	-13,5720	2L 45 45 5	430	13,5	147,407	1,625	-	3,302	-	53,1249	-	-	-	Aman	v
	39	2663	12,5160	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	197,259	185,7600	Aman	v
	43	2663	14,0840	-	-	2L 45 45 5	430	13,5	-	-	-	-	-	-	197,259	185,7600	Aman	v
47	1990	-	-15,4440	2L 45 45 5	430	13,5	147,407	1,625	-	3,302	-	53,1249	-	-	-	Aman	v	
51	1317	-	-49,2200	2L 45 45 5	430	13,5	97,556	1,076	-	1,446	-	121,2923	-	-	-	Aman	v	
K2	1	1709	16,8320	-	2L 70 70 7	940	21,24	-	-	-	-	-	-	80,461	406,08	Aman	a	
	2	2197	-	-99,2120	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	3	2197	-	-153,8900	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	4	2197	-	-172,8680	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	5	2197	-	-175,3800	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	6	1800	-	-151,0120	2L 70 70 7	940	21,24	84,746	0,934	1,468	-	261,1998	-	-	-	Aman	a	
	7	1800	-	-153,9040	2L 70 70 7	940	21,24	84,746	0,934	1,468	-	261,1998	-	-	-	Aman	a	
	8	1800	-	-153,8960	2L 70 70 7	940	21,24	84,746	0,934	1,468	-	261,1998	-	-	-	Aman	a	
	9	1800	-	-146,4280	2L 70 70 7	940	21,24	84,746	0,934	1,468	-	261,1998	-	-	-	Aman	a	
	10	2197	-	-166,0920	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	11	2197	-	-160,6040	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	12	2197	-	-142,4400	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	13	2197	-	-92,0920	2L 70 70 7	940	21,24	103,437	1,141	1,711	-	224,1656	-	-	-	Aman	a	
	14	1709	16,8400	-	-	2L 70 70 7	940	21,24	-	-	-	-	-	-	80,461	406,08	Aman	a
15	1400	-	-14,1680	2L 50 50 5	480	15,1	65,913	0,727	1,285	-	298,5139	-	-	-	-	Aman	b	
16	2023	-	-23,4180	2L 50 50 5	480	15,1	133,974	1,477	-	2,728	-	71,7913	-	-	-	Aman	b	
17	2023	99,7440	-	-	2L 50 50 5	480	15,1	-	-	-	-	-	-	133,974	207,36	Aman	b	
18	2023	149,3240	-	-	2L 50 50 5	480	15,1	-	-	-	-							



Tabel 4.9 Lanjutan

Kuda-Kuda	No.	Pan-jang (mm)	Nu tarik (kN)	Nu tekan (kN)	Profil	A (mm²)	rx (mm)	Analisis Batang Tekan						Analisis Batang Tank		Ket.	Jenis Batang	
								Lk/rx <200	λc	ω1	ω2	φNn1 (kN)	φNn2 (kN)	L/rx <240	φNn (kN)			
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	
K3	42	2444	11,9860	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	181,037	146,0160	Aman	d	
	44	2444	18,6040	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	181,037	146,0160	Aman	d	
	46	2444	39,4520	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	181,037	146,0160	Aman	d	
	48	2444	46,1520	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	181,037	146,0160	Aman	d	
	50	1842	41,2280	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	136,444	146,0160	Aman	d	
	52	1801	83,4160	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	133,407	146,0160	Aman	d	
	31	1317	-	-46,4120	2L 45 45.5	338	13,5	97,556	1,076	1,626	-	-	84,794	-	97,556	-	Aman	v
	35	1653	-	-29,4640	2L 45 45.5	338	13,5	122,444	1,350	-	2,279	-	-	60,52	122,444	-	Aman	v
	39	1653	-	-10,9800	2L 45 45.5	338	13,5	122,444	1,350	-	2,279	-	-	60,52	122,444	-	Aman	v
	43	1653	-	-10,9800	2L 45 45.5	338	13,5	122,444	1,350	-	2,279	-	-	60,52	122,444	-	Aman	v
	47	1653	-	-29,4640	2L 45 45.5	338	13,5	122,444	1,350	-	2,279	-	-	60,52	122,444	-	Aman	v
51	1317	-	-44,3560	2L 45 45.5	338	13,5	97,556	1,076	1,626	-	-	84,794	-	97,556	-	Aman	v	
K4	1	1709	15,0520	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	126,593	185,7600	Aman	a	
	2	1800	5,5320	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	3	1800	4,1840	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	4	1800	0,8440	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	5	1800	2,4900	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	6	1800	0,9140	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	7	1800	3,4800	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	8	1800	3,4800	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	9	1800	1,0690	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	10	1800	1,4690	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	11	1800	0,9600	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	12	1800	3,9600	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	13	1800	5,3000	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	a	
	14	1709	15,0440	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	126,593	185,7600	Aman	a	
	15	1400	-	-6,6720	2L 45 45.5	430	13,5	103,704	1,143	1,715	-	-	102,3020	-	-	-	Aman	b
	16	1800	-	-12,4120	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	17	1800	-	-5,8720	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	18	1800	-	-4,0240	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	19	1800	-	-1,1590	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	20	1800	-	-2,2040	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	21	1800	-	-0,9910	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	22	1800	0,9200	-	2L 45 45.5	430	13,5	-	-	-	-	-	-	133,333	185,7600	Aman	b	
	23	1800	-	-2,2680	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	24	1800	-	-1,3930	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	25	1800	-	-4,0400	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	26	1800	-	-5,8880	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	27	1800	-	-12,6440	2L 45 45.5	430	13,5	133,333	1,470	-	2,702	-	-	64,9321	-	-	Aman	b
	28	1400	-	-12,6720	2L 45 45.5	430	13,5	103,704	1,143	1,715	-	-	102,3020	-	-	-	Aman	b
	29	980	-	-24,5040	O 76,3.3,2	734,9	25,9	37,838	0,417	1,083	-	-	138,4357	-	-	-	Aman	vp
	33	980	-	-11,0640	O 76,3.3,2	734,9	25,9	37,838	0,417	1,083	-	-	138,4357	-	-	-	Aman	vp
	37	980	-	-10,4160	O 76,3.3,2	734,9	25,9	37,838	0,417	1,083	-	-	138,4357	-	-	-	Aman	vp
	41	980	-	-9,3720	O 76,3.3,2	734,9	25,9	37,838	0,417	1,083	-	-	138,4357	-	-	-	Aman	vp
	45	980	-	-10,4080	O 76,3.3,2	734,9	25,9	37,838	0,417	1,083	-	-	138,4357	-	-	-	Aman	vp
	49	980	-	-11,0880	O 76,3.3,2	734,9	25,9	37,838	0,417	1,083	-	-	138,4357	-	-	-	Aman	vp
	53	980	-	-24,7760	O 76,3.3,2	734,9	25,9	37,838	0,417	1,083	-	-	138,4357	-	-	-	Aman	vp
	30	2049	7,6400	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	32	2049	2,1290	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	34	2049	3,7640	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	36	2049	-	-1,9560	2L 45 45.5	338	13,5	151,778	1,674	-	3,501	-	-	39,3885	-	-	Aman	d
	38	2049	2,2440	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	40	2049	-	-3,6280	2L 45 45.5	338	13,5	151,778	1,674	-	3,501	-	-	39,3885	-	-	Aman	d
	42	2049	-	-3,6040	2L 45 45.5	338	13,5	151,778	1,674	-	3,501	-	-	39,3885	-	-	Aman	d
	44	2049	2,2230	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	46	2049	-	-2,0040	2L 45 45.5	338	13,5	151,778	1,674	-	3,501	-	-	39,3885	-	-	Aman	d
	48	2049	3,8200	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	50	2049	2,0640	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	52	2049	7,6560	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	151,778	146,0160	Aman	d	
	31	980	-	-17,8920	2L 45 45.5	338	13,5	72,593	0,800	1,344	-	-	102,5794	-	-	-	Aman	v
	35	980	-	-10,4120	2L 45 45.5	338	13,5	72,593	0,800	1,344	-	-	102,5794	-	-	-	Aman	v
	39	980	-	-5,2280	2L 45 45.5	338	13,5	72,593	0,800	1,344	-	-	102,5794	-	-	-	Aman	v
	43	980	4,0900	-	2L 45 45.5	338	13,5	-	-	-	-	-	-	72,593	146,0160	Aman	v	
47	980	-	-7,8320	2L 45 45.5	338	13,5	72,593	0,800	1,344	-	-	102,5794	-	-	-	Aman	v	
51	980	-	-17,9000	2L 45 45.5	338	13,5	72,593	0,800	1,344	-	-	102,5794	-	-	-	Aman	v	

Keterangan Tabel 4.9:

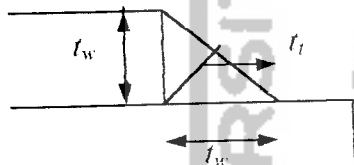
- [1] Kuda-Kuda
- [2] Nomor batang
- [3] Panjang batang
- [4] Nu tarik = gaya batang tarik
- [5] Nu tekan = gaya batang tekan
- [6] Profil terpasang
- [7] A = luas penampang profil
- [8] rx = jari-jari girasi profil terkecil
- [9]  $Lk/rx < 200$  (syarat angka perbandingan kelangsingan batang tekan)
- [10]  $\lambda c = (1/\pi) \cdot (Lk/r) \cdot (fy/E)^{0,5}$  (parameter kelangsingan batang tekan)
- [11]  $\omega 1 = 1,43 \cdot (1,6 - 0,67 \lambda c)$  untuk:  $0,25 < \lambda c < 1,2$
- [12]  $\omega 2 = 1,25 \cdot (\lambda c)^2$  untuk:  $\lambda c \geq 1,2$
- [13]  $\phi Nn1 = 0,85 \cdot Ag \cdot (fy/\omega 1)$  : kuat tekan nominal
- [14]  $\phi Nn2 = 0,85 \cdot Ag \cdot (fy/\omega 2)$  : kuat tekan nominal
- [15]  $L/rx < 240$  (syarat angka perbandingan kelangsingan batang tarik)
- [16]  $\phi Nn = 0,9 \cdot Ag \cdot fy$
- [17]  $Nu \leq \phi Nn$  : profil aman dipakai
- [18] Jenis batang: a = batang atas, b = batang bawah  
d = batang diagonal, v = batang vertikal  
vp = batang pertemuan antar kuda-kuda

### 4.3.5 Perencanaan Sambungan Titik Buhul Rangka Baja

#### a. Perencanaan Sambungan Las

Sebagai contoh perhitungan ditinjau pada sambungan las kuda-kuda K1 batang 20b dengan plat buhul 14, sebagai berikut ini:

- Profil 2L 50.50.5 dengan:
  - tegangan putus minimum baja profil,  $f_u$  profil = 370 MPa
  - Gaya batang kombinasi faktor beban maksimum,  $N_u = 179,4840$  kN
- Data-data las yang digunakan untuk menyambung:
  - mutu las, E60
  - tegangan tarik putus logam las,  $f_{uw} = 413,7$  MPa
  - tebal kaki las,  $t_w = 3$  mm, tebal rencana las,  $t_l = 2$  mm



Gambar 4.24 Ukuran las sudut

- Kuat las sudut per satuan panjang

1. Dari bahan las

$$\begin{aligned}\phi_f R_{nw} &= 0,75 \cdot t_l (0,6 \cdot f_{uw}) \\ &= 0,75 \cdot 2 \cdot (0,6 \cdot 413,7) \\ &= 372,3300 \text{ N/mm}\end{aligned}$$

2. Dari bahan dasar profil

$$\begin{aligned}\phi_f R_{nw} &= 0,75 \cdot t_l (0,6 \cdot f_u) \\ &= 0,75 \cdot 2 \cdot (0,6 \cdot 370) \\ &= 333,0000 \text{ N/mm}\end{aligned}$$

dipilih kuat las sudut per satuan panjang yang terkecil

$$\phi_f R_{nw} = 333,0000 \text{ N/mm}$$

- Tentukan panjang las ( $l_n$ )

$$N_u = \phi_f R_{nw} \cdot l_n$$

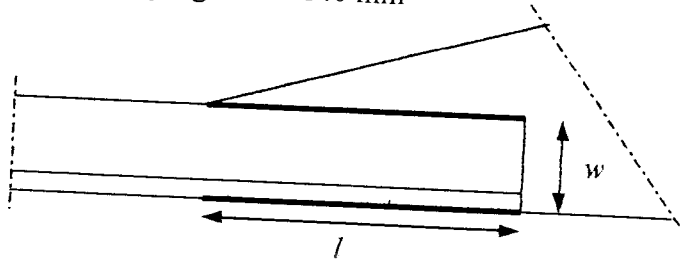
$$179,4840 = 333 \cdot 10^{-3} \cdot l_n$$

$$l_n = 538,99 \text{ mm}$$

Panjang las pada masing-masing profil, tiap sisi:

$$l = l_w/4 = 538,99/4 = 134,75 \text{ mm}$$

dipakai panjang las  $l = 140 \text{ mm}$



Gambar 4.25 Panjang sambungan las

- Kasus gaya tarik yang disalurkan ke sebuah komponen struktur pelat dengan pengelasan sepanjang kedua sisi pada ujung pelat, dengan  $l > w$ :

untuk  $l \geq 2w$       $U = 1,0$

untuk  $2w > l \geq 1,5w$       $U = 0,87$

untuk  $1,5w > l \geq w$       $U = 0,75$

dengan:  $l$  = panjang pengelasan, mm

$w$  = lebar pelat (jarak antar sumbu pengelasan), mm

Pada perhitungan,

$$l/w = 140/50 = 2,8 \text{ dengan syarat diatas } U=1,0$$

- Gaya tarik nominal las

$$\phi_f \cdot N_{mw} = 4 \cdot 0,75 \cdot A_{\text{netto las}} \cdot (0,6 f_u)$$

dengan:

$$\phi_f \cdot N_{mw} = \text{gaya tarik nominal las terfaktor (N)}$$

$$A_{\text{netto las}} = l \cdot t_f \cdot U$$

$f_u$  = tegangan putus minimum bahan pelat (MPa)

$$\phi_f \cdot N_{mw} = 4 \cdot 0,75 \cdot (140 \cdot 2) \cdot 1 \cdot (0,6 \cdot 370)$$

$$= 186480 \text{ N}$$

$$= 186,4800 \text{ kN}$$

$$(\phi_f \cdot N_{mw} = 186,4800 \text{ kN}) > (N_u = 179,4840 \text{ kN}) \quad \text{-aman-}$$

Dengan cara yang sama dapat dihitung untuk semua perencanaan sambungan las rangka baja kuda-kuda, disajikan pada Tabel 4.10.

Tabel 4.10 Perencanaan Sambungan Las Kuda-Kuda

Kuda-Kuda	No. J	No. B	Profil	Jenis	$N_u$ (kN)	$t_f$ (mm)	$f_{up}$ (MPa)	Mutu fas	$f_{uw}$ (MPa)	$t_w$ (mm)	$t_t$ (mm)	$\phi R_{nw1}$ (N/mm)	$\phi R_{nw2}$ (N/mm)	$I_n$ (mm)	$I_n/4$ (mm)	$I$ (mm)	$w$ (mm)	$I/w$	$U$	$\phi N_n$ (kN)	Ket	
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]	[20]	[21]	[22]	
K1	1	15	2L70.70.7a 2L50.50.5b	a b	16,8800 14,2160	7 5	370 370	E60 E60	413,7 413,7	3 3	2 2	372,3300 372,3300	333,0000 333,0000	50,69 42,69	12,67 10,67	125 125	70 50	1,79 2,50	0,87 1	144,8550 166,5000	aman aman	
	2	29	2L70.70.7a O76.3.3.2vp 2L45.45.5d	a vp d	16,8800 104,3880 83,3200 98,4240	7 7 3,2 5	370 370 370 370	- - E60 E60	- - 413,7 413,7	- - 3 3	- - 2 2	- - 372,3300 372,3300	- - 333,0000 333,0000	- - - 250,21	- - - 62,55	- - - 130	70 50 76,3	1,79 2,50 1,70	0,87 - 0,87	144,8550 - 150,6492	aman - aman	
	3	31	2L70.70.7a 2L45.45.5v 2L45.45.5d	a v d	104,3880 162,1840 52,7240 47,8200	7 7 5 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	313,48 487,04 121,76 158,33	78,37 121,76 140 70	125 140 70 45	70 2,00 2,00 2,78	0,87 1 1 1	144,8550 186,4800 166,5000 166,5000	aman aman aman aman		
	4	33	2L70.70.7a O76.3.3.2vp 2L45.45.5d	a vp d	162,1840 183,1520 29,6800 17,7880	7 7 3,2 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	143,60 - - 89,13	35,90 - - 22,28	125 - - 125	45 - - 76,3	2,78 - - 1,64	0,87 - - 0,87	166,5000 - - 144,8550	aman - - aman	
	5	35	2L70.70.7a 2L45.45.5v 2L45.45.5d	a v d	183,1520 187,2000 13,5720 5,9650	7 7 5 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	550,01 562,16 40,76 17,91	137,50 140,54 10,19 4,48	145 145 125 125	70 70 45 45	2,07 2,07 2,07 2,78	1 1 1 1	193,1400 193,1400 166,5000 166,5000	aman aman aman aman	
	6	37	2L70.70.7a O76.3.3.2vp 2L45.45.5d	a vp d	187,2000 178,0760 3,3410 10,5040	7 7 3,2 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	10,03 - - 10,03	2,51 - - 2,51	125 - - 125	76,3 - - 76,3	1,64 - - 1,64	0,87 - - 0,87	144,8550 - - 144,8550	aman - - aman	
	7	39	2L70.70.7a 2L45.45.5v 2L45.45.5d	a v d	178,0760 162,2560 12,5160 18,0120	7 7 5 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	534,76 487,26 37,59 54,09	133,69 121,81 9,40 13,52	140 140 125 125	70 70 45 45	2,00 2,00 2,78 2,78	1 1 1 1	186,4800 186,4800 166,5000 166,5000	aman aman aman aman	
	8	41	2L70.70.7a O76.3.3.2vp	a vp	162,2560 162,4880 152,6440	7 7 3,2	370 370 370	E60 E60 E60	413,7 413,7 413,7	3 3 3	2 2 2	372,3300 372,3300 372,3300	333,0000 333,0000 333,0000	458,39 - - 458,39	114,60 - - 114,60	145 - - 145	76,3 - - 76,3	1,90 - - 1,90	0,87 - - 0,87	168,0318 - - 168,0318	aman - - aman	
	9	16	2L50.50.5b 2L50.50.5b O76.3.3.2vp	b b vp	14,2160 25,4040 83,3200	5 5 3,2	370 370 370	E60 E60 E60	413,7 413,7 413,7	3 3 3	2 2 2	372,3300 372,3300 372,3300	333,0000 333,0000 333,0000	250,21 76,29 - - 250,21	62,55 19,07 - - 62,55	130 125 - - 130	76,3 50 - - 76,3	1,70 2,50 - - 1,70	0,87 1 - - 0,87	150,6492 166,5000 - - 150,6492	aman aman - - aman	
	10	30	2L50.50.5b 2L45.45.5d 2L45.45.5v	b d v	105,4760 98,4240 52,7240	5 5 5	370 370 370	E60 E60 E60	413,7 413,7 413,7	3 3 3	2 2 2	372,3300 372,3300 372,3300	333,0000 333,0000 333,0000	316,74 295,57 - - 316,74	79,19 73,89 - - 79,19	125 125 - - 125	50 45 - - 50	2,50 2,78 - - 2,50	1 1 - - 1	166,5000 166,5000 - - 166,5000	aman aman - - aman	
	11	17	2L50.50.5b 2L50.50.5b 2L45.45.5d O76.3.3.2vp	b b d vp	105,4760 157,8880 47,8200 29,6800	5 5 5 3,2	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	158,33 - - - 158,33	39,58 - - - 39,58	125 - - - 125	45 - - - 45	2,78 - - - 2,78	1 - - - 1	166,5000 - - - 166,5000	aman - - - aman	
	12	18	2L50.50.5b 2L50.50.5b 2L45.45.5d 2L45.45.5v	b b d v	157,8880 176,4680 17,7880 13,5720	5 5 5 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	89,13 474,14 529,93 53,42	22,28 118,53 132,48 13,35	125 130 140 125	76,3 50 50 45	1,64 2,60 2,80 2,78	0,87 1 1 1	144,8550 173,1600 186,4800 166,5000	aman aman aman aman	
	13	19	2L50.50.5b 2L50.50.5b 2L45.45.5d O76.3.3.2vp	b b d vp	176,4680 179,4840 5,9650 3,3410	5 5 5 3,2	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	40,76 - - - 40,76	10,19 - - - 10,19	125 - - - 125	45 - - - 45	2,78 - - - 2,78	1 - - - 1	166,5000 - - - 166,5000	aman - - - aman	
	14	20	2L50.50.5b 2L50.50.5b 2L45.45.5d 2L45.45.5v	b b d v	179,4840 170,0800 10,5040 12,5160	5 5 5 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	10,03 538,99 510,75 31,54	2,51 134,75 127,69 7,89	125 140 130 125	76,3 50 50 45	1,64 2,80 2,70 2,78	0,87 1 1 1	144,8550 186,4800 179,8200 166,5000	aman aman aman aman	
	15	21	2L50.50.5b 2L50.50.5b 2L45.45.5d O76.3.3.2vp 2L45.45.5d	b b d vp d	170,0800 163,3840 18,0120 152,6440 19,4440	5 5 5 3,2 5	370 370 370 370 370	E60 E60 E60 E60 E60	413,7 413,7 413,7 413,7 413,7	3 3 3 3 3	2 2 2 2 2	372,3300 372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000 333,0000	37,59 - - - - 37,59	9,40 - - - - 9,40	125 - - - - 125	45 - - - - 45	2,78 - - - - 2,78	1 - - - - 1	166,5000 - - - - 166,5000	aman - - - - aman	
	K2	1	15	2L70.70.7a 2L50.50.5b	a b	16,8320 14,1680	7 5	370 370	E60 E60	413,7 413,7	3 3	2 2	372,3300 372,3300	333,0000 333,0000	50,55 42,55	12,64 10,64	125 125	70 50	1,79 2,50	0,87 1	144,8550 166,5000	aman aman
		2	29	2L70.70.7a O76.3.3.2vp 2L45.45.5d	a vp d	16,8320 99,2120 80,1200 94,1520	7 7 3,2 5	370 370 370 370	- - E60 E60	- - 413,7 413,7	- - 3 3	- - 2 2	- - 372,3300 372,3300	- - 333,0000 333,0000	- - - 240,60	- - - 60,15	- - - 130	76,3 - - 76,3	1,70 - - 1,70	0,87 - - 0,87	150,6492 - - 150,6492	aman - - aman
		3	31	2L70.70.7a 2L45.45.5v 2L45.45.5d	a v d	99,2100 153,8900 50,3640 45,2240	7 7 5 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	297,93 462,13 151,24 135,81	74,48 115,53 37,81 33,95	130 140 70 125	1,86 2,00 2,00 2,78	0,87 1 1 1	150,6492 186,4800 166,5000 166,5000	aman aman aman aman	
		4	33	2L70.70.7a O76.3.3.2vp 2L45.45.5d	a vp d	153,8900 172,8680 27,8640 15,9640	7 7 3,2 5	370 370 370 370	E60 E60 E60 E60	413,7 413,7 413,7 413,7	3 3 3 3	2 2 2 2	372,3300 372,3300 372,3300 372,3300	333,0000 333,0000 333,0000 333,0000	135,81 - - 83,68	33,95 - - 20,92	125 - - 125	45 - - 76,3	2,78 - - 1,64	1 - - 0,87	166,5000 - - 144,8550	aman - - aman

Tabel 4.10. Lanjutan.

Kuda-Kuda	No. J	No. B	Profil	Je-nis	Nu (kN)	t <sub>f</sub> (mm)	f <sub>uP</sub> (MPa)	Mutu las	f <sub>uw</sub> (MPa)	t <sub>w</sub> (mm)	t <sub>t</sub> (mm)	φR <sub>nw1</sub> (N/mm)	φR <sub>nw2</sub> (N/mm)	I <sub>n</sub> (mm)	I <sub>n/4</sub> (mm)	I (mm)	w (mm)	I/w	U	φN <sub>n</sub> (kN)	Ket	
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]	[20]	[21]	[22]	
K2	5	4	2L70.70.7a	a	172,8680	7	370	E60	413,7	3	2	372,3300	333,0000	519,12	129,78	140	70	2,00	1	186,4800	aman	
		5	2L70.70.7a	a	175,3800	7	370	E60	413,7	3	2	372,3300	333,0000	526,67	131,67	140	70	2,00	1	186,4800	aman	
		35	2L45.45.5v	v	11,5800	5	370	E60	413,7	3	2	372,3300	333,0000	34,77	8,69	125	45	2,78	1	166,5000	aman	
		36	2L45.45.5d	d	4,5440	5	370	E60	413,7	3	2	372,3300	333,0000	13,65	3,41	125	45	2,78	1	166,5000	aman	
	6	5	2L70.70.7a	a	175,4000	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		6	2L70.70.7a	a	151,0120	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		37	O76.3.3.2vp	vp	77,8800	3,2	370	E60	413,7	3	2	372,3300	333,0000	233,87	58,47	130	76,3	1,70	0,87	150,6492	aman	
		38	2L45.45.5d	d	18,1920	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	7	6	2L70.70.7a	a	151,0120	7	370	E60	413,7	3	2	372,3300	333,0000	453,49	113,37	140	70	2,00	1	186,4800	aman	
		7	2L70.70.7a	a	153,9040	7	370	E60	413,7	3	2	372,3300	333,0000	462,17	115,54	140	70	2,00	1	186,4800	aman	
		39	2L45.45.5v	v	12,4800	5	370	E60	413,7	3	2	372,3300	333,0000	37,48	9,37	125	45	2,78	1	166,5000	aman	
		40	2L45.45.5d	d	12,1680	5	370	E60	413,7	3	2	372,3300	333,0000	36,54	9,14	125	45	2,78	1	166,5000	aman	
	8	7	2L70.70.7a	a	153,8040	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		8	2L70.70.7a	a	153,8960	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	41	O76.3.3.2vp	vp	10,1080	3,2	370	E60	413,7	3	2	372,3300	333,0000	30,35	7,59	125	76,3	1,64	0,87	144,8550	aman		
		15	2L50.50.5b	b	14,1680	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	9	16	2L50.50.5b	b	23,4180	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		29	O76.3.3.2vp	vp	80,1200	3,2	370	E60	413,7	3	2	372,3300	333,0000	240,60	60,15	130	76,3	1,70	0,87	150,6492	aman	
	10	16	2L50.50.5b	b	23,4180	5	370	E60	413,7	3	2	372,3300	333,0000	70,32	17,58	125	50	2,50	1	166,5000	aman	
		17	2L50.50.5b	b	99,7440	5	370	E60	413,7	3	2	372,3300	333,0000	299,53	74,88	125	50	2,50	1	166,5000	aman	
		30	2L45.45.5d	d	94,1520	5	370	E60	413,7	3	2	372,3300	333,0000	282,74	70,68	125	45	2,78	1	166,5000	aman	
		31	2L45.45.5v	v	50,3640	5	370	E60	413,7	3	2	372,3300	333,0000	151,24	37,81	125	45	2,78	1	166,5000	aman	
	11	17	2L50.50.5b	b	99,7440	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		18	2L50.50.5b	b	149,3240	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		32	2L45.45.5d	d	45,2240	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		33	O76.3.3.2vp	vp	27,8640	3,2	370	E60	413,7	3	2	372,3300	333,0000	83,68	20,92	125	76,3	1,64	0,87	144,8550	aman	
	12	18	2L50.50.5b	b	149,3240	5	370	E60	413,7	3	2	372,3300	333,0000	448,42	112,11	130	50	2,60	1	173,1600	aman	
		19	2L50.50.5b	b	165,9360	5	370	E60	413,7	3	2	372,3300	333,0000	498,31	124,58	135	50	2,70	1	179,8200	aman	
		34	2L45.45.5d	d	15,9640	5	370	E60	413,7	3	2	372,3300	333,0000	47,94	11,98	125	45	2,78	1	166,5000	aman	
		35	2L45.45.5v	v	11,5800	5	370	E60	413,7	3	2	372,3300	333,0000	34,77	8,69	125	45	2,78	1	166,5000	aman	
	13	19	2L50.50.5b	b	165,9360	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		20	2L50.50.5b	b	149,2280	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		36	2L45.45.5d	d	4,5440	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		37	O76.3.3.2vp	vp	77,8800	3,2	370	E60	413,7	3	2	372,3300	333,0000	233,87	58,47	130	76,3	1,70	0,87	150,6492	aman	
	14	20	2L50.50.5b	b	149,2280	5	370	E60	413,7	3	2	372,3300	333,0000	448,13	112,03	130	50	2,60	1	173,1600	aman	
		21	2L50.50.5b	b	155,8120	5	370	E60	413,7	3	2	372,3300	333,0000	467,90	116,98	130	50	2,60	1	173,1600	aman	
		38	2L45.45.5d	d	18,1920	5	370	E60	413,7	3	2	372,3300	333,0000	54,63	13,66	125	45	2,78	1	166,5000	aman	
		39	2L45.45.5v	v	12,4800	5	370	E60	413,7	3	2	372,3300	333,0000	37,48	9,37	125	45	2,78	1	166,5000	aman	
	15	21	2L50.50.5b	b	155,8120	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		22	2L50.50.5b	b	151,2280	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		40	2L45.45.5d	d	12,1680	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		41	O76.3.3.2vp	vp	10,1080	3,2	370	E60	413,7	3	2	372,3300	333,0000	30,35	7,59	125	76,3	1,64	0,87	144,8550	aman	
	42	2L45.45.5d	d	13,1280	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		1	2L70.70.7a	a	16,2680	7	370	E60	413,7	3	2	372,3300	333,0000	48,85	12,21	125	70	1,79	0,87	144,8550	aman	
	15	2L50.50.5b	b	11,3860	5	370	E60	413,7	3	2	372,3300	333,0000	34,19	8,55	125	50	2,50	1	166,5000	aman		
		2	1	2L70.70.7a	a	16,2680	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	2		2L70.70.7a	a	91,2520	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	29		O76.3.3.2vp	vp	74,9520	3,2	370	E60	413,7	3	2	372,3300	333,0000	225,08	56,27	130	76,3	1,70	0,87	150,6492	aman	
30	2L45.45.5d		d	87,1280	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
3	2	2L70.70.7a	a	91,2520	7	370	E60	413,7	3	2	372,3300	333,0000	274,03	68,51	135	70	1,93	0,87	156,4434	aman		
	3	2L70.70.7a	a	140,8000	7	370	E60	413,7	3	2	372,3300	333,0000	422,82	105,71	135	70	1,93	0,87	156,4434	aman		
	31	2L45.45.5v	v	46,4120	5	370	E60	413,7	3	2	372,3300	333,0000	139,38	34,84	125	45	2,78	1	166,5000	aman		
	32	2L45.45.5d	d	41,1240	5	370	E60	413,7	3	2	372,3300	333,0000	123,50	30,87	125	45	2,78	1	166,5000	aman		
4	3	2L70.70.7a	a	140,8000	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	4	2L70.70.7a	a	148,2280	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
33	O76.3.3.2vp	vp	37,3160	3,2	370	E60	413,7	3	2	372,3300	333,0000	112,06	28,02	125	76,3	1,64	0,87	144,8550	aman			
	34	2L45.45.5d	d	46,1360	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
5	4	2L70.70.7a	a	148,2280	7	370	E60	413,7	3	2	372,3300	333,0000	445,13	111,28	140	70	2,00	1	186,4800	aman		
	5	2L70.70.7a	a	175,3640	7	370	E60	413,7	3	2	372,3300	333,0000	526,62	131,65	140	70	2,00	1	186,4800	aman		
	35	2L45.45.5v	v	29,4640	5	370	E60	413,7	3	2	372,3300	333,0000	88,48	22,12	125	45	2,78	1	166,5000	aman		
	36	2L45.45.5d	d	39,4520	5	370	E60	413,7	3	2	372,3300	333,0000	118,47	29,62	125	45	2,78	1	166,5000	aman		
6	5	2L70.70.7a	a	175,3640	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	6	2L70.70.7a	a	187,1560																		



Tabel 4.10. Lanjutan.

Kuda-Kuda	No. J	No. B	Profil	Je-nis	Nu (kN)	tr (mm)	fup (MPa)	Mutu las	fuw (MPa)	tw (mm)	tt (mm)	$\phi R_{nw1}$ (N/mm)	$\phi R_{nw2}$ (N/mm)	ln (mm)	ln/4 (mm)	l (mm)	w (mm)	l/w	U	$\phi N_n$ (kN)	Ket	
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]	[20]	[21]	[22]	
K3	9	15	2L50.50.5b		11,3860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		16	2L50.50.5b		18,1040	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		29	O76.3.3.2vp		74,9520	3,2	370	E60	413,7	3	2	372,3300	333,0000	225,08	56,27	130	76,3	1,70	0,87	150,6492	aman	
	10	16	2L50.50.5b		18,1040	5	370	E60	413,7	3	2	372,3300	333,0000	54,37	13,59	125	50	2,50	1	166,5000	aman	
		17	2L50.50.5b		88,8840	5	370	E60	413,7	3	2	372,3300	333,0000	266,92	66,73	125	50	2,50	1	166,5000	aman	
		30	2L45.45.5d		87,1280	5	370	E60	413,7	3	2	372,3300	333,0000	261,65	65,41	125	45	2,78	1	166,5000	aman	
		31	2L45.45.5v		46,4160	5	370	E60	413,7	3	2	372,3300	333,0000	139,39	34,85	125	45	2,78	1	166,5000	aman	
	11	17	2L50.50.5b		88,8840	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		18	2L50.50.5b		119,2840	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		32	2L45.45.5d		41,1240	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	12	33	O76.3.3.2vp		37,3160	3,2	370	E60	413,7	3	2	372,3300	333,0000	112,06	28,02	125	76,3	1,64	0,87	144,8550	aman	
		18	2L50.50.5b		119,2840	5	370	E60	413,7	3	2	372,3300	333,0000	358,21	89,55	125	50	2,50	1	166,5000	aman	
		19	2L50.50.5b		151,3000	5	370	E60	413,7	3	2	372,3300	333,0000	454,35	113,59	130	50	2,60	1	173,1600	aman	
		34	2L45.45.5d		46,1360	5	370	E60	413,7	3	2	372,3300	333,0000	138,55	34,64	125	45	2,78	1	166,5000	aman	
	13	35	2L45.45.5v		29,4640	5	370	E60	413,7	3	2	372,3300	333,0000	88,48	22,12	125	45	2,78	1	166,5000	aman	
		19	2L50.50.5b		151,3400	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		20	2L50.50.5b		178,5040	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		36	2L45.45.5d		39,4520	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	14	37	O76.3.3.2vp		20,6880	3,2	370	E60	413,7	3	2	372,3300	333,0000	62,13	15,53	125	76,3	1,64	0,87	144,8550	aman	
		21	2L50.50.5b		178,5040	5	370	E60	413,7	3	2	372,3300	333,0000	536,05	134,01	145	50	2,90	1	193,1400	aman	
		20	2L50.50.5b		190,2000	5	370	E60	413,7	3	2	372,3300	333,0000	571,17	142,79	155	50	3,10	1	206,4600	aman	
		38	2L45.45.5d		18,6040	5	370	E60	413,7	3	2	372,3300	333,0000	55,87	13,97	125	45	2,78	1	166,5000	aman	
		39	2L45.45.5v		10,9800	5	370	E60	413,7	3	2	372,3300	333,0000	32,97	8,24	125	45	2,78	1	166,5000	aman	
		21	2L50.50.5b		190,2000	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		22	2L50.50.5b		188,2240	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	15	40	2L45.45.5d		10,8880	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		41	O76.3.3.2vp		10,0480	3,2	370	E60	413,7	3	2	372,3300	333,0000	30,17	7,54	125	76,3	1,64	0,87	144,8550	aman	
		42	2L45.45.5d		11,9860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		1	2L70.70.7a		15,0520	7	370	E60	413,7	3	2	372,3300	333,0000	45,20	11,30	125	70	1,79	0,87	144,8550	aman	
	K4	15	15	2L50.50.5b		6,6720	5	370	E60	413,7	3	2	372,3300	333,0000	20,04	5,01	125	50	2,50	1	166,5000	aman
			2	1	2L70.70.7a		15,0520	7	370	-	-	-	-	-	-	-	-	-	-	-	-	
	2	2	2L70.70.7a		5,5320	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		29	O76.3.3.2vp		24,5040	3,2	370	E60	413,7	3	2	372,3300	333,0000	73,59	18,40	125	76,3	1,64	0,87	144,8550	aman	
		30	2L45.45.5d		7,6400	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		3	2	2L70.70.7a		5,5320	7	370	E60	413,7	3	2	372,3300	333,0000	16,61	4,15	125	70	1,79	0,87	144,8550	aman
	3	3	2L70.70.7a		4,1840	7	370	E60	413,7	3	2	372,3300	333,0000	12,56	3,14	125	70	1,79	0,87	144,8550	aman	
31		2L45.45.5v		17,8920	5	370	E60	413,7	3	2	372,3300	333,0000	53,73	13,43	125	45	2,78	1	166,5000	aman		
32		2L45.45.5d		2,1290	5	370	E60	413,7	3	2	372,3300	333,0000	6,39	1,60	125	45	2,78	1	166,5000	aman		
4	3	2L70.70.7a		4,1840	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	4	2L70.70.7a		0,8440	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	33	O76.3.3.2vp		11,0640	3,2	370	E60	413,7	3	2	372,3300	333,0000	33,23	8,31	125	76,3	1,64	0,87	144,8550	aman		
5	34	2L45.45.5d		3,7640	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	4	2L70.70.7a		0,8440	7	370	E60	413,7	3	2	372,3300	333,0000	2,53	0,63	125	70	1,79	0,87	144,8550	aman		
	5	2L70.70.7a		2,4900	7	370	E60	413,7	3	2	372,3300	333,0000	7,48	1,87	125	70	1,79	0,97	161,5050	aman		
5	35	2L45.45.5v		10,4120	5	370	E60	413,7	3	2	372,3300	333,0000	31,27	7,82	125	45	2,78	1	166,5000	aman		
	36	2L45.45.5d		1,9560	5	370	E60	413,7	3	2	372,3300	333,0000	5,87	1,47	125	45	2,78	1	166,5000	aman		
	6	5	2L70.70.7a		2,4900	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-		
6	6	2L70.70.7a		0,9140	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	37	O76.3.3.2vp		10,4160	3,2	370	E60	413,7	3	2	372,3300	333,0000	31,28	7,82	125	76,3	1,64	0,87	144,8550	aman		
	38	2L45.45.5d		2,2440	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
7	6	2L70.70.7a		0,9140	7	370	E60	413,7	3	2	372,3300	333,0000	2,74	0,69	125	70	1,79	0,87	144,8550	aman		
	7	2L70.70.7a		3,4800	7	370	E60	413,7	3	2	372,3300	333,0000	10,45	2,61	125	70	1,79	0,87	144,8550	aman		
	39	2L45.45.5v		5,2280	5	370	E60	413,7	3	2	372,3300	333,0000	15,70	3,92	125	45	2,78	1	166,5000	aman		
	40	2L45.45.5d		3,6280	5	370	E60	413,7	3	2	372,3300	333,0000	10,89	2,72	125	45	2,78	1	166,5000	aman		
8	7	2L70.70.7a		3,4800	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	8	2L70.70.7a		3,4800	7	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	41	O76.3.3.2vp		9,3720	3,2	370	E60	413,7	3	2	372,3300	333,0000	28,14	7,04	125	76,3	1,64	0,87	144,8550	aman		
9	15	2L50.50.5b		6,6720	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	16	2L50.50.5b		12,4120	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	29	O76.3.3.2vp		24,5040	3,2	370	E60	413,7	3	2	372,3300	333,0000	73,59	18,40	125	76,3	1,64	0,87	144,8550	aman		
10	16	2L50.50.5b		12,4120	5	370	E60	413,7	3	2	372,3300	333,0000	37,27	9,32	125	50	2,50	1	166,5000	aman		
	17	2L50.50.5b		5,8720	5	370	E60	413,7	3	2	372,3300	333,0000	17,63	4,41	125	50	2,50	1	166,5000	aman		
	30	2L45.45.5d		7,6400	5	370	E60	413,7	3	2	372,3300	333,0000	22,94	5,74	125	45	2,78	1	166,5000	aman		
	31	2L45.45.5v		17,8920	5	370	E60	413,7	3	2	372,3300	333,0000	53,73	13,43	125	45	2,78	1				

Tabel 4.10. Lanjutan.

Kuda-Kuda	No. J	No. B	Profil	Jenis	$N_u$ (kN)	$t_f$ (mm)	$f_{up}$ (MPa)	Mutu las	$f_{uw}$ (MPa)	$t_w$ (mm)	$t_t$ (mm)	$\phi R_{nw1}$ (N/mm)	$\phi R_{nw2}$ (N/mm)	$l_n$ (mm)	$l_n/4$ (mm)	$l$ (mm)	$w$ (mm)	$l/w$	$U$	$\phi N_n$ (kN)	Ket
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]	[20]	[21]	[22]
K4	13	19	2L50.50.5	b	1,1590	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		20	2L50.50.5	b	2,2040	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		36	2L45.45.5	d	1,9560	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		37	076.3.3.2	vp	10,4160	3,2	370	E60	413,7	3	2	372,3300	333,0000	31,28	7,82	125	76,3	1,64	0,87	144,8550	aman
	14	20	2L50.50.5	b	2,2040	5	370	E60	413,7	3	2	372,3300	333,0000	6,62	1,65	125	50	2,50	1	166,5000	aman
		21	2L50.50.5	b	0,9910	5	370	E60	413,7	3	2	372,3300	333,0000	2,98	0,74	125	50	2,50	1	166,5000	aman
		38	2L45.45.5	d	2,2440	5	370	E60	413,7	3	2	372,3300	333,0000	6,74	1,68	125	45	2,78	1	166,5000	aman
		39	2L45.45.5	v	5,2280	5	370	E60	413,7	3	2	372,3300	333,0000	15,70	3,92	125	45	2,78	1	166,5000	aman
	15	21	2L50.50.5	b	0,9910	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		22	2L50.50.5	b	0,9200	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		40	2L45.45.5	d	3,6280	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		41	076.3.3.2	vp	9,3720	3,2	370	E60	413,7	3	2	372,3300	333,0000	28,14	7,04	125	76,3	1,64	0,87	144,8550	aman
			42	2L45.45.5	d	3,6040	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-

- Keterangan Tabel 4.10:
- [1] Kuda-kuda: K1, K2, K3, dan K4
  - [2] Nomor joint titik buhul
  - [3] Nomor batang yang disambung
  - [4] Profil batang yang disambung
  - [5] Jenis batang; a = batang atas, b = batang bawah, d = batang diagonal, v = batang vertikal  
vp = batang vertikal pertemuan antar kuda-kuda
  - [6]  $N_u$  = gaya batang maksimum kombinasi faktor beban
  - [7]  $t_f$  = tebal profil
  - [8]  $f_{up}$  = tegangan putus tarik putus pelat/profil
  - [9] Mutu las
  - [10]  $f_{uw}$  = tegangan tarik putus logam las
  - [11]  $t_w$  = tebal kaki las
  - [12]  $t_t$  = tebal rencana las
  - [13]  $\phi R_{nw1} = 0,75.t_f.(0,6.f_{uw})$  (kuat las sudut, dengan  $f_{uw}$  = tegangan tarik putus logam las)
  - [14]  $\phi R_{nw2} = 0,75.t_t.(0,6.f_u)$  (kuat las sudut, dengan  $f_u$  = tegangan tarik putus pelat/profil)
  - [15]  $l_n = N_u/\phi R_{nw}$  (panjang las yang dibutuhkan)
  - [16]  $l_n/4$  = panjang las pada tiap sisi masing-masing profil
  - [17]  $l$  = panjang las terpakai pada tiap sisi masing-masing profil
  - [18]  $w$  = lebar pelat profil (jarak antar sumbu pengelasan)
  - [19]  $l/w$  = perbandingan panjang las terpakai dengan jarak antar sumbu pengelasan
  - [20] untuk  $l \geq 2.w$   $U = 1,0$   
 untuk  $2.w > l \geq 1,5w$   $U = 0,87$   
 untuk  $1,5w > l \geq w$   $U = 0,75$
  - [21]  $\phi N_n = 4.(0,75.U.l.t_f.(0,6.f_u))$  (kuat tarik las nominal terfaktor)
  - [22]  $N_u \leq \phi N_n$



## b. Perencanaan Sambungan Baut

Sebagai contoh perhitungan ditinjau pada perencanaan sambungan baut kuda-kuda K1 batang 20 b dengan plat buhul 13, sebagai berikut ini:

- Profil 2L 50.50.5 dengan:

tegangan putus minimum baja profil,  $f_u$  profil = 370 MPa

Gaya batang kombinasi faktor beban maksimum,  $N_u = 179,4840$  kN

- Data-data baut yang digunakan untuk menyambung:

mutu baut, A.307

tegangan tarik putus baut,  $f_{ub} = 410$  Mpa, diameter baut,  $d = 16$  mm.

- **Kekuatan satu baut**

### 1. Kuat geser rencana baut

$$\phi_f R_{ng} = \phi_f r_l f_u^b A_b$$

dengan

$\phi_f R_{ng}$  = kuat geser rencana baut

$\phi_f = 0,75$  (faktor reduksi kekuatan untuk fraktur)

$r_l = 0,4$  (untuk baut dengan ulir pada bidang geser)

$f_u^b = 410$  MPa (tegangan tarik putus baut)

$A_b = \frac{1}{4} \pi \cdot 16^2 = 201,06$  mm<sup>2</sup> (uas brutto penampang baut)

$$\begin{aligned} \phi_f R_{ng} &= 0,75 \cdot 0,4 \cdot 410 \cdot 200,96 \\ &= 24718,1 \text{ N} = 24,7181 \text{ kN} \end{aligned}$$

### 2. Kuat tarik rencana baut

$$\phi_f R_{n,ta} = \phi_f \cdot 0,75 \cdot f_u^b \cdot A_b$$

$$\phi_f R_{n,ta} = 0,75 \cdot 0,75 \cdot 410 \cdot 200,96$$

$$= 46346,4 \text{ N} = 46,3464 \text{ kN}$$

### 3. Kuat tumpu rencana baut

$$\phi_f R_{n,tu} = 2,4 \cdot \phi_f \cdot d_b \cdot t_f \cdot f_u$$

dengan

$\phi_f R_{n,tu}$  = Kuat tumpu rencana baut

$\phi_f = 0,75$  (faktor reduksi kekuatan untuk fraktur)

$d_b = 16$  mm (diameter baut)

$t_f$  pelat buhul = 8 mm,  $t_f < t$  pelat buhul, maka dipakai  $t_f$

4. Beban titik  $P_4$ 

- Berat sendiri:  $PK_2 + PK_4 = 1,16 + 1,00 = 2,16$  kN
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95$  kN
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69$  kN
- Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054}$  kN +  
 $P_4 = 6,424$  kN

5. Beban titik  $P_5$ 

- Berat sendiri:  $PK_2 = 1,16$  kN
- Berat penutup atap:  $0,5 \cdot 1,099 \cdot 3,6 = 1,99$  kN
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69$  kN
- Berat sagrod:  $0,022 \cdot 0,855 \cdot 2 \cdot 1,25 = \underline{0,047}$  kN +  
 $P_5 = 4,289$  kN

6. Beban titik  $P_6$ 

- Berat sendiri:  $PK_2 = 1,16$  kN  
 $P_6 = 1,16$  kN

7. Beban titik  $P_7$ 

- Berat sendiri:  $PK_2 = 1,16$  kN
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95$  kN
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69$  kN
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = \underline{0,121}$  kN +  
 $P_7 = 5,921$  kN

8. Beban titik  $P'1$ 

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 3,6 = 1,426$  kN
- Penggantung baja ( $d = 3/4''$ ) =  $0,022 \times 5,541 = \underline{0,122}$  kN +  
 $P'1 = 1,548$  kN

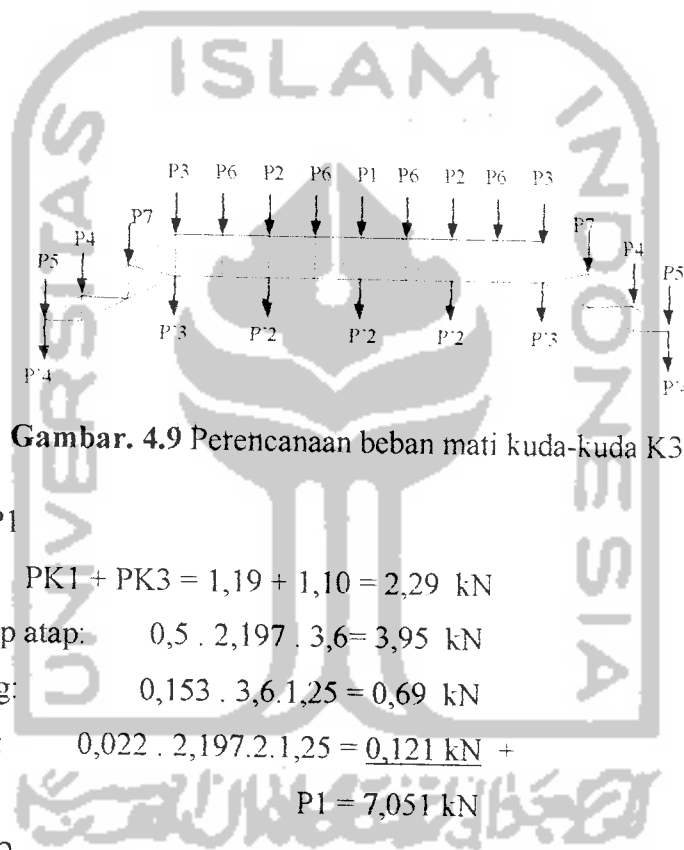
9. Beban titik  $P'2$ 

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 5,4 = 2,138$  kN
- Penggantung baja ( $d = 3/4''$ ) =  $0,022 \times 1,848 = \underline{0,041}$  kN +  
 $P'2 = 2,179$  kN

## 10. Beban titik P'4

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 1,8 = 0,713 \text{ kN}$
- Penggantung baja ( $d=3/4''$ ) =  $0,022 \times 0 = 0,000 \text{ kN}$  +  
 $P'4 = 0,713 \text{ kN}$

## c. Perencanaan Beban Mati Kuda-Kuda K3



Gambar. 4.9 Perencanaan beban mati kuda-kuda K3

1. Beban titik P1
  - Berat sendiri:  $PK1 + PK3 = 1,19 + 1,10 = 2,29 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = 0,121 \text{ kN}$  +  
 $P1 = 7,051 \text{ kN}$
2. Beban titik P2
  - Berat sendiri:  $PK2 + PK3 = 1,16 + 1,1 = 2,26 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 2,197 \cdot 2 \cdot 1,25 = 0,121 \text{ kN}$  +  
 $P2 = 7,021 \text{ kN}$
3. Beban titik P3
  - Berat sendiri:  $2 \cdot P'K3 = 2 \cdot 2,28 = 4,56 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$

- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2,1,25 = \underline{0,121 \text{ kN}}$  +  
 $P3 = 9,321 \text{ kN}$

## 4. Beban titik P4

- Berat sendiri:  $PK3 + PK4 = 1,1 + 1,00 = 2,1 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 1,953 \cdot 2,1,25 = \underline{0,054 \text{ kN}}$  +  
 $P4 = 6,364 \text{ kN}$

## 5. Beban titik P5

- Berat sendiri:  $PK3 = 1,1 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 1,099 \cdot 3,6 = 1,99 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 0,855 \cdot 2,1,25 = \underline{0,047 \text{ kN}}$  +  
 $P5 = 4,229 \text{ kN}$

## 6. Beban titik P6

- Berat sendiri:  $PK3 = 1,1 \text{ kN}$   
 $P6 = 1,1 \text{ kN}$

## 7. Beban titik P7

- Berat sendiri:  $PK3 = 1,1 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 2,197 \cdot 2,1,25 = \underline{0,121 \text{ kN}}$  +  
 $P5 = 5,861 \text{ kN}$

## 8. Beban titik P'2

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 5,4 = 2,138 \text{ kN}$
- Penggantung baja (  $d = 3/4''$  )  $= 0,022 \times 1,848 = \underline{0,041 \text{ kN}}$  +  
 $P'2 = 2,179 \text{ kN}$

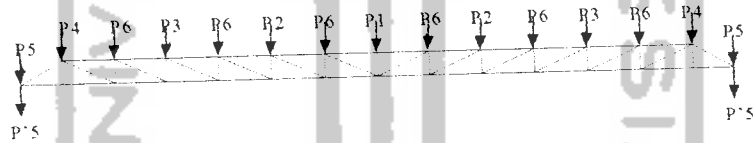
## 9. Beban titik P'3

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 5,4 \times 5,4 = 3,2076 \text{ kN}$
- Penggantung baja (d = 3/4") =  $0,022 \times 1,848 = \underline{0,041 \text{ kN}}$  +  
 $P'3 = 3,2486 \text{ kN}$

## 10. Beban titik P'4

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 3,6 \times 1,8 = 0,713 \text{ kN}$
- Penggantung baja (d = 3/4") =  $0,022 \times 0 = \underline{0,000 \text{ kN}}$  +  
 $P'4 = 0,713 \text{ kN}$

## d. Perencanaan Beban Mati Kuda-Kuda K4



Gambar. 4.10 Perencanaan pembebanan mati kuda-kuda K4

## 1. Beban titik P1

- Berat sendiri:  $PK1 + PK4 = 1,19 + 1,0 = 2,29 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +  
 $P1 = 6,454 \text{ kN}$

## 2. Beban titik P2

- Berat sendiri:  $PK2 + PK4 = 1,16 + 1,0 = 2,16 \text{ kN}$
- Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
- Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
- Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +

$$P2 = 6,424 \text{ kN}$$

3. Beban titik P3

- Berat sendiri:  $PK3 + PK4 = 1,1 + 1,0 = 2,1 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +
- $$P3 = 6,364 \text{ kN}$$

4. Beban titik P4

- Berat sendiri:  $2 \cdot PK4 = 2 \cdot 2,04 = 4,08 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,054 \text{ kN}}$  +
- $$P4 = 8,344 \text{ kN}$$

5. Beban titik P5

- Berat sendiri:  $PK4 = 1,0 \text{ kN}$
  - Berat penutup atap:  $0,5 \cdot 2,197 \cdot 3,6 = 3,95 \text{ kN}$
  - Berat gording:  $0,153 \cdot 3,6 \cdot 1,25 = 0,69 \text{ kN}$
  - Berat sagrod:  $0,022 \cdot 1,953 \cdot 2 \cdot 1,25 = \underline{0,047 \text{ kN}}$  +
- $$P5 = 5,687 \text{ kN}$$

6. Beban titik P6

- Berat sendiri:  $PK4 = 1,0 \text{ kN}$
- $$P6 = 1,0 \text{ kN}$$

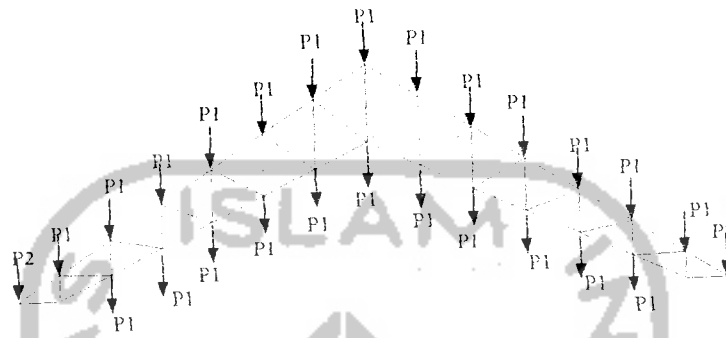
7. Beban titik P'5

- Langit-langit ( rusuk-rusuk kayu dan asbes ) :  
 $= 0,11 \times \text{Luas pembebanan} = 0,11 \times 4,86 = 0,5346 \text{ kN}$
  - Penggantung baja (  $d = 3/4''$  ) =  $0,022 \times 0 = \underline{0,000 \text{ kN}}$  +
- $$P'5 = 0,5346 \text{ kN}$$



### 3. Perencanaan Beban Hidup Kuda-Kuda

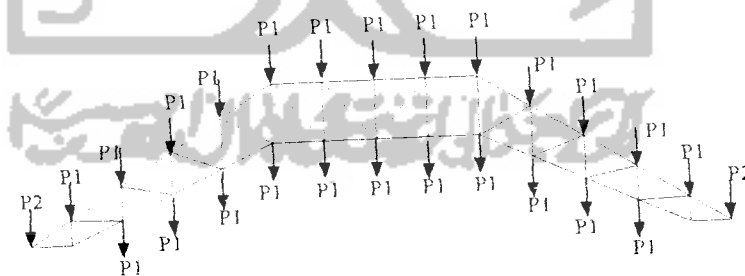
#### a. Perencanaan beban hidup kuda-kuda K1



Gambar. 4.11 Perencanaan beban hidup kuda-kuda K1

Beban hidup :  $P1 = 1 \text{ kN}$   
 $P2 = 2 \text{ kN}$

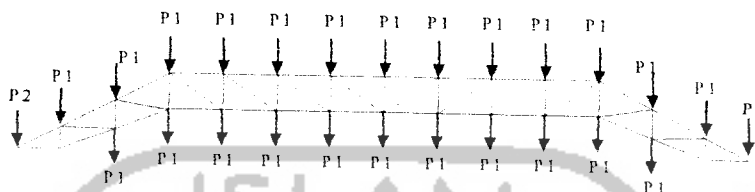
#### b. Perencanaan beban hidup kuda-kuda K2



Gambar.4.12 Perencanaan beban hidup kuda-kuda K2

Beban hidup:  $P1 = 1 \text{ kN}$   
 $P2 = 2 \text{ kN}$

### c. Perencanaan Beban Hidup Kuda-Kuda K3

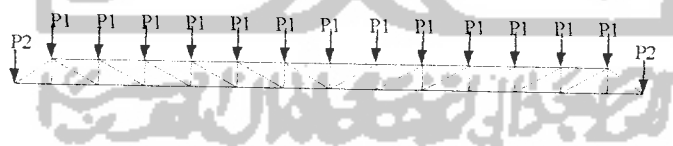


**Gambar. 4.13** Perencanaan beban hidup kuda-kuda K3

Beban hidup:  $P1 = 1 \text{ kN}$

$P2 = 2 \text{ kN}$

### d. Perencanaan beban hidup kuda-kuda K4



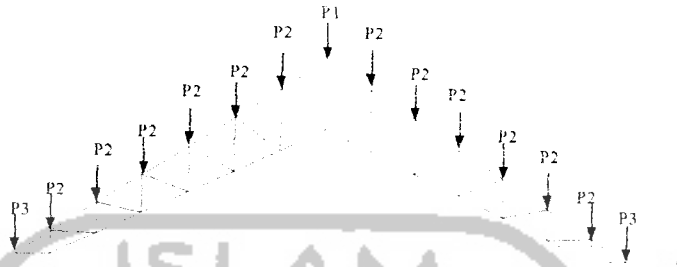
**Gambar. 4.14** Perencanaan beban hidup kuda-kuda K4

Beban hidup:  $P1 = 1 \text{ kN}$

$P2 = 2 \text{ kN}$

#### 4. Perencanaan Beban Air Hujan Kuda-Kuda

##### a. Perencanaan beban air hujan kuda-kuda K1

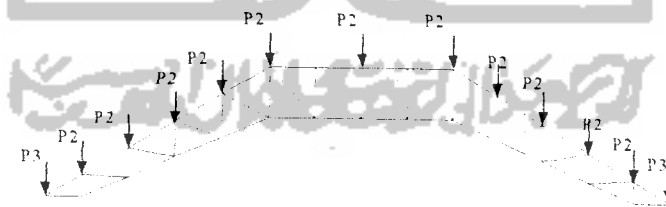


Gambar. 4.15 Perencanaan beban air hujan kuda-kuda K1

Beban air hujan :

- $P1 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6 : 2) = 0,48 \text{ kN}$
- $P2 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8 \cdot 35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

##### b. Perencanaan beban air hujan kuda-kuda K2

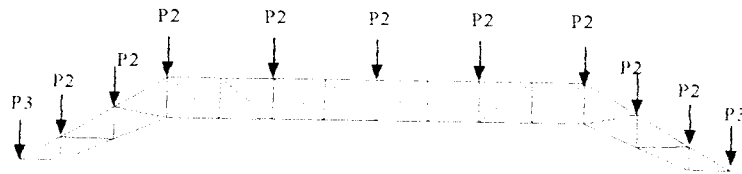


Gambar. 4.16 Perencanaan beban air hujan kuda-kuda K2

Beban air hujan :

- $P2 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8 \cdot 35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

**c. Perencanaan beban air hujan kuda-kuda K3**

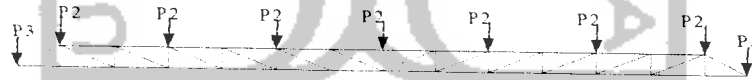


**Gambar. 4.17** Perencanaan beban air hujan kuda-kuda K3

Beban air hujan :

- $P2 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8 \cdot 35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

**d. Perencanaan beban air hujan kuda-kuda K4**



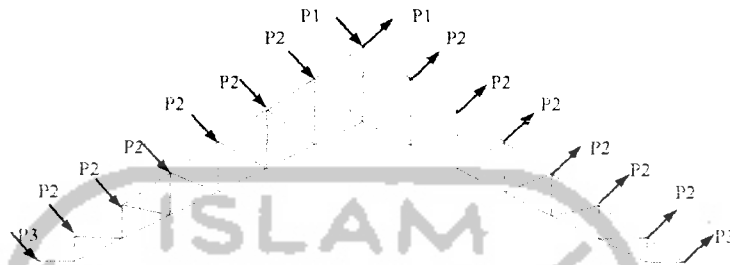
**Gambar. 4.18** Perencanaan beban air hujan kuda-kuda K4

Beban air hujan :

- $P1 = 0,01 \times (40 - 0,8 \cdot 35) \times (2,197 \times 3,6) = 0,95 \text{ kN}$
- $P3 = 0,01 \times (40 - 0,8 \cdot 35) \times (1,099 \times 3,6) = 0,58 \text{ kN}$

## 5. Perencanaan Beban Angin Kuda-Kuda

### a. Perencanaan beban angin kuda-kuda K1



**Gambar. 4.19** Perencanaan beban angin kuda-kuda K1

Beban Angin:

- P1

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6 : 2) = 0,18 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,15 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,10 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6 : 2) = 0,24 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,19 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,14 \text{ kN}$$

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = 1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

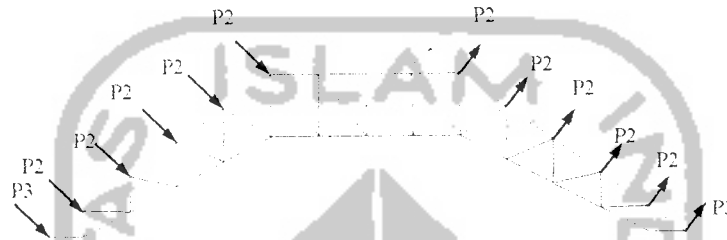
$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = 1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$

### b. Perencanaan beban angin kuda-kuda K2



**Gambar. 4.20** Perencanaan beban angin kuda-kuda K2

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = 1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = 1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$

### c. Perencanaan beban angin kuda-kuda K3



Gambar. 4.21 Perencanaan beban angin kuda-kuda K3

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = -1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

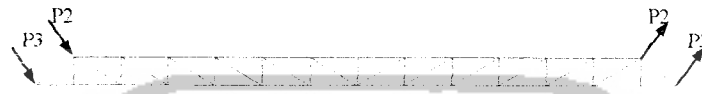
$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = -1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$

#### d. Perencanaan beban angin kuda-kuda K4



Gambar. 4.22 Perencanaan beban angin kuda-kuda K4

- P2

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 1,42 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,17 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,82 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (2,197 \times 3,6) = -1,9 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 1,55 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 1,09 \text{ kN}$$

- P3

$$\text{Tiup angin} = (0,02 \cdot 35 - 0,4) \cdot 0,6 \cdot (2,197 \times 3,6) = 0,87 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,72 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,50 \text{ kN}$$

$$\text{Hisap angin} = -0,4 \cdot 0,6 \cdot (1,099 \times 3,6) = -1,16 \text{ kN}$$

$$W_y = W \cdot \cos 35^\circ = 0,95 \text{ kN}$$

$$W_x = W \cdot \sin 35^\circ = 0,67 \text{ kN}$$

#### 4.3.2 Analisis Struktur Kuda-Kuda

Analisis struktur kuda-kuda rangka baja menggunakan program aplikasi komputer SAP 90, dengan input data-data sebagai berikut ini:

1. Nomor joint dan element, sesuai bentuk dan ukuran rangka
2. Dukungan rangka baja dianggap sendi dan roll.
3. Luas profil baja yang dipakai.



$$t_f = 5 \text{ mm (tebal pelat profil)}$$

$$f_u = 370 \text{ MPa (tegangannya tarik putus pelat profil)}$$

$$\phi_f R_n = 2,4 \cdot 0,75 \cdot 16 \cdot 5 \cdot 370$$

$$= 53280 \text{ N} = 53,2800 \text{ kN}$$

- Menghitung jumlah baut sambungan

Dari perhitungan diatas kuat rencana baut yang terkecil adalah kuat baut dalam geser, yaitu:  $\phi_f R_n = 24,7181 \text{ kN}$

$$\text{jumlah baut, } n = N_u / \phi_f R_n = 179,4840 / 24,7181 = 7,26$$

jumlah baut

$$\text{- vertikal} = n/2 = 3,63 \quad \text{jumlah baut terpasang, } n_p = 4 \text{ baut}$$

$$\text{- horizontal} = n/2 = 3,63 \quad \text{jumlah baut terpasang } n_p = 4 \text{ baut}$$

$$\text{masing-masing sayap } n_p = 2 \text{ baut}$$

- **Cek kegagalan robekan pada lubang baut**

#### 1. Pelelehan geser – retakan tarik

$$\phi_f T_{nl} = \phi (0,6 f_y A_{vg} + f_u A_{nt})$$

dengan

$\phi_f T_{nl}$  = kekuatan nominal tarik pelat profil pelelehan geser-retakan tarik

$$\phi = 0,75$$

$f_y = 240 \text{ MPa}$  (tegangannya leleh minimum)

$$A_{vg} = (s' + (n_p - 1) \cdot s) \cdot t_p$$

dengan

$s' = 30 \text{ mm}$  (jarak lubang baut dengan tepi pelat profil)

$s = 50 \text{ mm}$  (jarak antar lubang baut)

$d_p = 16 \text{ mm}$  (diameter baut)

$t_p = 5 \text{ mm}$  (tebal profil)

$n_p = 4$  (jumlah baut pada daerah yang ditinjau)

$$A_{vg} = (30 + (4 - 1) \cdot 50) \cdot 5$$

$$= 900 \text{ mm}^2 \text{ (luas bruto pelelehan geser)}$$

$f_u = 370 \text{ MPa}$  (tegangannya tarik putus profil)

$$A_{nt} = (b/2 - (d_b + 1)/2) \cdot t_f$$

dengan

$$b = 50 \text{ mm (panjang kaki profil)}$$

$$A_{nt} = (50/2 - (16+1)/2) \cdot 5$$

$$= 82,5 \text{ mm}^2 \text{ (luas bersih retakan tarik)}$$

$$\phi T_{n1} = 0,75(0,6 \cdot 240 \cdot 900 + 370 \cdot 82,5)$$

$$= 120095 \text{ N} = 120,095 \text{ kN (untuk satu profil)}$$

$$\phi T_{n1} = 120,095 \cdot 2 = 240,1875 \text{ kN (untuk dua profil)} \geq N_u = 179,4840 \text{ kN}$$

aman-

## 2. Retakan geser – pelepasan tarik

$$\phi T_{n2} = \phi (0,6 \cdot f_u \cdot A_{ns} + f_y \cdot A_{tg})$$

dengan

$\phi T_{n2}$  = kekuatan nominal tarik pelat profil retakan geser-pelepasan tarik

$$\phi = 0,75$$

$f_y = 240 \text{ MPa}$  (tegangan leleh minimum)

$$A_{ns} = (s' + (n_p - 1) \cdot s - n_p \cdot d_p) \cdot t_p$$

$$= (30 + (4 - 1) \cdot 50 - 4 \cdot 16) \cdot 5$$

$$= 560 \text{ mm}^2 \text{ (luas bersih retakan geser)}$$

$f_u = 370 \text{ MPa}$  ( tegangan tarik putus profil)

$$A_{tg} = (l_p/2) \cdot t$$

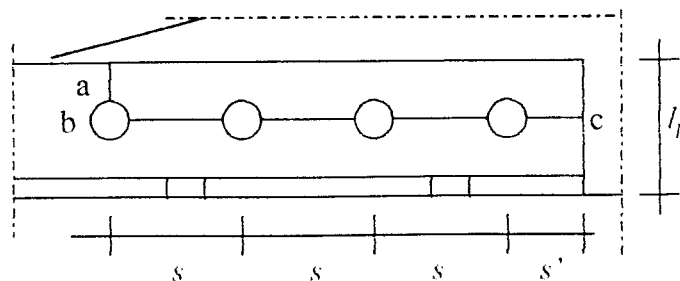
$$= (50/2) \cdot 5$$

$$= 125 \text{ mm}^2 \text{ (luas kotor pelepasan geser)}$$

$$\phi T_{n2} = 0,75(0,6 \cdot 370 \cdot 560 + 240 \cdot 125)$$

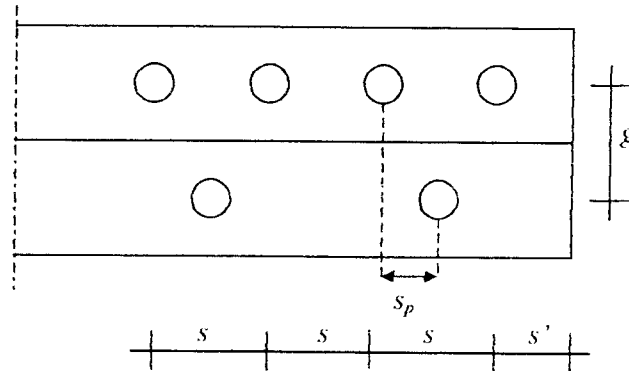
$$= 115740 \text{ N} = 115,74 \text{ kN (untuk satu profil)}$$

$$\phi T_{n2} = 115,74 \cdot 2 = 231,4800 \text{ kN (untuk dua profil)} \geq N_u = 179,4840 \text{ kN} \text{ -aman-}$$



**Gambar 4.26** Daerah yang diarsir dapat terjadi kegagalan robekan

- Cek kuat tarik profil dengan luas netto profil



Gambar 4.27 Profil siku dengan kaki-kaki yang diratakan menjadi satu bidang datar

$$\phi T_{n3} = \phi A_{netto} f_u$$

dengan,

$$\phi = 0,75$$

$$A_{netto} = l_p - 2 \cdot (d_p + 1) + (s_p^2 / 4 \cdot g)$$

$$s_p = s / 2 = 50 / 2 = 25 \text{ mm}$$

$$g = g_a + g_b - t_f$$

$$= b / 2 + b / 2 + t_f$$

$$= 50 / 2 + 50 / 2 - 5$$

$$= 45 \text{ mm}$$

$$A_{netto} = 2 \cdot ((2 \cdot 50 - 5) - 2 \cdot (16 + 1) + (25^2 / 4 \cdot 45)) \cdot 5$$

$$= 644,7222 \text{ mm}^2$$

$$\phi T_{n3} = 0,75 \cdot 644,7222 \cdot 370 \cdot 10^{-3}$$

$$= 179,6976 \text{ kN} \geq N_u = 179,4840 \text{ kN} \quad \text{-aman-}$$

Dengan cara yang sama dapat dihitung perencanaan untuk semua sathbungan baut titik buhul rangka baja seluruh kuda-kuda, yang disajikan pada Tabel 4.11.













Tabel 4.11 Lanjutan

Kuda- Kuda	No.	Profil	je- nis	Nu (kN)	Ag (mm2)	tp (mm)	fu profil (MPa)	Perencanaan, mutu, diameter, jumlah, dan jarak baut										Cek p.geser-tarik				Cek t.geser-p.tarik				Cek An. profil		Ket	
								Mutu Baut	fu (MPa)	φ <sub>sub</sub> (mm)	φ <sub>geser</sub> (mm)	φ <sub>Vn</sub> (kN)	φ <sub>Tn</sub> (kN)	φ <sub>Rn</sub> tump. (kN)	n	n/2	np	s (mm)	s' (mm)	Avg (mm2)	Ant (mm2)	φ <sub>Tn1</sub> (kN)	Ans (mm2)	Atg (mm2)	φ <sub>Tn2</sub> (kN)	An (mm2)	φ <sub>Nn</sub> (kN)		
[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]	[17]	[18]	[19]	[20]	[21]	[22]	[23]	[24]	[25]	[26]	[26]	[27]	[28]	
K4	10	16	2L50.50.5	b	12,4120	960	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		17	2L50.50.5	b	5,8720	960	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		30	2L45.45.5	d	7,6400	860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		31	2L45.45.5	v	17,8920	860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	11	17	2L50.50.5	b	5,8720	960	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,2	0,1	2	50	30	280	82,5	106,2675	230	125	121,5900	644,7222	179,6976	aman	
		18	2L50.50.5	b	4,0240	960	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,2	0,1	2	50	30	280	82,5	106,2675	230	125	121,5900	644,7222	179,6976	aman	
		32	2L45.45.5	d	2,1290	860	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,1	-	2	50	30	280	70	99,3300	230	112,5	117,0900	548,0625	153,0352	aman	
		33	O76.3.3.2	vp	11,0640	734,9	3,2	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	12	18	2L50.50.5	b	4,0240	960	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		19	2L50.50.5	b	1,1590	960	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		34	2L45.45.5	d	3,7640	860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		35	2L45.45.5	v	10,4120	860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	13	19	2L50.50.5	b	1,1590	960	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,0	0,0	2	50	30	280	82,5	106,2675	230	125	121,5900	644,7222	179,6976	aman	
		20	2L50.50.5	b	2,2040	960	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,1	0,0	2	50	30	280	82,5	106,2675	230	125	121,5900	644,7222	179,6976	aman	
		36	2L45.45.5	d	1,9560	860	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,1	-	2	50	30	280	70	99,3300	230	112,5	117,0900	548,0625	153,0352	aman	
		37	O76.3.3.2	vp	10,4160	734,9	3,2	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	14	20	2L50.50.5	b	2,2040	960	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		21	2L50.50.5	b	0,9910	960	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		38	2L45.45.5	d	2,2440	860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		39	2L45.45.5	v	5,2280	860	5	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	15	21	2L50.50.5	b	0,9910	960	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,0	0,0	2	50	30	280	82,5	106,2675	230	125	121,5900	748,8689	208,7311	aman	
		22	2L50.50.5	b	0,9200	960	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,0	0,0	2	50	30	280	82,5	106,2675	230	125	121,5900	748,8689	208,7311	aman	
		40	2L45.45.5	d	3,6280	860	5	370	A.307	410	16	24,7181	46,3464	53,2800	0,1	-	2	50	30	280	70	99,3300	230	112,5	117,0900	666,25	185,6979	aman	
		41	O76.3.3.2	vp	9,3720	734,9	3,2	370	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	42	2L45.45.5	d	3,6040	860	5	370	370	A.307	410	16	24,7181	46,3464	53,2800	0,1	-	2	50	30	280	70	99,3300	230	112,5	117,0900	666,25	185,6979	aman	

Keterangan Tabel 4.11:

- [1] Kuda-kuda
- [2] Nomor joint/itik buhul
- [3] Nomor batang
- [4] Profil batang
- [5] jenis batang, a = batang atas, b = batang bawah, d = batang diagonal, v = batang vertikal, vp = batang vertikal pertemuan
- [6] Nu = gaya batang kombinasi faktor beban maksimum
- [7] Ag = luas penampang ketor profil
- [8] tp = tebal pelat profil
- [9] fu profil = tegangan tarik putus profil
- [10] Mutu baut
- [11] fu<sub>b</sub> = tegangan tarik putus baut
- [12] d = diameter baut
- [13] φ<sub>Vn</sub> geser = kuat geser satu baut
- [14] φ<sub>Tn</sub> tarik = kuat tarik satu baut
- [15] φ<sub>Rn</sub> tumpu = kuat tumpu satu baut
- [16] n = Nu/φ<sub>Vn</sub> (jumlah baut nominal)
- [17] n/2 = jumlah baut pada profil siku sayap horizontal dan sayap vertikal
- [18] np = jumlah baut terpasang
- [19] s = jarak antar pusat lubang baut
- [20] s' = jarak dari pusat lubang baut ke tepi pelat sayap profil
- [21] Avg = (s + (np-1)s)/p (luas bruto yang mengalami pelepasan geser)
- [22] Ant = (p/2 - (d+1)/2).tp (luas bersih yang mengalami retakan tarik)
- [23] φ<sub>Tn1</sub> = 0,75.(0,6.fy.Avg + fu.Ant) (kekutan nominal terfaktor pelepasan geser-retakan tarik)
- [24] Ans = (s' + (np-1).s - np.d).tp (luas bersih yang mengalami retakan geser)
- [25] Atg = (p/2).tp (luas bruto yang mengalami pelepasan tarik)
- [26] φ<sub>Tn2</sub> = 0,75.(0,6.fu.Ans + fy.Atg) (kekutan nominal terfaktor retakan geser-pelepasan tarik)
- [27] Ant = Ag - n.d.t + ∑(sp<sup>2</sup>/4g) (luas penampang netto profil)
- [28] φ<sub>Nn</sub> = 0,75.Anetto.fup (kuat tarik nominal terfaktor profil dengan Anetto)