

LAMPIRAN

REAKTOR (R)

Tugas : Mereaksikan diethanol amine menjadi morpholine dengan katalis oleum

dengan kecepatan umpan = 100.000 Kg/jam

Jenis : Reaktor Alir Tangki Berpengaduk

Kondisi Operasi : Tekanan : 10 atm

Suhu : 190 °C

NERACA MASSA :

Umpan total masuk :

$$\text{C}_4\text{H}_{11}\text{NO}_2 = 155,0903 \text{ Kgmol/j} = 16284,4824 \text{ Kg/j}$$

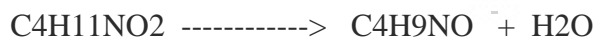
$$\text{H}_2\text{O} = 9,1383 \text{ Kgmol/j} = 164,4897 \text{ Kg/j}$$

$$\text{H}_2\text{SO}_4 = 218,8720 \text{ Kgmol/j} = 21449,4590 \text{ Kg/j}$$

$$\text{SO}_3 = 67,0296 \text{ Kgmol/j} = 5362,3647 \text{ Kg/j}$$

$$\text{Jumlah} = 450,1302 \text{ Kgmol/j} = 43260,7969 \text{ Kg/j}$$

Reaksi yang terjadi :



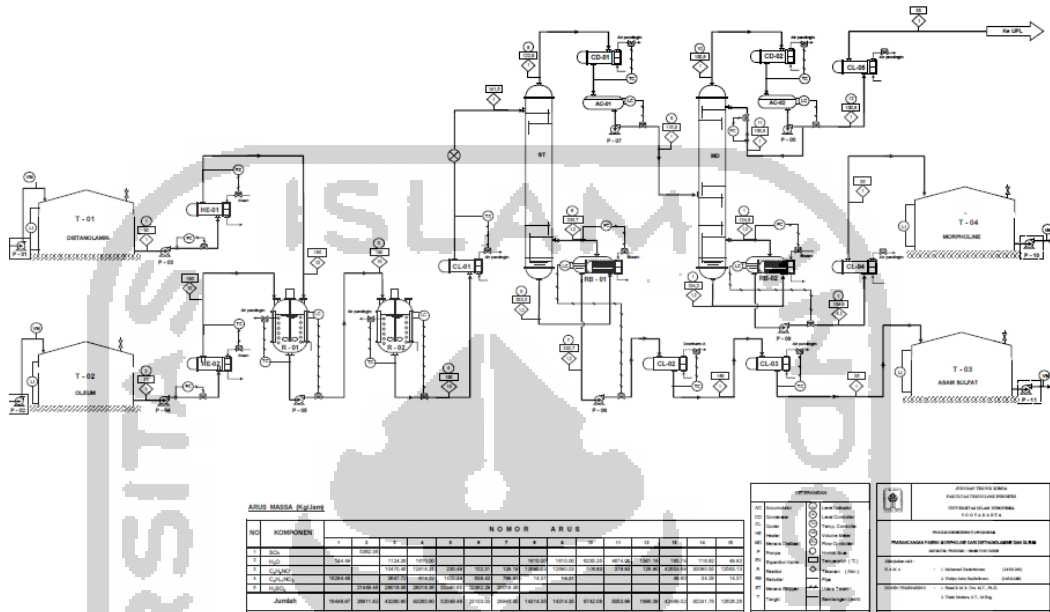
Konversi : 0,95

Hasil reaksi :

$$\text{C}_4\text{H}_{11}\text{NO}_2 = 7,7545 \text{ Kgmol/j} = 814,2241 \text{ Kg/j}$$

$$\text{H}_2\text{O} = 89,4445 \text{ Kgmol/j} = 1610,0020 \text{ Kg/j}$$

PROCESS ENGINEERING FLOW DIAGRAM
 PRARANCANGAN FABRIK MORPHOLINE DARI DIETHANOLAMINE DAN OLEUM
 KAPASITAS PRODUKSI : 100.000 TON / TAHUN

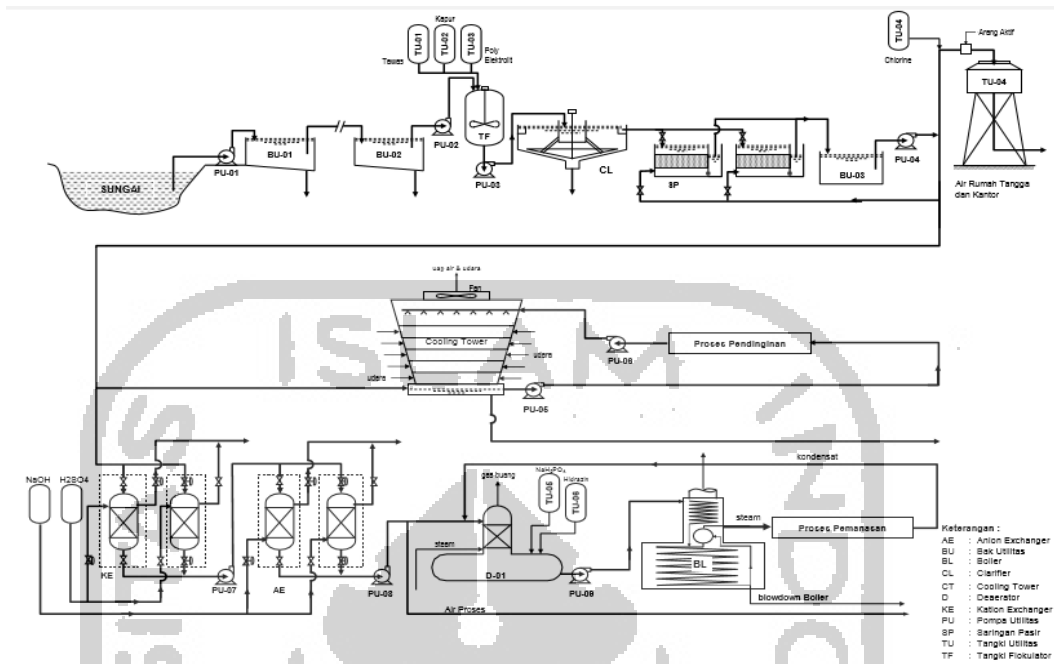


ARUS MASSA (kg/jam)

| NO | KOMPONEN | NOMOR ALIR | | | | | | | | | | | | | |
|--------|-----------------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| 1 | SO ₂ | 7668,0 | | | | | | | | | | | | | |
| 2 | SO ₃ | | 1014,0 | | | | | | | | | | | | |
| 3 | COAL | | 1014,0 | 1014,0 | | | | | | | | | | | |
| 4 | DIETHANOLAMINE | | | | 1014,0 | | | | | | | | | | |
| 5 | OLEUM | | | | | 1014,0 | | | | | | | | | |
| 6 | AMAR SULFAT | | | | | | 1014,0 | | | | | | | | |
| Jumlah | | 7668,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 | 2028,0 |

| <p>LEGENDA</p> <ul style="list-style-type: none"> □ Tank ○ Pompa ◇ Katup ◇ Katup Otomatis ◇ Katup Kontrol ◇ Katup Safety ◇ Katup Lock ◇ Katup Lockout ◇ Katup Lockdown ◇ Katup Lockup ◇ Katup Lockdown ◇ Katup Lockup ◇ Katup Lockdown ◇ Katup Lockup | <p>REVISI</p> <table border="1"> <tr> <th>NO</th> <th>REVISI</th> <th>REVISI</th> </tr> <tr> <td>1</td> <td>1</td> <td>1</td> </tr> </table> | NO | REVISI | REVISI | 1 | 1 | 1 |
|---|--|--------|--------|--------|---|---|---|
| NO | REVISI | REVISI | | | | | |
| 1 | 1 | 1 | | | | | |

Gambar 5.1 PEFD



Gambar Skema Unit Pengolahan Air

Gambar 5.2 Skema Unit Pengolahan Air

$$\text{H}_2\text{SO}_4 = 285,9016 \text{ Kgmol/j} = 28018,3555 \text{ Kg/j}$$

$$\text{C}_4\text{H}_9\text{NO} = 147,3358 \text{ Kgmol/j} = 12818,2139 \text{ Kg/j}$$

$$\text{Jumlah} = 530,4364 \text{ Kgmol/j} = 43260,7969 \text{ Kg/j}$$

NERACA PANAS

Diketahui Cp rata-rata untuk masing-masing komponen

sebagai berikut :

$$cp \text{ C}_4\text{H}_{11}\text{NO}_2 = 32,62 \text{ Kcal/kmol K}$$

$$cp \text{ H}_2\text{O} = (92,05 - 0,03995 T - 2,1103\text{E-}04 T^2 + 5,3469\text{E} - 07 T^3) / 4,2 \text{ Kcal/kmol K}$$

$$cp \text{ H}_2\text{SO}_4 = (26,00 + 0,70337 T - 0,0013856 T^2 + 1,0342\text{E-}06 T^3) / 4,2 \text{ Kcal/kmol K}$$

$$cp \text{ SO}_3 = 12,21 \text{ Kcal/kmol K}$$

$$cp \text{ C}_4\text{H}_9\text{NO} = 39,24 \text{ Kcal/kmol K}$$

Enthalpi Umpan Masuk Diethanolamine

$$\text{Suhu Umpan masuk Reaktor} = 190,0^\circ\text{C}$$

$$\text{Suhu referensi} = 25^\circ\text{C}$$

| Komponen | M | cp dT | H = m cp dT |
|--------------------------------------|-------------|-----------|---------------|
| $\text{C}_4\text{H}_{11}\text{NO}_2$ | 10.500,0000 | 9823,4207 | 398479,816 |
| H_2O | 106,0606 | 4136,4284 | 5649,534 |
| Jumlah | | | 404129,350 |

Enthalpi Umpan masuk (H1) = 404129,350 Kj/jam

Enthalpi Umpan Masuk Asam Sulfat dan Oleum

Suhu Umpan masuk Reaktor = 190,0 °C

Suhu referensi = 25 °C

| Komponen | M | cp dT | H = m cp dT |
|--------------------------------|----------|----------|---------------|
| H ₂ SO ₄ | 4867,711 | 7298,227 | 592094,401 |
| SO ₃ | 4,873 | 4136,428 | 1119,728 |
| Jumlah | 4872,584 | | 593214,128 |

Enthalpi Umpan masuk (H2) = 593214,128 Kj/jam

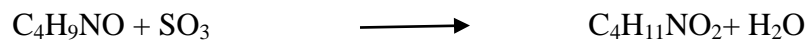
Enthalpi Hasil Reaksi

Suhu hasil reaksi keluar Reaktor = 190,0 °C

Suhu referensi = 25 °C

| Komponen | M | cp dT | H = m cp dT |
|--|----------|-----------|---------------|
| C ₄ H ₉ NO | 851,850 | 9823,421 | 139467,935 |
| H ₂ O | 504,302 | 4136,428 | 115889,451 |
| C ₄ H ₁₁ NO ₂ | 2689,411 | 11329,360 | 298718,640 |
| H ₂ SO ₄ | 11,926 | 7904,480 | 961,918 |
| Jumlah | 7343,193 | | 954701,666 |

Enthalpi hasil reaksi (H4) = 954701,666Kj/jam

Panas Reaksi :

Dari data Literatur diperoleh :

$$\text{Panas Pembentukan } \text{C}_4\text{H}_9\text{NO} = 5,41 \text{ Kj/kmol}$$

$$\text{Panas Pembentukan } \text{SO}_3 = 11,715 \text{ Kj/kmol}$$

$$\text{Panas Pembentukan } \text{C}_4\text{H}_{11}\text{NO}_2 = 8,88 \text{ Kj/kmol}$$

$$\text{Panas Pembentukan } \text{H}_2\text{O} = 6,002 \text{ Kj/kmol}$$

Panas reaksi pada suhu 25 °C

$$= \text{DHf produk} - \text{DHf reaktan}$$

$$= (\text{DHf } \text{C}_4\text{H}_{11}\text{NO}_2 + \text{DHf } \text{H}_2\text{O}) - (\text{DHf } \text{C}_4\text{H}_9\text{NO} + \text{DHf } \text{SO}_3)$$

$$= (8,88 + 6,002) - (5,41 + 11,715)$$

$$= -2,243 \text{ Kj/kmol}$$

$$\text{Panas reaksi suhu } 80 \text{ }^\circ\text{C} = \text{DHr}_0 + \int_{298}^T \text{cp } dT$$

$$= \text{DHr}_0 + \int_{298}^T (\text{Cp produk} - \text{Cp reaktan}) dT$$

dimana :

$$\int_{298}^T \text{cp } dT = \int_{298}^T 392,3903 - 451,5309 dT$$

$$= -59,1407 \text{Kj/jam}$$

maka :

Panas reaksi pada suhu 80 °C

$$= \text{DHr}0 + \int_{298}^T d \text{ cp dT}$$

$$= -59,1407 + 954701,6659 \text{ KCal/gmol}$$

$$= 43600,5205 \text{ Kj/jam}$$

Jadi :

$$\text{Panas Masuk (H1 + H2 + H3)} = 998361,3270 \text{ Kj/jam}$$

$$\text{Panas Reaksi (Qr)} = 43600,5205 \text{ Kj/jam}$$

Neraca Panas disekitar reaktor :

$$\text{Input - output} = \text{Accumulation}$$

$$\text{Panas Masuk} - (\text{Panas keluar} + \text{panas reaksi} + \text{panas dibuang}) = 0$$

$$(H1 + H2 + H3) - (H4 + Qr + Ql) = 0$$

Panas Yang dikeluarkan (Ql) :

$$(Ql) = (H1 + H2 + H3) - (H4 + Qr)$$

$$= 998361,3270 - (954701,666 + 43600,5205)$$

$$= 59,1405 \text{ Kj/jam}$$

Neraca Panas :

| Komponen | Input (Kj/jam) | Output (Kj/jam) |
|-------------|----------------|-----------------|
| Q in | 998361,3270 | |
| Q out | | 954701,67 |
| Q reaksi | | 43600,5205 |
| subtotal | 998361,3270 | 998302,1864 |
| Q pendingin | | 59,1407 |
| Total | 998361,3270 | 998361,3270 |

Perhitungan Volume dan Ukuran Reaktor

Dari data diperoleh :

$$\text{Densitas } C_4H_{11}NO_2 = 725,3978 \text{ Kg/m}^3$$

$$\text{Densitas } H_2O = 975,6407 \text{ Kg/m}^3$$

$$\text{Densitas } CH_3COOH = 983,7055 \text{ Kg/m}^3$$

$$\text{Densitas } C_4H_9NO = 808,2536 \text{ Kg/m}^3$$

$$\text{Densitas } SO_3 = 1764,6882 \text{ Kg/m}^3$$

Dari data percobaan patent dapat ditentukan konstanta kecepatanreaksi untuk kondisi operasi $T = 80^\circ C$ dan tekanan Atmosferis

Volume cairan :

| Komponen | massa kg | densitas | Volume |
|--|------------|------------|------------|
| C ₄ H ₉ NO | 860,322757 | 725,397854 | 624076,282 |
| H ₂ O | 509,318476 | 975,640716 | 496911,842 |
| C ₄ H ₁₁ NO ₂ | 3318,38778 | 983,70559 | 3264316,6 |
| H ₂ SO ₄ | 2716,16185 | 808,253699 | 2195347,86 |
| C ₄ H ₉ NO | 12,0445186 | 1764,6882 | 21254,8198 |
| JUMLAH | | | 6601907,41 |

Menentukan Konstanta Kecepatan Reaksi

Konstanta kecepatan reaksi ditentukan berdasarkan teori analisis data dengan persamaan reaksi :

Reaksi



$$\text{Konversi } X_A = 0,65$$

$$(1 - X_A) = 0,35$$

maka

$$\text{C}_4\text{H}_9\text{NO} = n_{A0} (1 - X_A)$$

$$= 40,5643 * 0,35$$

$$= 14,1975 \quad \text{Kmol/jam}$$

$$\begin{aligned} \text{SO}_3 &= n_{\text{Bo}} - n_{\text{Ao}} \text{XA} \\ &= 81,1285 - 40,5643 * 0,65 \\ &= 54,7618 \quad \text{Kmol/jam} \end{aligned}$$

$$\text{C}_4\text{H}_{11}\text{NO}_2 = 26,3667 \quad \text{Kmol/jam}$$

$$\text{H}_2\text{O} = 26,3667 \quad \text{Kmol/jam}$$

sehingga :

Konstanta kecepatan reaksi :

$$\begin{aligned} K_c &= 1,57748\text{E}+13 * \text{EXP}(-8881,918657/T) \\ &= 2,2309\text{E}+13 * \text{EXP}(-8881,918657/353) \\ &= 263,6883 \text{ lt}/(\text{Kgmol jam}) \end{aligned}$$

Anggapan :

- Volume cairan selama reaksi tetap
- Bisa dianggap isothermal karena cairan dalam tangki mixed flow
- Reaksi orde dua



dengan $-r_a = -\frac{dC_A}{dt} = k * C_A * C_B$

Volume cairan :

| Komponen | massa kg | densitas | Volume |
|--|------------|------------|------------|
| C ₄ H ₉ NO | 860,322757 | 725,397854 | 624076,282 |
| H ₂ O | 509,318476 | 975,640716 | 496911,842 |
| C ₄ H ₁₁ NO ₂ | 3318,38778 | 983,70559 | 3264316,6 |
| H ₂ SO ₄ | 2716,16185 | 808,253699 | 2195347,86 |
| SO ₃ | 12,0445186 | 1764,6882 | 21254,8198 |
| JUMLAH | | | 6601907,41 |

Kondisi Awal :

$$\text{Konsentrasi awal C}_4\text{H}_9\text{NO} = 0,005217 \text{ grmol/lt}$$

$$\text{Konsentrasi awal SO}_3 = 0,010434 \text{ grmol/lt}$$

$$\text{Perbandingan konsentrasi} = 2,000000$$

maka diperoleh volume reaktor dengan volume:

$$\text{Konversi Reaktor (Xa)} = 0,65$$

Volume cairan dalam reaktor :

$$F_v, x_a$$

$$V = \frac{F_v, x_a}{k * C_{Ao} (1 - x_a)(M - x_a)}$$

$$k * C_{Ao} (1 - x_a)(M - x_a)$$

$$19168,1085 * 0,650$$

$$= \frac{\quad}{\quad}$$

$$263,6883 * 0,005217 * (1 - 0,650) * (2,000 - 0,650)$$

$$= 135 \text{ liter}$$

Over Design : 20 %

$$\text{Volume reaktor} = (100/80) * 21701,8409 \text{ lt}$$

$$= 27127,3011 \text{ lt}$$

$$\text{Dipakai Volume reaktor} = 27,127 \text{ m}^3$$

Menghitung ukuran reaktor :

Reaktor berbentuk silinder tegak dengan perbandingan $H : D = 1 : 1$

$$V_t = \frac{\pi * D^2 * (h/d) * D}{4} + \frac{\pi}{12} D^2 * D$$

Atau :

$$\text{diameter (D)} = \left[\frac{V_t}{\frac{\pi}{4} \left(\frac{h}{d} \right) + \frac{\pi}{12}} \right]^{1/3}$$

$$\text{diameter (D)} = \left[\frac{27,127}{\frac{\pi}{4} * 1. + \frac{\pi}{12}} \right]^{1/3}$$

$$= 2,86 \text{ m}$$

$$\text{Tinggi (H)} = 1 * 2,86$$

$$= 2,86 \text{ m}$$

diperoleh ukuran Reaktor :

$$\text{diameter} = 2,86 \text{ m}$$

$$\text{tinggi} = 2,86 \text{ m}$$

$$\text{Volume cairan dalam head} = \left(\frac{1}{2} \right) * \left(\frac{\pi}{12} \right) * 27,89 \text{ m}^3$$

$$= 3,65 \text{ m}^3$$

$$\text{Volume cairan dibadan Reaktor} = 21,7018 \text{ m}^3 - 3,64 \text{ m}^3$$

$$= 18,05 \text{ m}^3$$

$$\text{Tinggi cairan dibadan Reaktor} = (4 * 18,05) / (3,14 * (2,85^2)) \text{ m}$$

$$= 2,82 \text{ m}$$

Menghitung tebal shell dan head

Tebal shell :

$$\text{Tekanan design (p)} = 2,19 \text{ psi}$$

$$\text{Allowable stress} = 18750 \text{ psi}$$

$$\text{Efisiensi sambungan} = 0,85$$

$$\text{Faktor korosi} = 0,125 \text{ in}$$

$$\text{Jari-jari Reaktor} = 56,22 \text{ in}$$

$$t_{\text{shell}} = \frac{p \cdot r_i}{S \cdot e - 0,6 \cdot p} + c$$

$$= \frac{2,19 \cdot 56,22}{18750 \cdot 0,85 - 0,6 \cdot 22,0} + 0,125$$

$$= 0,1369 \text{ in}$$

Maka dipilih tebal shell $\frac{3}{16}$ in

Tebal Head :

$$th = \frac{P \cdot r \cdot w}{(2 \cdot S \cdot E) - (0,2 \cdot P)} + C$$

$$= 0,1955 \text{ in}$$

Maka dipilih tebal head $\frac{1}{4}$ in

Menghitung pengaduk dalam Reaktor

Dipilih : Pengaduk type Turbine dengan 6 blade

Jumlah baffle 4 buah

Dari tabel 477, Brown diperoleh :

$$D_i/DR = 1/3$$

$$E = D_i = 1$$

$$W = D_i/5$$

$$L = D_i/4$$

$$B = DR/12$$

$$\text{Diameter Impeler} = 0,95 \text{ m}$$

$$\text{Tinggi Impeler} = 0,95 \text{ m}$$

$$\text{Lebar Baffle} = 0,24 \text{ m}$$

$$\text{Tinggi Zone pegadukan} = 0,19 \text{ m}$$

$$\text{Jumlah Impeller} = 5 \text{ Impeller}$$

diambil :

$$z_i/D_i = 1$$

$$\text{Putaran} = 2,88 \text{ rps}$$

$$\text{efisiensi} = 70 \%$$

Tinggi baffle diambil sama dengan tinggi cairan bilangan Reynold dalam Reaktor:

$$Re = \frac{\rho_L N D I^2}{\mu_L}$$

$$5257,68 * 73 * 0,95$$

$$= \frac{\quad}{\quad}$$

$$0,44$$

$$= 824179,6422$$

Dari fig, 477 brown diperoleh

$$P = \frac{N^3 D I^5 \rho N_p}{550 \text{ gc}}$$

$$(1,21^3) * (0,95/0,3048)^5 * 328,23 * 7$$

$$= \frac{\quad}{\quad}$$

$$550 * 32,2$$

$$= 69,47 \text{ Hp}$$

effisiensi : 70 %

$$P = 69,47$$

$$\text{Power} = \frac{\quad}{\quad} = \frac{\quad}{\quad}$$

$$\text{eff} = 0,70$$

$$= 99,24 \text{ Hp}$$

Digunakan motor dengan daya = 100 Hp

Spesifikasi Reaktor

Tugas : Mereaksikan Diethanolamine dan Oleum menjadi Morpholine dan Air dengan katalis Asam Sulfat dengan kecepatan umpan = 7343,1935 kg/j

Jenis : Reaktor Alir Tangki Berpengaduk

Kondisi Operasi :

Tekanan : 10 atm

Suhu : 190 °C

Diperoleh ukuran Reaktor :

Diameter = 2,86 m

Tinggi = 3,99 m

Volume cairan dalam head = 3,65 m³

Volume cairan dibadan Reaktor = 18,05 m³

Tinggi cairan dibadan Reaktor = 2,82 m

Dipilih Tebal shell : $\frac{3}{16}$ in

Tebal Head : $\frac{1}{4}$ in

Dipilih : Pengaduk type Turbine dengan 6 blade

Jumlah baffle 4 buah

Diameter Impeler = 0,95 m

Tinggi Impeler = 0,95 m

Lebar Baffle = 0,24 m

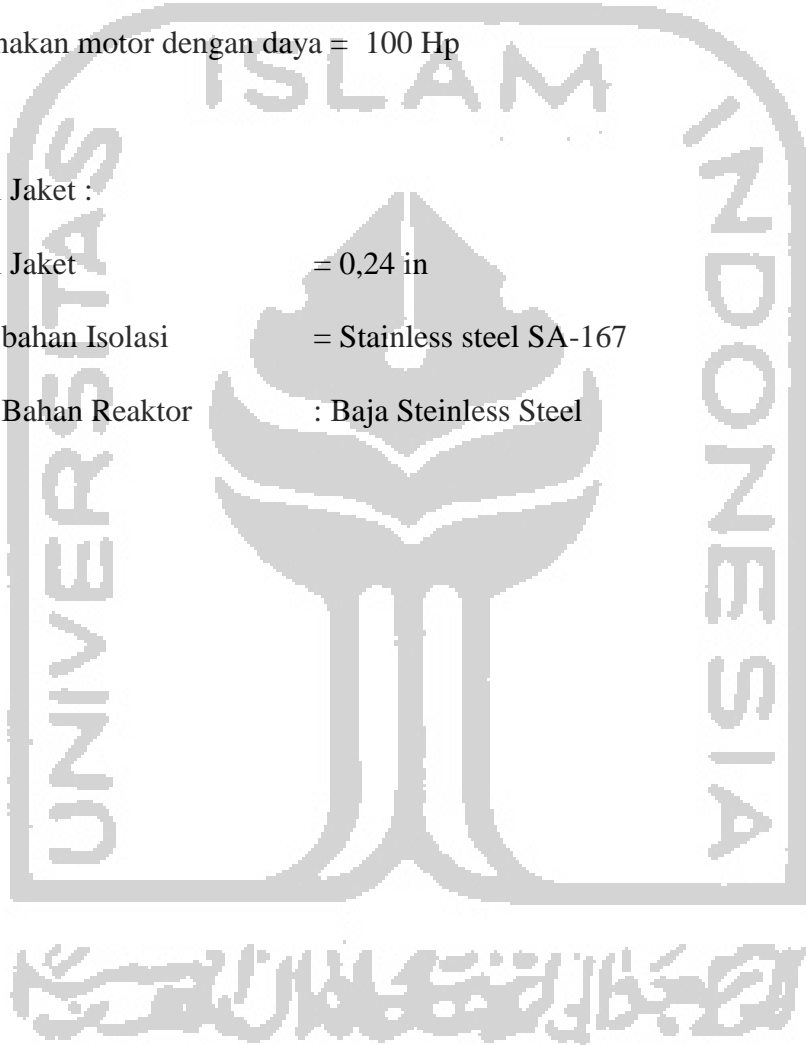
Digunakan motor dengan daya = 100 Hp

Tebal Jacket :

Tebal Jacket = 0,24 in

Jenis bahan Isolasi = Stainless steel SA-167

Jenis Bahan Reaktor : Baja Steinless Steel



LAMPIRAN GAMBAR REAKTOR RATB

