

DAFTAR PUSTAKA

- Aries, R.S., and Newton, R.D., 1955, "*Chemical Engineering Cost Estimation*", Mc Graw Hill Handbook Co, Inc, New York.
- Brownell, L.E., and Young, E.H., 1959, "*Process Equipment Design*", John Wiley and Sons, Inc, New York.
- Coulson, J.M., and Richardson, J.F., 1983, "*Chemical Engineering*", Vol 1, Pergamon Internasional Library, New York.
- Holman, J., 1981, "*Heat Transfer*", Mc Graw Hill Book Co, Inc, New York.
- Kern, D.Q., 1983, "*Process Heat Transfer*", Mc Graw Hill Book Co, Inc, New York.
- Keulks, George, W., Rosynek, Michael, P., Daniel, Chelliah,. "*Bismuth Molybdate Catalysts*", Department of Chemistry and Laboratory for Surface Studies, University of Wisconsin-Milwaukee, 1971
- Lei, M., Lesage, F., Latifi, M.A., Tretjak, S., "*Optimization of acrolein production in a fixed-bed reactor system*", Universty de Lorraine, International Conference on Process Control (PC), 2013.
- Mc Cabe, Smith, J.C., and Harriot, 1985, "*Unit Operation of Chemical Engineering*", 4th ed., Mc Graw Hill Book Co, Inc, New York.
- Othmer, D.F., Kirk, R.E., 1949, "*Encyclopedia of Chemical Technology*", Volume 5, 5th Edition, ISBN: 978-0-471-48518-6, John Wiley and Son, Inc, New York.
- Perry, R.H., and Green, D.W., 1986, *Perry's Chemical Engineer's Handbook*, 6th ed., Mc Graw Hill Book Co., Inc., New York
- Speight, James, G., 2002, "*CHEMICAL AND PROCESS DESIGN HANDBOOK*", ISBN 0-07-137433-7, Mc Graw Hill Book Co, Inc, New York.

Wibawanta, Sandra, Anni, Setyowati,. “*Catalytic Partial Oxidation of Propylene for Acrolein Production*”, Thesis, Tidak diterbitkan, Curtin University of Thecnology, 2011.

Yaws, Carl L., 1998, “*Chemical Properties Handbook*”, Mc Graw Hill Book Co, Inc, New York.

Badan Pusat Statistik, 2017, Kebutuhan Impor NaOH dan NaCl, dipublikasikan <https://www.bps.go.id/> .

Bank Indonesia, 2017, Nilai Suku Bunga, dipublikasikan <http://www.bi.go.id/id/Default.aspx>

Clarke Energy, 2017, *Coal Seam Gas*, dipublikasikan <https://www.clarke-energy.com/coal-gas/coal-seam-methane/>

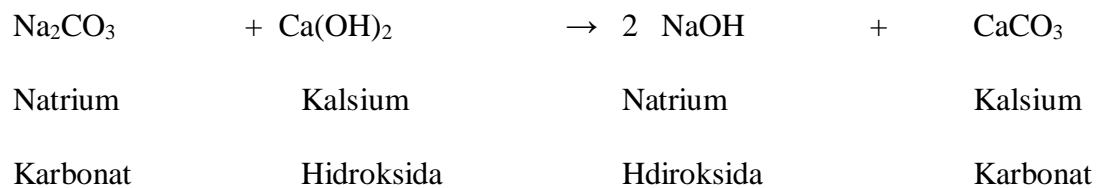
LAMPIRAN

REAKTOR

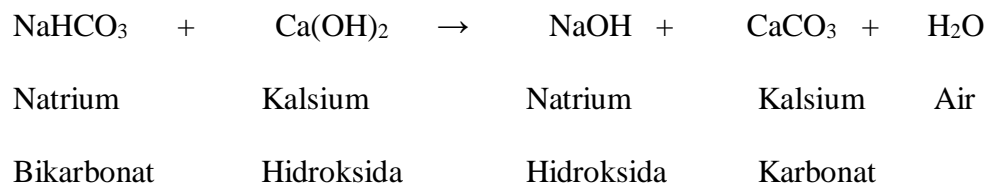
Jenis : Reaktor Alir Tangki Berpengaduk
Fungsi : Tempat berlangsungnya reaksi pencampuran Brine dengan Katalis
Kondisi Operasi : Suhu = 90 °C
Tekanan = 1 atm

Reaksi yang terjadi dalam reaktor :

Reaksi 1 :



Reaksi 2 :



1. Neraca Massa :

Umpan Masuk :

a. Umpan Masuk CSG :

$$\text{NaCl} = 114,3220 \text{ Kgmol/j} = 6.687,8374 \text{ Kg/j}$$

$$\text{Na}_2\text{CO}_3 = 14,0607 \text{ Kgmol/j} = 1.490,4324 \text{ Kg/j}$$

$$\text{NaHCO}_3 = 8,5304 \text{ Kgmol/j} = 716,5540 \text{ Kg/j}$$

$$\text{CaCO}_3 = 1,1943 \text{ Kgmol/j} = 119,4257 \text{ Kg/j}$$

$$\text{H}_2\text{O} = 2.153,1121 \text{ Kgmol/j} = 38.756,0156 \text{ Kg/j}$$

$$\text{Jumlah} = 2.291,2195 \text{ Kgmol/j} = 47.770,2656 \text{ Kg/j}$$

b. Umpan katalis

$$\text{Ca(OH)}_2 = 22,5911 \text{ Kgmol/j} = 1.671,7404 \text{ Kg/j}$$

$$\text{H}_2\text{O} = 835,8702 \text{ Kgmol/j} = 15.045,6641 \text{ Kg/j}$$

$$\text{Jumlah} = 858,4613 \text{ Kgmol/j} = 16.717,4043 \text{ Kg/j}$$

Hasil reaksi :

$$\text{NaCl} = 114,3220 \text{ Kgmol/j} = 6.687,8374 \text{ Kg/j}$$

$$\text{Na}_2\text{CO}_3 = 0,2812 \text{ Kgmol/j} = 29,8086 \text{ Kg/j}$$

$$\text{NaHCO}_3 = 0,1706 \text{ Kgmol/j} = 14,3311 \text{ Kg/j}$$

$$\text{CaCO}_3 = 23,3335 \text{ Kgmol/j} = 2.333,3523 \text{ Kg/j}$$

$$\text{H}_2\text{O} = 2.997,3420 \text{ Kgmol/j} = 53.952,1563 \text{ Kg/j}$$

$$\text{Ca(OH)}_2 = 0,4518 \text{ Kgmol/j} = 33,4348 \text{ Kg/j}$$

$$\text{NaOH} = 35,9187 \text{ Kgmol/j} = 1.436,7494 \text{ Kg/j}$$

$$\text{Jumlah} = 3.171,8201 \text{ Kgmol/j} = 64.487,6680 \text{ Kg/j}$$

2. Neraca Panas

Diketahui Cp rata-rata untuk masing-masing komponen sebagai berikut :

$$\text{Cp NaCl} = 8,55 \text{ Kcal/kmol K}$$

$$\text{Cp Na}_2\text{CO}_3 = 26,53 \text{ Kcal/kmol K}$$

$$\text{Cp NaHCO}_3 = 20,98 \text{ Kcal/kmol K}$$

$$\text{Cp CaCO}_3 = 19,57 \text{ Kcal/kmol K}$$

$$\text{Cp H}_2\text{O} = 17,99 \text{ Kcal/kmol K}$$

$$\text{Cp Ca(OH)}_2 = 20,91 \text{ Kcal/kmol K}$$

$$\text{Cp NaOH} = 14,23 \text{ Kcal/kmol K}$$

a. Enthalpi umpan masuk reaktor :

$$\text{Suhu Umpan masuk Reaktor} = 90,0 \text{ }^\circ\text{C}$$

$$\text{Suhu referensi} = 25 \text{ }^\circ\text{C}$$

Komponen	M Kmol	Cp dT kcal/kmol	H = m CP dT kcal/jam
NaCl	114,3220	555,7500	63.534,4515
Na ₂ CO ₃	14,0607	1.724,4500	24.246,9741
NaHCO ₃	8,5304	1.363,7000	11.632,9065
CaCO ₃	1,1943	1.272,0500	1.519,2093
H ₂ O	2.988,9823	1.169,3500	3.495.166,4525
Ca(OH) ₂	22,5911	1.359,1500	30.704,6936
	3.149,6808		3.626.804,6875

$$H1 = 3.626.804,6875 \text{ kcal/jam}$$

b. Enthalpi produk Keluar reaktor :

$$\text{Suhu Umpan masuk Reaktor} = 90,0 \text{ }^\circ\text{C}$$

$$\text{Suhu referensi} = 25 \text{ }^\circ\text{C}$$

Komponen	M Kmol	Cp dT kcal/kmol	H = m CP dT kcal/jam
NaCl	114,3220	555,7500	63.534,4515
Na ₂ CO ₃	0,2821	1.724,4500	486,4673
NaHCO ₃	0,1706	1.363,7000	232,6472
CaCO ₃	23,3335	1.272,0500	29.681,3787
H ₂ O	2.997,3421	1.169,3500	3.504.941,9846
Ca(OH) ₂	0,4518	1.359,1500	614,0640
NaOH	35,9178	924,9500	33.222,1691
	3.171,8199		3.632.713,1625

$$H2 = 3.632.713,1625$$

c. Panas Reaksi

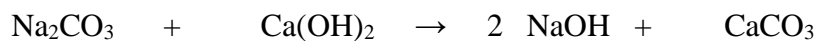
Reaksi 1 :

$$\text{Panas Pembentukan Na}_2\text{CO}_3 = -270,30 \text{ Kcal/mol} = -11.316.916,55 \text{ kj/kmol}$$

$$\text{Panas Pembentukan Ca(OH)}_2 = -235,70 \text{ Kcal/mol} = -986.828,332 \text{ kj/kmol}$$

$$\text{Panas Pembentukan NaOH} = -101,99 \text{ Kcal/mol} = -427.011,54 \text{ kj/kmol}$$

$$\text{Panas Pembentukan CaCO}_3 = -269,80 \text{ Kcal/mol} = -1.129.598,151 \text{ kj/kmol}$$



$$\Delta H_f \text{ produk} = -1.983.621,25 \text{ Kj/kmol}$$

$$\Delta H_f \text{ reaktan} = -2.118.519,88 \text{ Kj/kmol}$$

$$\Delta H_{R 298} = \Delta H_f \text{ produk} - \Delta H_f \text{ reaktan}$$

$$= 134.898,64 \text{ Kj/kmol}$$

$$\Delta H_r = 3.083,60 \text{ Kj/kmol}$$

$$\Delta H_p = 3.121,9500 \text{ Kj/kmol}$$

$$\Delta H_R = 134.936,9876 \text{ Kj/kmol}$$

$$= 32.229,15974 \text{ kkal/kmol}$$

Reaksi 2 :

$$\text{Panas Pembentukan Na}_2\text{CO}_3 = -270,30 \text{ Kcal/mol} = -11.316.916,55 \text{ kj/kmol}$$

$$\text{Panas Pembentukan Ca(OH)}_2 = -235,70 \text{ Kcal/mol} = -986.828,332 \text{ kj/kmol}$$

$$\text{Panas Pembentukan NaOH} = -101,99 \text{ Kcal/mol} = -427.011,54 \text{ kj/kmol}$$

$$\text{Panas Pembentukan CaCO}_3 = -269,80 \text{ Kcal/mol} = -1.129.598,151 \text{ kj/kmol}$$

$$\text{Panas Pembentukan H}_2\text{O} = -68,32 \text{ Kcal/mol} = -286.042,0522 \text{ kj/kmol}$$



$$\Delta H_f \text{ produk} = -1.842.651,75 \text{ Kj/kmol}$$

$$\Delta H_f \text{ reaktan} = -1.935.138,12 \text{ Kj/kmol}$$

$$\Delta H_R \text{ 298} = \Delta H_f \text{ produk} - \Delta H_f \text{ reaktan}$$

$$= 92.486,37 \text{ Kj/kmol}$$

$$\Delta H_r = 2.722,8500 \text{ Kj/kmol}$$

$$\Delta H_p = 3.366,3500 \text{ Kj/kmol}$$

$$\Delta H_R = 93.129,8720 \text{ Kj/kmol}$$

$$= 22.243,6974 \text{ kkal/kmol}$$

$$\Delta H_R \text{ total} = 54.472,8571 \text{ kkal/kmol}$$

$$= 228.066,8596 \text{ Kj/kmol}$$

Panas Masuk (kcal/jam)		Panas Keluar (kcal/jam)	
Panas masuk	3.626.804,6875	Panas keluar	3.632.713,1625
Panas reaksi	54.472,8571	Panas yang diambil	48.564,3822
Total	3.681.277,5446	Total	3.681.277,5446

3. Menentukan Konstanta Kecepatan Reaksi

Dari data di Perry's Hand Book diperoleh :

Komponen	Densitas (kg/lt)
NaCl	2,1640
Na ₂ CO ₃	2,5330
NaHCO ₃	2,2000
CaCO ₃	2,7100
H ₂ O	1,0000
Ca(OH) ₂	2,2400

Konstanta kecepatan

Reaksi untuk kondisi operasi $T = 90,0\text{ }^{\circ}\text{C}$ dan Tekanan 1 atm

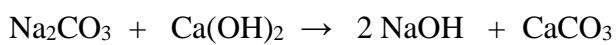
Volume cairan :

Komponen	Massa, kg	Densitas, (kg/lt)	Volume
NaCl	6.687,837	2,164	3.090,498
Na ₂ CO ₃	1.490,432	2,533	588,406
NaHCO ₃	716,554	2,200	325,706

CaCO ₃	119,426	2,710	44,069
H ₂ O	53.801,680	1,000	53.801,680
Ca(OH) ₂	1.671,740	2,240	746,313
			58.596,672

Konstanta kecepatan reaksi ditentukan berdasarkan data Patent no. CA 2870073

A1 dengan persamaan reaksi :



Kondisi Awal : Konsentrasi awal Na₂CO₃ = 0,000240 Kgmol/lit

Konsentrasi awal Ca(OH)₂ = 0,000386 Kgmol/lit

Perbandingan konsentrasi = 1,607

Konversi Reaktor (X_a) = 0,98

Waktu reaksi dalam reaktor = 1,00 jam

Untuk Reaktor Alir Tangki Berpengaduk berlaku :

$$(V / F_v) = \frac{C_{A_0} \cdot x_a}{(-r_a)}$$

$$(V / F_v) = \frac{C_{A_0} \cdot x_a}{k \cdot C_A C_B}$$

$$(V / F_v) = \frac{x_a}{k \cdot C_{A_0} (1 - x_a)(M - x_a)}$$

$$k = \frac{x_a}{(V / F_v) C_{A_0} (1 - x_a)(M - x_a)}$$

$$= \frac{0.980}{1,00 \times 0,000240 (1 - 0,98)(1,61 - 0,98)}$$

$$= 325.847,09 \text{ Lt}/(\text{Kmol jam})$$

4. Perhitungan Volume dan ukuran reaktor

Anggapan :

- Volume cairan selama reaksi tetap
- Bisa dianggap isothermal karena cairan dalam tangki mixed flow
- Reaksi sederhana orde dua semu

Reaksi : $A + B \rightarrow \text{Produk}$

dengan $-r_a = -dCA/dt = k_1 \cdot CA \cdot CB$

$$= k_1 \cdot CA_0(1 - x_a) \cdot CA_0(M - x_a)$$

Kondisi Awal : Konsentrasi awal $Na_2CO_3 = 0,000240 \text{ Kgmol/lit}$

Konsentrasi awal $Ca(OH)_2 = 0,000386 \text{ Kgmol/lit}$

Perbandingan konsentrasi = 1,607

maka diperoleh volume reaktor dengan volume:

Konversi Reaktor (X_a) = 0,98

Volume cairan dalam reaktor :

$$\begin{aligned} V &= \frac{F_v \cdot x_a}{k \cdot CA_0 (1 - x_a) (M - x_a)} \\ &= \frac{(58.596,672) \times 0,9800}{325.847,09 \times 0,00024 (1 - 0,98)(2 - 0,98)} \\ &= 58.596,668 \text{ lt} \end{aligned}$$

Over Design : 20 %

Volume reaktor = 1,2 X 58.596,668 lt

$$= 70.316,008 \text{ lt}$$

Dipakai Volume reaktor = 70,32 m^3

Menghitung ukuran reaktor :

Reaktor berbentuk silinder tegak dengan perbandingan $H : D = 1,5 : 1$

$$V_t = \frac{\pi \cdot D^2 \cdot (h/d) \cdot D}{4} + \frac{\pi}{12} D^2 \cdot D$$

Atau :

$$\begin{aligned} \text{Diameter (D)} &= \left[\frac{V_t}{\pi/4 (h/d) + \pi / 12} \right]^{1/3} \\ &= \left[\frac{70,316}{\pi/4 \cdot 1,50 + \pi / 12} \right]^{1/3} \\ &= 3,66 \text{ m} \end{aligned}$$

$$\text{Tinggi (H)} = 1,5 \times 3,66$$

$$= 5,48 \text{ m}$$

$$\text{Diperoleh ukuran Reaktor : Diameter} = 3,66 \text{ m}$$

$$\text{Tinggi} = 5,48 \text{ m}$$

$$\text{Volume cairan dalam head} = (1/2) (\pi/12) 3,656\text{m}^3$$

$$= 6,392 \text{ m}^3$$

$$\text{Volume cairan dibadan Reaktor} = 58,597 \text{ m}^3 - 6,392 \text{ m}^3$$

$$= 52,204 \text{ m}^3$$

$$\text{Tinggi cairan dibadan Reaktor} = 52,204 / 10,491 \text{ m}$$

$$= 4,976 \text{ m}$$

Ukuran yang di peroleh terlalu besar maka di lakukan proses optimasi yang

dipasang secara seri :

Kecepatan Volume Umpan :

Komponen	BM	Kgmol/jam	Kg/jam	densitas	Volume
NaCl	58,5	114,3220	6.687,8373	2,1640	3090,4978
Na ₂ CO ₃	106	14,0607	1.490,4323	2,5330	588,4060
NaHCO ₃	84	8,5304	716,5540	2,2000	325,7064
CaCO ₃	100	1,1943	119,4257	2,7100	44,0685
Ca(OH) ₂	74	22,5911	1.671,7404	2,2400	746,3127
H ₂ O	18	2.988,9823	53.801,6811	1,0000	53.909,5001
		3.149,6807	64.487,6709		58.704,4915

Optimasi jumlah Reaktor

persamaan umum

$$X_{An-1} = X_{An} - \frac{V k C_{A_0} (1 - X_{An})(M - X_{An})}{F_v}$$

1. Jumlah Reaktor = 1

$$X_{A_1} = 0,98$$

$$k = 325.846,97 \text{ lt/kgmol jam}$$

$$F_v = 58.704,4915 \text{ lt/jam}$$

$$C_{A_0} = 0,000240 \text{ Kgmol/lt}$$

$$M = B/A = 1,606685$$

$$V \text{ Coba} = 112.131,1107 \text{ liter}$$

$$q \text{ reaktor} = 1,9100942 \text{ jam}$$

$$X_{A_0} = X_{A_1} - \frac{V k C_{A_0} (1 - X_{A_1})(M - X_{A_1})}{F_v}$$

$$X_{A_0} = 0,98 - \frac{112.131,1107 \times 325.846,97 \times 0,00024 \times 0,02 \times 0,626685}{58.704,4915}$$

$$= -8,885E-01$$

2. Jumlah Reaktor = 2

$$\begin{aligned}
X_{A_2} &= 0,98 \\
k &= 325.846,97 \text{ liter/kgmol jam} \\
F_v &= 58.704,492 \text{ liter/jam} \\
C_{A_0} &= 0,0002395 \text{ kgmol/liter} \\
M = B/A &= 1,606685 \\
V \text{ Coba} &= 12.792,101 \text{ liter} \\
q \text{ reaktor} &= 0,2179067 \text{ jam}
\end{aligned}$$

$$X_{A_1} = X_{A_2} - \frac{V k C_{A_0} (1 - X_{A_2})(M - X_{A_2})}{F_v}$$

$$\begin{aligned}
X_{A_1} &= 0,98 - \frac{12.792,101 \times 325.846,97 \times 0,0002395 \times 0,02 \times 0,626685}{58.704,4915} \\
&= 0,7668435
\end{aligned}$$

$$X_{A_0} = X_{A_1} - \frac{V k C_{A_0} (1 - X_{A_1})(M - X_{A_1})}{F_v}$$

$$\begin{aligned}
X_{A_0} &= 0,7668435 - \frac{12.792,101 \times 325.846,97 \times 0,0002395 \times 0,2331565 \times 0,839841}{58.704,4915} \\
&= -2,563309 \\
&= -25.633,09
\end{aligned}$$

3. Jumlah Reaktor = 3

$$\begin{aligned}
X_{A_3} &= 0,98 \\
K &= 325.846,97 \text{ liter/kgmol jam} \\
F_v &= 58.704,492 \text{ liter/jam} \\
C_{A_0} &= 0,0002395 \text{ kgmol/liter} \\
M = B/A &= 1,606685 \\
V \text{ Coba} &= 5.413,9507 \text{ liter}
\end{aligned}$$

$$q \text{ reaktor} = 0,0922238 \text{ jam}$$

$$XA_2 = XA_3 - \frac{V k CA_0 (1 - Xa_3)(M - Xa_3)}{Fv}$$

$$XA_2 = 0,98 - \frac{5.413,9507 \times 325.846,97 \times 0,0002395 \times 0,02 \times 0,626685}{58.704,4915}$$

$$= 0,8897866$$

$$XA_1 = XA_2 - \frac{V k CA_0 (1 - Xa_2)(M - Xa_2)}{Fv}$$

$$XA_1 = 0,8897866 - \frac{5.413,9507 \times 325.846,97 \times 0,0002395 \times 0,1102134 \times 0,716898}{58.704,4915}$$

$$= 0,321086$$

$$XA_0 = XA_1 - \frac{V k CA_0 (1 - Xa_1)(M - Xa_1)}{Fv}$$

$$XA_0 = 0,321086 - \frac{5.413,9507 \times 325.846,97 \times 0,0002395 \times 0,678914 \times 1,285599}{58.704,4915}$$

$$= -5,961117$$

$$= -59611,17$$

4. Jumlah Reaktor = 4

$$XA_4 = 0,98$$

$$k = 325.846,97 \text{ liter/kgmol jam}$$

$$Fv = 58.704,4915 \text{ liter/jam}$$

$$Ca_0 = 0,0002395 \text{ kgmol/liter}$$

$$M = B/A = 1,606685$$

$$V \text{ Coba} = 3.265,1681 \text{ liter}$$

$$q \text{ reaktor} = 0,0556204 \text{ jam}$$

$$XA_3 = XA_4 - \frac{V k CA_0 (1 - Xa_4)(M - Xa_4)}{Fv}$$

$$XA_3 = 0,98 - \frac{3.265,1681 \times 325.846,97 \times 0,0002395 \times 0,02 \times 0,626685}{58.704,4915}$$

$$= 0,9255921$$

$$XA_2 = XA_3 - \frac{V kCA_0(1 - Xa_3)(M - Xa_3)}{Fv}$$

$$XA_2 = 0,9255921 - \frac{3.265,1681 \times 325.846,97 \times 0,0002395 \times 0,0744079 \times 0,681093}{58.704,4915}$$

$$= 0,7055992$$

$$XA_1 = XA_2 - \frac{V kCA_0(1 - Xa_2)(M - Xa_2)}{Fv}$$

$$XA_1 = 0,7055992 - \frac{3.265,1681 \times 325.846,97 \times 0,0002395 \times 0,2944008 \times 0,901086}{58.704,4915}$$

$$= -0,445965$$

$$XA_0 = XA_1 - \frac{V kCA_0(1 - Xa_1)(M - Xa_1)}{Fv}$$

$$XA_0 = -0,445965 - \frac{3.265,1681 \times 325.846,97 \times 0,0002395 \times 1,4459648 \times 2,052650}{58.704,4915}$$

$$= -13,33011$$

$$= -133301,1$$

5. Jumlah Reaktor = 5

$$XA_5 = 0,98$$

$$K = 325.846,97 \quad \text{liter/kgmol jam}$$

$$Fv = 58.704,492 \quad \text{liter/jam}$$

$$Ca_0 = 0,0002395 \quad \text{kgmol/liter}$$

$$M = B/A = 1,606685$$

$$V \text{ Coba} = 2.298,5237$$

$$q \text{ reaktor} = 0,0391541 \quad \text{jam}$$

$$XA_4 = XA_5 - \frac{V kCA_0(1 - X_{a5})(M - X_{a5})}{Fv}$$

$$XA_4 = 0,98 - \frac{2.298,5237 \times 325.846,97 \times 0,0002395 \times 0,02 \times 0,626685}{58.704,4915}$$

$$= 0,9416994$$

$$XA_3 = XA_4 - \frac{V kCA_0(1 - X_{a4})(M - X_{a4})}{Fv}$$

$$XA_3 = 0,9416994 - \frac{2.298,5237 \times 325.846,97 \times 0,0002395 \times 0,0583006 \times 0,664986}{58.704,4915}$$

$$= 0,8232285$$

$$XA_2 = XA_3 - \frac{V kCA_0(1 - X_{a3})(M - X_{a3})}{Fv}$$

$$XA_2 = 0,8232285 - \frac{2.298,5237 \times 325.846,97 \times 0,0002395 \times 0,1767715 \times 0,783457}{58.704,4915}$$

$$= 0,4000208$$

$$XA_1 = XA_2 - \frac{V kCA_0(1 - X_{a2})(M - X_{a2})}{Fv}$$

$$XA_1 = 0,4000208 - \frac{2.298,5237 \times 325.846,97 \times 0,0002395 \times 0,5999792 \times 1,206664}{58.704,4915}$$

$$= -1,812305$$

$$XA_0 = XA_1 - \frac{V kCA_0(1 - X_{a1})(M - X_{a1})}{Fv}$$

$$XA_0 = -1,812305 - \frac{2.298,5237 \times 325.846,97 \times 0,0002395 \times 2,8123049 \times 3,418990}{58.704,4915}$$

$$= -31,19466$$

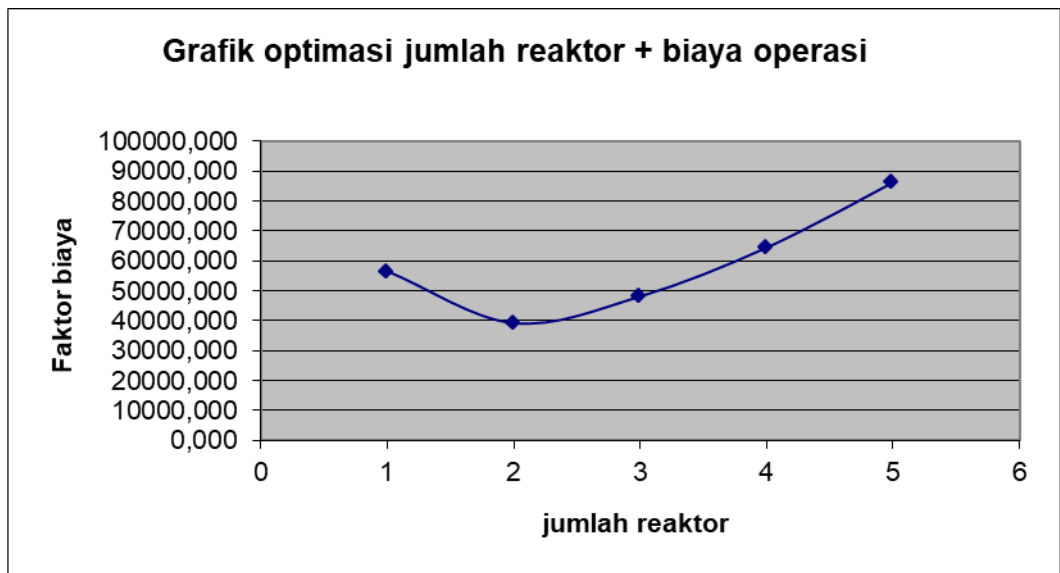
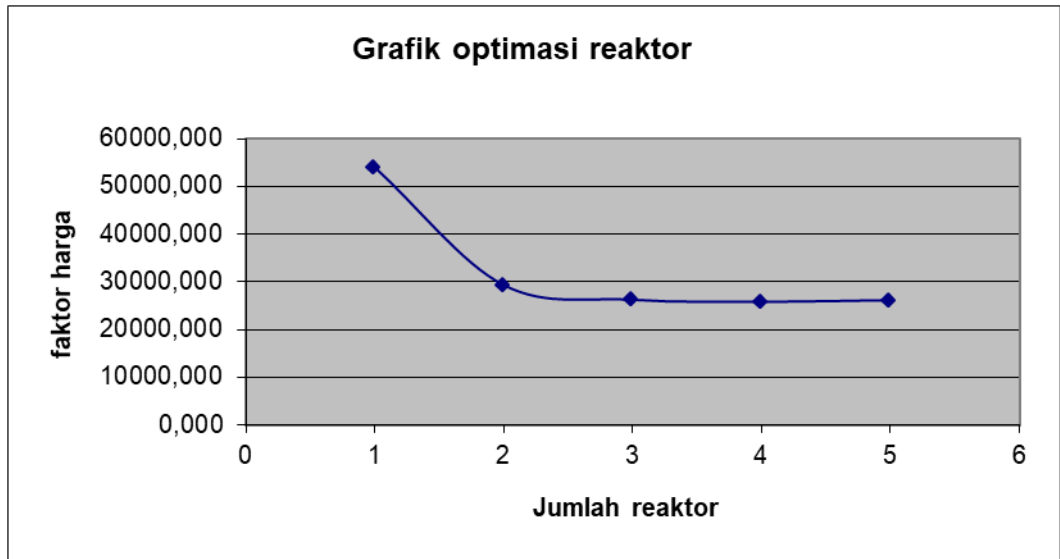
$$= -311946,6$$

n	Volume
1	112.131,11

2	12.792,10
3	5.413,95
4	3.265,17
5	2.298,52

Jumlah	Harga	Motor	Harga	Listrik/10th	Harga
1	54.000,000	0,500	200	29.529,716	2.362,377
2	29.359,808	1,000	400	118.118,864	9.449,509
3	26.289,839	1,500	600	265.767,444	21.261,396
4	25.879,829	2,000	800	472.475,457	37.798,037
5	26.205,803	2,500	1000	738.242,901	59.059,432

Jumlah	Harga
1	56.562,377
2	39.209,317
3	48.151,234
4	64.477,866
5	86.265,235



Digunakan jmlah reaktor seri = 2 reaktor

Konversi keluar reaktor 1 = 0,868 reaktor

Konversi keluar reaktor 2 = 0,980 reaktor

Volume tiap reaktor = 6.709,42 Lt

Over Design : 20 %

Volume reaktor = 1,20 X 6.709,42 lt

= 8.051 lt

dipakai Volume reaktor = 8.05 m³

Menghitung ukuran reaktor :

Reaktor berbentuk silinder tegak dengan perbandingan $H : D = 1,5 : 1$

$$V_t = \frac{\pi \cdot D^2 \cdot (h/d) \cdot D}{4} + \frac{\pi}{12} D^2 \cdot D$$

Atau :

$$\begin{aligned} \text{diameter (D)} &= \left[\frac{V_t}{\pi/4 (h/d) + \pi / 12} \right]^{1/3} \\ &= \left[\frac{8,051}{\pi/4 \cdot 1,50 + \pi / 12} \right]^{1/3} \\ &= 1,78 \text{ m} \end{aligned}$$

$$\begin{aligned} \text{Tinggi (H)} &= 1,5 \times 1,78 \\ &= 2,66 \text{ m} \end{aligned}$$

$$\text{Diperoleh ukuran Reaktor : Diameter} = 1,78 \text{ m}$$

$$\text{Tinggi} = 2,66 \text{ m}$$

$$\begin{aligned} \text{Volume cairan dalam head} &= (1/2)(\pi/12) 1,775^3 \\ &= 0,732 \text{ m}^3 \end{aligned}$$

$$\begin{aligned} \text{Volume cairan dibadan Reaktor} &= 6,709 \text{ m}^3 - 0,732 \text{ m}^3 \\ &= 5,977 \text{ m}^3 \end{aligned}$$

$$\begin{aligned} \text{Tinggi cairan dibadan Reaktor} &= 5,977 / 2,474 \text{ m} \\ &= 2,416 \text{ m} \end{aligned}$$

5. Menghitung tebal shell dan head

Tebal shell

Tekanan operasi (p) = 29,40 psi

Tekanan design (p) = 35,28 psi

Allowable stress = 18,750 psi

Efisiensi sambungan = 0,85

Faktor korosi = 0,125 in

Jari-jari Reaktor = 34,95 in

$$\begin{aligned}t_{\text{shell}} &= \frac{p \cdot r_i}{S \cdot e - 0,6 \cdot p} + c \\&= \frac{35 \times 34,95}{18.750 \times 0,85 - 0,6 \times 35,3} + 0,125 \\&= 0,202 \text{ in}\end{aligned}$$

Dipilih tebal shell 7/16 in

Tebal Head :

$$\begin{aligned}t_{\text{head}} &= \frac{0,885 \cdot p \cdot d}{2 \cdot S \cdot e - 0,2 \cdot p} + c \\&= \frac{0,885 \times 35 \times 69,89}{2 \times 18750 \times 0,85 - 0,2 \times 35,3} + 0,125 \\&= 0,193 \text{ in}\end{aligned}$$

Dipilih tebal head 7/16 in

6. Menghitung pengaduk dalam Reaktor

Dipilih : Pengaduk type Marine dengan 3 blade

Jumlah baffle 4 buah

Dari tabel 477 Brown diperoleh :

$$Dt/Di = 3$$

$$zi/Di = 0,75 - 1,3$$

$$W/Di = 0,1$$

$$\text{Diameter Impeler} = 59,17 \text{ cm}$$

$$\text{Tinggi Impeler} = 59,17 \text{ cm}$$

$$\text{Lebar Baffle} = 5,92 \text{ cm}$$

diambil :

$$zi/Di = 1$$

$$\text{Putaran} = 1,5 \text{ rps}$$

$$\text{efisiensi} = 80 \%$$

Tinggi baffle diambil sama dengan tinggi cairan

bilangan Reynold dalam Reaktor :

$$\begin{aligned} Re &= \frac{n \cdot di^2 \cdot \text{den}}{\text{visc}} \\ &= \frac{1,5 \times 59,17^2 \times 2,201}{0,0095} \\ &= 1.215.641,6 \end{aligned}$$

Dari fig. 477 brown diperoleh $po = 0.94$

$$po = \frac{P \cdot gc}{n^3 \cdot \text{den} \cdot Di^5} \quad (\text{pers. 461 Brown})$$

Atau

$$P = \frac{\rho_o \cdot n^3 \cdot \text{den.} \cdot D_i^5}{g_c}$$

$$= \frac{0,94 \times 1,50^3 \times 137,347 \times 1,941^5}{550 \times 32,17}$$

$$= 0,311 \text{ Hp}$$

Effisiensi : 80 %

$$\text{Power} = \frac{P}{\text{eff}} = \frac{0,311}{0,80}$$

$$= 0,388 \text{ Hp}$$

Digunakan motor dengan daya = 0,5 Hp

7. Menghitung perpindahan panas :

Dipilih pemanas Jacket dengan media pemanas Steam Jenuh

Dengan : Suhu masuk = 302 F

Suhu keluar = 302 F

Kebutuhan Steam Jenuh

$$W_a = \frac{Q}{H_{fg}}$$

Dengan Q : Jumlah panas yang harus diserap = 1.322.067 Btu/j

Hfg : Panas pengembunan steam = 978 Btu/lb

$$W_a = \frac{1.322.067 \text{ Btu/j}}{978,0 \text{ Btu/lb}}$$

$$= 1.351,806396 \text{ lb/j}$$

a. Menghitung koefisien transfer panas :

- Untuk steam dalam reaktor maka dipakai persamaan 20,4 Kern.

$$h_c = \frac{0.87 \cdot k}{D} \left[\frac{L^2 \cdot N \cdot \text{den}}{\text{visc.}} \right]^{2/3} \left[\frac{C_p \cdot \text{visc.}}{k} \right]^{1/3} \left[\frac{\text{visc.}}{\text{viscw.}} \right]^{0.14}$$

dengan :

h_c = Koeff. transfer panas steam, Btu/sqft j F

D_i = Diameter reaktor = 5,824207 ft

K = Konduktivitas panas = 1,835 Btu/j sqft (F/ft)

L = diameter putar pengaduk = 1,941402 ft

Den = densitas larutan = 2,201069 lb/cuft

C_p = panas jenis = 0,845743 Btu/lb F

Visc = Viskositas bahan = 7,797778E-04 lb/j ft

viscw = Viskositas bahan pada dinding = 5,604974 lb/j ft

$$\frac{L^2 \cdot N \cdot \text{den}}{\text{visc.}} = \frac{1,941402^2 \times 1,5 \times 2,201069}{0,000780}$$

$$= 15.958,250977$$

$$\frac{C_p \cdot \text{visc}}{k} = \frac{0,845743 \times 1,160000}{1,835000}$$

$$= 0.534639$$

$$\text{asumsi } \frac{\text{visc}}{\text{viscw}} = 1$$

$$h_c = \frac{0.87 \cdot 1.835000}{5,824207} \left[15.958,251 \right]^{2/3} \left[0.535 \right]^{1/3} \left[0.21 \right]^{0.14}$$

maka diperoleh :

$$h_c = 113,106079 \text{ Btu/j sqft F}$$

- Untuk pemanas dalam Jacket :

$$\begin{aligned} Re &= \frac{D \cdot Wa}{\text{Visc} \cdot At} \\ &= \frac{77,1858/12 \times 1.351,81}{4,348740 \times 2,732/144} \\ &= 105.384,5938 \end{aligned}$$

Unk kondensasi steam diperoleh $h_{io} = 1.500 \text{ Btu/j ft}^2 \text{ F}$

b. Overall heat transfer U_d :

Overall transfer panas saat start up

$$\begin{aligned} U_c &= \frac{h_{io} \cdot h_o}{h_{io} + h_o} \\ &= \frac{1.500,00 \times 113,11}{1.500,00 + 113,11} \\ &= 105,175423 \text{ Btu/j ft}^2 \text{ F} \end{aligned}$$

Dari Kern p.846 untuk Steam Jenuh $R_d = 0,0005$

dan untuk bahan organik $R_d = 0,001$

Jadi $R_d \text{ total} = 0,0015$

$$\begin{aligned} U_d &= \frac{U_c}{U_c \cdot R_d + 1} \\ &= \frac{112,41}{105,18 \times 0,0020 + 1} \end{aligned}$$

maka diperoleh :

$$U_d = 86,896637 \text{ Btu/j sqft F}$$

c. Menghitung Luas transfer panas :

$$\begin{aligned} \text{LMTD} &= T_1 - t_1 \\ &= 302,0 - 194,0 \\ &= 108,00 \text{ F} \end{aligned}$$

maka luas perpindahan panas :

$$\begin{aligned} A_o &= \frac{Q}{U_d \cdot \text{LMTD}} \\ &= \frac{1.322.066,6250}{86,896637 \times 108,00} \\ &= 140,872635 \text{ ft}^2 \end{aligned}$$

Tinggi Jacket :

$$\begin{aligned} H &= \frac{A \text{ Silinder}}{\text{Keliling}} \\ &= \frac{114,244339}{\pi \cdot 5,824207} \\ &= 6,246953 \text{ ft} \\ &= 1,904071 \text{ m} \end{aligned}$$

Sedangkan tinggi Cairan dalam reaktor = 2,416269 m

Jadi Tinggi cairan lebih tinggi dari tinggi Jacket.

8. Spesifikasi Reaktor

Tugas : Produk NaOH dan NaCl dari limbah CSG dengan kecepatan umpan =

6.313,13131 Kg/jam

Jenis : Reaktor Alir Tangki Berpengaduk

Kondisi Operasi : Tekanan = 1 atm

Suhu = 90 °C

Diperoleh ukuran reaktor : Diameter = 1,78 m

Tinggi = 2,66 m

Volume cairan dalam *head* = 0,732 m

Volume cairan dibadan RATB = 5,977 m

Tinggi cairan dibadan RATB = 2,416 m

Dipilih Tebal shell : 7/16 in

Tebal Head : 7/16 in

Dipilih : Pengaduk tipe Marine dengan 3 blade

Jumlah baffle 4 buah

Diameter Impeler = 59,17 cm

Tinggi Impeler = 59,17 cm

Lebar Baffle = 5,92 cm

Digunakan motor dengan daya = 0,5 Hp

Luas perpindahan Panas : A = 140,8726 ft²

Jacket pendingin : Tebal Jacket = 15,748032 in

Tinggi Jacket = 6,246953 ft

Tebal Isolasi : Tebal Isolasi = 3 in

Jenis bahan Isolasi = Asbes

Jenis Bahan Reaktor : Baja Steinless Steel

Jumlah reaktor = 2