

LAMPIRAN**REAKTOR**

Jenis	= Reaktor alir tangki Berpengaduk (CSTR)
Fase	= Cair - Gas
Bentuk	= Tangki Silinder
Jumlah	= 1
Head	= Torispherical dished head 342, Brownell & Young
Bahan	= Stainless Steel SA 167 grade 10 tipe 310 (Appendix D, item 4, halaman342, Brownell & Young)
Suhu Operasi	= 35 °C
Tekanan	= 3 atm
Waktu Tinggal (θ)	= 35 hari = 840 jam
Laju Alir Massa	= 37.224,6000 Kg/jam
Densitas Kotoran Sapi	= 1200 Kg/m ³
Volume Cairan	= 226057,2200 m ³

A. Menghitung Dimensi Reaktor

Perancangan reaktor dibuat dengan over design sebesar 20%,

sehingga volume reaktor menjadi :

$$\text{Volume reaktor} = 1,2 \times \text{volume cairan}$$

$$\text{Volume reaktor} = 1,2 \times 22657,2200 \text{ m}^3$$

$$\text{Volume reactor} = 31.268,664 \text{ m}^3$$

1. Menghitung diameter dan tinggi reaktor

Reaktor yang digunakan berbentuk silinder tegak

$$\begin{aligned}\text{Volume} &= \text{volume silinder} + \text{volume tutup} \\ &= \text{volume silinder} + 2 \text{ volume head}\end{aligned}$$

Tutup berbentuk *torispherical dished head*

Dengan :

Volume head = 0,000049 d³

Sehingga :

$$\text{Volume} = \left(\frac{1}{4} \times \pi \times D^2 \times H \right) + [2 \times (0,000049) \times (D^3)]$$

$$\text{Diameter tangki} = \left(\frac{31268,664}{5.420598} \right)^{1/3}$$

$$\text{Diameter tangki} = 18,3943202 \text{ m} = 60,3488 \text{ ft}$$

Perbandingan diameter dan tinggi reactor = 2.5 : 1

Maka tinggi reaktor :

$$H = 7,357728063 \text{ m} = 24,1395 \text{ ft}$$

Diambil ukuran standar tangki : (App., E, Brownell)

$$\text{Diameter standar} = 70 \text{ ft} = 840 \text{ in} = 21,3360 \text{ m}$$

$$\text{Tinggi standar} = 30 \text{ ft} = 360 \text{ in} = 9,1440 \text{ m}$$

Sehingga kapasitas standar tangki sebesar= 3268,77272 m³

Menentukan Tebal shell

$$ts = \frac{P \cdot ri}{f \cdot E - 0,6P} + C \quad \text{Eq. 14.34 (Brownell & Young. 275)}$$

ts:tebal shell, in

ri:jari-jari shell, (D/2), in

f:allowable stress, psi (Tabel 13.1 Brownell 251)

E:joint efficiensi tipe double-butt weld (0.8) (Tabel 13.2 Brownell 254)

C:faktor koreksi, in (Tabel 6. Timmerhaus, 1991: 542)

P:internal pressure, lb/in²

Diketahui:

Allowble working stres (f) =18750 psi

Joint efficieny (E) =0.8

Faktor korosi (C) = 0.125

umur alat (n) = 10 tahun

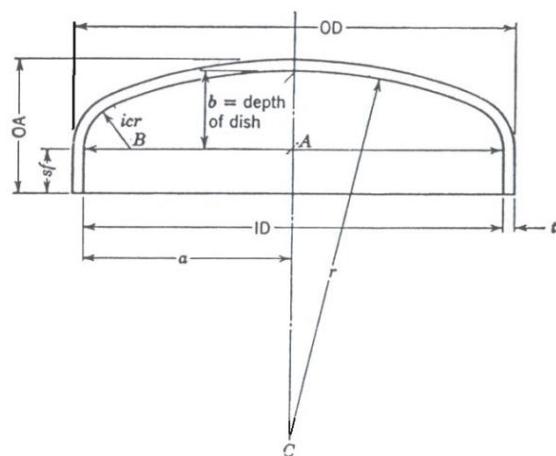
Sehingga, Tebal Shell yang diperoleh adalah:

$$ts = 1,1135 \text{ in}$$

$$ts \text{ standar} = 1(1/8)\text{in} = 1,125 \text{ in}$$

B. Menentukan Head Design

1. Menentukan jenis head



Head yang digunakan adalah jenis *Torispherical dished head*

Keterangan :

T = Tebal head, in

icr = Inside corner radius, in

r = Radius of dish, in

OD = Outside diameter, in

ID = Inside diameter, in

b = Depth of dish, in

sf = Straight flange

2. Material : Stainless Steel SA 167 grade 10 tipe 310

3. Menentukan tekanan desain reaktor

$$P_{\text{operasi}} = 3 \text{ atm} = 44,1 \text{ psia}$$

$$P_{\text{hidrostatik}} = \frac{\rho(g/g_c)H_L}{144} = 12,5582 \text{ psi}$$

Tekanan desain 5 – 10% di atas tekanan kerja normal/absolut (Coulson, 1983). Tekanan desain diambil 5% di atas tekanan kerja normal.

$$P_{\text{desain}} = 1,05 \times (P_{\text{operasi}} + P_{\text{hidrostatik}})$$

$$P_{\text{desain}} = 1,05 \times (44,1 + 12,5582)$$

$$P_{\text{desain}} = 59,43 \text{ psi}$$

4. Menentukan tebal head (th)

$$t_h = \frac{PD}{(2fE - 0,2P)} + c$$

$$f = 18750 \text{ psi} \quad (\text{Brownell \& Young, 1959})$$

$$E = 0.8 \quad (\text{double welded butt joint})$$

$$c = 0.125 \text{ in}$$

$$D = 1680 \text{ in} \quad (\text{Brownell \& Young, 1959})$$

$$P_{\text{operasi}} = 3 \text{ atm}$$

$$\text{diperoleh Tebal Head (th)} = 1.113 \text{ in}$$

$$\text{th standar} = 1(1/8)=1.125 \text{ in}$$

5. Menentukan tinggi head (h_h)

$$t_h = \frac{0,885 \cdot P \cdot r_c}{f \cdot E - 0,1 \cdot P}$$

P = Tekanan Perancangan, Psi

f = Tekanan maksimum yang diijinkan pada bahan, Psi

E = Welded joint efficiency

r_c = radius of crown

t_h = tebal head

i_{cr} = inside radius corner

$r_c = OD$ (Brownell & Young hal 88)

$i_{cr} = 6\% \times OD$ (For torispherical dished head in which the knuckle radius is 6% of the inside crown radius)

$$OD = ID + 2t$$

$$= 1682.25 \text{ in}$$

$$r_c = 1682.25 \text{ in}$$

$$i_{cr} = 100.935 \text{ in}$$

jika, $ODs = 1680$ in

$$t_h = 1.125 \text{ in}$$

dari tabel 5.7 Brownell hal.90 didapat:

$$i_{cr} = 100.94 \text{ in}$$

$$r = 1682.25 \text{ in}$$

$$a = ID_s/2 = 840 \text{ in}$$

$$AB = a - icr = 739.065 \text{ in}$$

$$BC = r - icr = 1581 \text{ in}$$

$$AC = (BC^2 - AB^2)^{1/2} = 1397.977 \text{ in}$$

$$b = r - AC = 284.273 \text{ in}$$

Dari tabel 5.6 Brownell hal.88 dengan th 5/8 in didapat sf = 1.5 - 3.5 in

perancangan digunakan sf = 3 in

Sehingga, tinggi head (Hh) yang diperoleh adalah:

$$Hh = th + b + sf$$

$$= 288.398 \text{ in}$$

$$= 24.033 \text{ ft}$$

$$= 7.325 \text{ m}$$

Tinggi total tangki penyimpanan U.K :

$$\text{tinggi tangki + tutup} = 14.641 \text{ m}$$

C. Menghitung Dimensi Pengaduk

Volume cairan yang diaduk = 26057.2200 m³

Jenis pengaduk yang dipilih yaitu *Flat Six-Blade Turbine Impeller*

with disk

Perancangan untuk pengadukan dilakukan dengan prinsip similaritas

menggunakan model sesuai dengan referensi buku Brown

$$\frac{Da}{Dt} = 1:3 \quad \frac{L}{Da} = 1:4 \quad \frac{J}{Dt} = 1:12 \quad \frac{E}{Da} = 1:1 \quad \frac{W}{Da} = 1:5$$

Dimana:

D_t = Diameter tangki W = Lebar blade

D_a = Diameter impeller L = Panjang blade

E = Tinggi impeller J = Lebar baffle

Maka diperoleh :

- a. Diameter Impeller (D_a) = $\frac{1}{3} \times 21,3360 \text{ m} = 7,112 \text{ m}$
- b. Tinggi pengaduk dari dasar tangki (E) = $D_a = 7,112 \text{ m}$
- c. Lebar baffle (J) = $1/2 D_t = 1,778 \text{ m}$
- d. Lebar blade (W) = $1/5 \times D_a = 1,422 \text{ m}$
- e. Panjang blade (L) = $1/4 D_a = 1,778 \text{ m}$
- f. Kecepatan pengadukan, = 0,1 Putaran/detik (Tabel 10.2 Wallas)

Menghitung nilai Re :

$$Re = \frac{\rho \times N \times D_i^2}{\mu}$$

$$Re = \frac{1200 \times 0,1 \times (7,112)^2}{0,97}$$

$$Re = 6257,386887$$

Dari grafik 10.6 hal 292 (Wallas) diperoleh $NP = 3$

Sehingga :

$$P = \frac{N^3 \times D_i^5 \times \rho \times P_o}{gc}$$

$$P = 65503.007 \text{ watt}$$

$$P = 87,84 \text{ Hp}$$

Effisiensi motor $\eta = 80\%$ (Peters,dkk 2004)

$$\text{Daya motor} = 87,84 \times 0,8 = 109,801 \text{ Hp}$$

Sehingga, diambil daya motor standar 125 Hp