

LAMPIRAN

Perhitungan Reaktor

Fungsi : Tempat berlangsungnya reaksi dehidrogenasi Etanol menjadi Asethaldehid

Type : Fixed Bed Multi Tube

Kondisi operasi : Nonadiabatis - nonisothermal

T umpan = 260,0000 C = 533,0000 K

P umpan = 1,5000 atm

Fasa = Gas

1. Neraca Massa

Umpan masuk reaktor

Komponen	kmol/jam	fraksi mol	kg/jam
C ₂ H ₅ O	74,9820	0,9500	3449,1720
H ₂ O	3,9467	0,0500	71,0406
Total	78,9287	1,0000	3520,2126

Produk keluar reaktor

Komponen	kmol/jam	fraksi mol	kg/jam
CH3CHO	37,4933	0,3220	1649,7041
C2H5O	37,4933	0,3220	1724,6907
H2O	3,9467	0,0339	71,0399
H2	37,4933	0,3220	74,9866
Total	116,4265	1,0000	3520,4212

2. Viskositas (data diperoleh dari Yaws)

$$\mu_{\text{gas}} = A + BT + CT^2 \text{ (Joule/mol K)}$$

$$0,000339941 \text{ (Poise=g/cm s)}$$

3. viskositas campuran gas (Perry,1984)

$$\mu_{\text{mix}} = \frac{\sum (y_i \cdot \mu_i) \cdot (BM_i)^{0,5}}{\sum y_i \cdot BM_i^{0,5}}$$

$$\text{total} = 0,00102368 \quad 6,6553$$

$$\mu_{\text{mix}} = 0,00015381 \text{ g/cm.s}$$

4. Cp (data diperoleh dari Yaws)

$$C_p = A + BT + CT^2 + DT^3 + ET^4 \text{ (Joule/mol K)}$$

$$Y_i \cdot C_{p_i} = 2,12511998 \text{ Cp,j/g.K}$$

5. Konduktivitas Termal (data diperoleh dari Yaws)

$$\text{gas} = A + BT + CT^2 \text{ (W/m K)}$$

$$K \text{ gas mix} = 0,0417 \text{ W/m.K}$$

6. Menghitung Harga ΔHR (ΔH_f diperoleh dari Smith Vaness)

$$\Delta HR_{298} = \Delta H_f \text{ produk} - \Delta H_f \text{ reaktan}$$

$$\Delta HR = \Delta HR_{298} + \int C_p dT = 68920,0001$$

$$= 68,9100 \text{ kJ/mol} = 10,0001$$

$$= 68910,0000 \text{ j/mol} = 68910,0000$$

7. Densitas Umpan Gas (data diperoleh dari Carl Yaws)

$$\text{Densitas mix} = 0,9871 \text{ kg/m}^3 = 0,0010 \text{ g/cm}^3$$

8. Katalisator

$$\text{Katalis} = \text{Tembaga (Cu)}$$

$$\text{diameter} = 0,3450 \text{ cm}$$

$$\text{Partikel density} = 8,9600 \text{ g/cm}^3 \text{ [wikipedia]}$$

$$\text{Specific surface area} = 342,0000 \text{ m}^2/\text{g}$$

$$\text{porosity } (\epsilon) = 0,3500$$

9. Menentukan Jenis dan Ukuran Tube

Diameter reaktor dipilih berdasarkan pertimbangan agar perpindahan panas berjalan dengan baik.

Pengaruh rasio D_p/D_t terhadap koefisien perpindahan dalam pipa yang berisi butir-butir katalisator dibandingkan dengan pipa kosong (hw/h), telah diteliti oleh Colburn's, yaitu :

D_p/D_t 0,0500 0,1000 0,1500 0,2000 0,2500 0,3000

hw/h 5,5000 7,0000 7,8000 7,5000 7,0000 6,6000

(Smith, Chem Kinetik Eng, P.571)

dipilih $D_p/D_t = 0,1500 \text{ in} = 0,381 \text{ cm}$

dimana :

hw : koefisien perpindahan panas dalam pipa berisi katalis

h : koefisien perpindahan panas dalam pipa kosong

D_p : diameter katalisator

D_t : diameter tube

sehingga :

$$D_p/D_t = 0,1500 \text{ cm} = 0,0591 \text{ in}$$

$$D_p = 0,3450 \text{ cm} = 0,1358 \text{ in}$$

$$D_t = 2,3000 \text{ cm} = 0,9055 \text{ in}$$

dari hasil perhitungan, maka dipilih ukuran pipa standart :

IPS = 1,0000 in

OD = 1,3200 in 3,3528

Sc. Number = 40,0000

ID = 1,0490 in 2,6645 cm

Flow area per pipe = 0,8640 in²

Surface per lin ft :

Outside = 0,3440 ft²/ft (Kern, Pros.heat.tranf,

P.844)

Inside = 0,2740 ft²/ft

Weight per lin ft = 1,6800 lb steel

10. Menghitung Pemanas yang Dibutuhkan

Panas umpan reaktor :

suhu = 260,0000 C 533,0000 K

Komponen	Cp.dT (Kj/kmol)	Flowrate, kmol/j	Panas, kJ/jam
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C ₂ H ₅ OH	19364,44778	74,9820	1451985,0237
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H ₂ O	8103,418614	3,9467	31981,7622
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total = 1483966,7860

Produk keluar reaktor

$$\text{suhu} = 260,0000 \quad \text{C} \quad 533,0000 \quad \text{K}$$

Komponen	Cp.dT (Kj/kmol)	Flowrate, kmol/jam	Panas, kJ/jam
C ₂ H ₅ OH	19364,44778	37,4933	726036,5712
C ₂ H ₄ O	15832,87175	37,4933	593626,2188
H ₂ O	8103,418614	3,9467	31981,4426
H ₂	6842,497523	37,4933	256547,6432
total =	1608191,8757		

$$\text{Panas reaksi} = 2583348,0212 \text{ kJ/jam}$$

$$\text{Panas yang diberikan oleh pemanas} = -2707573,1110 \text{ kJ/jam}$$

Pemanas yang dipakai adalah steam :

$$\text{suhu steam masuk} = 350,0000 \text{ C} \quad 623,0000 \text{ K}$$

$$\text{suhu steam keluar} = 317,0000 \text{ C} \quad 590,0000 \text{ K}$$

$$\text{Cp air} = 4,1800 \text{ kJ/kg C} = 1,0000 \text{ kkal/jam}$$

$$\text{Steam panas yang dibutuhkan} \quad 19628,6292 \text{ kg/j} \rightarrow 20000 \text{ kg/jam}$$

11. Menentukan Jumlah Tube

$$\text{asumsi Re} = 3000$$

$$\text{Dp} = 0,3450 \text{ cm}$$

$$\mu = 0,00015381 \text{ g/cm.s}$$

$$G \text{ (umpan total)} = 3520,2126 \text{ kg/jam}$$

$$= 977,8368333 \text{ g/s}$$

$$G_t \text{ (kec. Massa per satuan luas)} = 1,337502421 \text{ g/cm}^2 \cdot \text{s}$$

$$A_t \text{ (luas penampang total)} = 731,0916362 \text{ cm}^2$$

Luas Penampang Pipa

$$A_o = 1,9505 \text{ cm}^2 = 0,000195055 \text{ m}^2$$

Jumlah Pipa Maksimal (Nt max)

$$N_t \text{ max} = 374,8 \text{ buah}$$

$$N_t = 220,4 \text{ Jumlah tube}$$

Note:

$$\text{densitas } s = 8,9600 \text{ g/cm}^3$$

$$P = 1 \text{ atm}$$

$$BM = 29 \text{ g/gmol}$$

$$R = 82,06 \text{ cm}^3 \text{ atm/gmol K}$$

$$T \text{ udara} = 298 \text{ K}$$

sehingga:

$$\text{densitas udara} = 0,001185906 \text{ g/cm}^3$$

$$\text{densitas B} = 5,824415067 \text{ g/cm}^3 = 5824415,067 \text{ G/M}^3$$

$$Q_v = 3566,081987 \text{ m}^3/\text{jam}$$

$$V_{\text{max}}^2 = 2662122,124$$

$$V_{\text{max}} = 1631,601092 \text{ cm/det} = 1631,601092$$

$$58737,63932 \text{ m/jam}$$

$$A_t = 0,060712041 \text{ m}^2$$

maka jumlah pipa min:

$$N_{t \text{ min}} = 311,2567116 \text{ buah}$$

jadi jumlah tube : 240-289 buah

$$\text{diambil } N_t = 240 \text{ buah}$$

12. Menghitung IDs (diameter reaktor)

Pipa (tube) disusun dengan pola 'triangular pitch' agar turbulensi yang terjadi pada aliran fluida dalam shell

Menjadi besar, sehingga akan memperbesar koefisien perpindahan panas konveksi (h_o)

$$\text{Susunan tube} = \text{triangular}$$

$$\text{Pitch tube (PT)} = 1.25 \text{ Odt} = 1,65 \text{ in} = 4,1910 \text{ cm}$$

$$\text{Clearance (C')} = \text{PT} - \text{OD} = 0,3300 \text{ in} = 0,8382 \text{ cm}$$

untuk menghitung diameter shell, dicari luas penampang shell total (A total).

luas shell = luas segitiga

A total = 2. Nt. (luas segitiga ABC)

$$\pi/4 * ID_s^2 = 2. Nt (1/2 * PT^2 * \sin 60)$$

$$\pi/4 * ID_s^2 = 2. Nt (1/2 * PT^2 * 0.866)$$

$$ID_s = 68,1942 \text{ cm} = 26,8481 \text{ in}$$

13. Menghitung koefisien perpindahan panas overall (Ud)

a. tube side

$$C_p = 94,99104265 \text{ kJ/kmol K} = 2,12511998 \text{ j/g k} = 0,507576407 \text{ btu/lb.F}$$

$$\mu = 0,00015381 \text{ g/cm s} = 0,037208695 \text{ lb/ft.h}$$

$$k = 0,0417 \text{ W/m k} = 0,024094637 \text{ Btu/ft h F}$$

$$Pr = C_p \cdot \mu / k = 0,783836506$$

$$G_t = 1,337502421 \text{ g/cm}^2 \cdot \text{s}$$

$$D_p = 0,3450 \text{ cm}$$

$$Re_t = G_t \cdot D_p = 3000 \rightarrow \text{ dari fig. 24 Kern, didapat } j_H = 12$$

$$h_i = 3,049766496 \text{ btu/hr.ft}^2 \cdot \text{F}$$

$$h_{io} = h_i \times (ID/OD) = 2,423640192 \text{ btu/hr.ft}^2 \cdot \text{F}$$

b. Shell side

Didalam shell digunakan steam sebagai media pemanas, dengan spesifikasi sbb :

$$C_p = 0,39 \text{ Btu/lb.oF} = 0,39 \text{ kkal/kg.K}$$

$$\mu = 0,0302 \text{ lb/ft.h} = 0,00012484 \text{ gram/cm.s}$$

$$k = 0,0127 \text{ Btu/ft.h}$$

Menghitung bilangan Reynold di shell (Res)

$$ID_s = \text{diameter dalam shell} = 26,8481 \text{ in}$$

$$B = \text{baffle spacing } (0.25 \cdot ID_s) \dots \text{kern,1965} = 6,7120 \text{ in}$$

$$PT = \text{pitch tube} = 1,6500 \text{ in}$$

$$C' = \text{jarak antar tube (clearance)} = 0,3300 \text{ in}$$

$$W_s = \text{laju aliran pemanas} = 20000,00 \text{ kg/jam} = 44092,4 \text{ lb/h}$$

$$a_s = \text{flow area pada shell, ft}^2$$

$$= (ID_s \cdot C' \cdot B) / (144 \cdot PT)$$

$$= 0,2503 \text{ in}^2$$

$$= 0,001737979 \text{ ft}^2$$

$$G_s = \text{mass velocity fluida dalam shell, lb/ft}^2 \cdot \text{h}$$

$$= W_s / a_s$$

$$= 176168,7 \text{ lb/ft}^2 \cdot \text{h}$$

Diameter Equivalen (D_e) (keren, 1983) P.139

$$D_e = 4 (0.5 P_t^2 \cdot 0.866 - 0.5 \pi \cdot (OD^2)/4) 0.5 \pi OD$$

$$D_e = 1,9453 \text{ in} = 0,162103388 \text{ ft} = 4,941108917 \text{ cm}$$

$$Res = (G_s \cdot D_p) / \mu_s = 945614,2547$$

dari fig.28 Kern, hal.838 didapat $j_H = 45$

$$h_o = 3,4381 \text{ Btu/h.ft}^2 \cdot \text{oF}$$

c. Clean overall coefficient (U_c)

$$U_c = 1,4215 \text{ Btu/h.ft}^2 \cdot \text{oF}$$

dari tabel.12 Kern, hal.845, didapat $\rightarrow R_d \text{ shell} = 0,0005$

$$R_d \text{ tube} = 0,001$$

$$R_d = R_d \text{ shell} + R_d \text{ tube} = 0,0015$$

$$U_d = 1,4185 \text{ Btu/h.ft}^2 \cdot \text{F}$$

$$= 6,9252 \text{ kkal/h.m}^2 \cdot \text{K}$$

$$= 28,9943 \text{ kj/jam.m}^2 \cdot \text{k}$$

14. Menghitung panjang reaktor

Persamaan yang digunakan :

$\frac{dX_A}{dZ}$	$= \frac{(-r_A) \rho_b \cdot Nt \cdot \pi / 4 \cdot (IDt)^2}{FAo}$	
$\frac{dT_s}{dZ}$	$= \frac{Ud \cdot \pi \cdot ODt \cdot Nt \cdot (T - T_s)}{Ws \cdot Cps}$	
$\frac{dT}{dZ}$	$= \frac{Ud \pi \cdot ODt Nt (T - T_s) + (-\Delta H_R) \cdot FAo \frac{dX}{dZ}}{\sum (F_i C_{p_i})}$	
$\frac{dP}{dZ}$	$= \frac{G}{\rho \cdot g \cdot Dp} \frac{(1 - \varepsilon)}{(\varepsilon)^3} \left(\frac{150 (1 - \varepsilon) \mu}{Dp} + 1.75 G \right)$	

$(-r_A) =$	$k_0 \exp \left[-\frac{Ea}{R.T} \right] \cdot \frac{F_{A_0} (1 - x)}{F_{T_0}} \cdot P$
$\Delta HR =$	$\Delta HR_{298} + \int_{298}^T \Delta C_p dT$
$\sum F_i C_{p_i} =$	$[F_{A_0}(1-x)C_{p_A}] + [(F_{B_0} + \frac{1}{2}F_{A_0}x)C_{p_B}] + [(F_{C_0} + \frac{1}{2}F_{A_0}x)C_{p_C}]$

konversi (X) = 0,467205047 = 0,5000

suhu gas masuk (Tin) = 533 K

suhu gas keluar (Tout) = 533,1652059 K = 260,0152 °C

Z (panjang pipa tube) = 2,2000 m = 86,6139 inch

tekanan masuk (P in) = 1,5 atm

tekanan keluar (P out) = 0,164704 atm

suhu pemanas masuk (Ts in) = 623 K

suhu pemanas keluar (Ts out) = 621,7380133 K

Dimensi Reaktor

		in	cm	1:10
<u>Tube :</u>	panjang =	86,613912	220,00	22,00
	IDt =	1,0490	2,66	0,27
	ODt =	1,3200	3,35	0,34
	pitch (PT) =	1,65	4,19	0,42
	clearance (C) =	0,3300	0,84	0,08
	penyangga tube =	0,130798033	0,33	0,03
<u>shell :</u>	IDs =	26,8481	68,19	6,82
	ODs =	27,22310779	69,15	6,91
	baffle space (B) =	6,7120	17,05	1,70
	ts =	0,1875	0,48	0,05
<u>head :</u>	tH =	0,1601	0,41	0,04
	hH =	6,9050	17,54	1,75
	icr =	1,7500	4,45	0,44
	r =	26,0000	66,04	6,60
	sf =	2	5,08	0,51
	(tinggi reaktor) HR =	100,4239427	255,08	25,51
<u>Nozzle :</u>	D gas in =	8,8384	22,45	2,24
	D gas out =	18,8245	47,81	4,78
	D pemanas in =	8,0447	20,43	2,04
	D pemanas out =	8,0447	20,43	2,04
<u>Isolasi :</u>	t (isolasi) =	1,37	3,48	0,35